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## COMPUTER PROGRAM FOR VIBRATION PREDICTION OF FIGHTER AIRCRAFT EQUIPMENTS

*COMBINED ENVIRONMENTS TEST GROUP  
ENVIRONMENTAL CONTROL BRANCH  
VEHICLE EQUIPMENT DIVISION*

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Final Report for Period 21 March 1976 to 15 April 1977

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AIR FORCE FLIGHT DYNAMICS LABORATORY  
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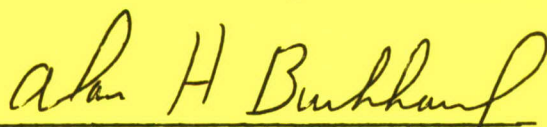
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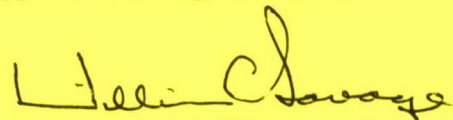
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the resultant vibration spectrum; beginning at the aircraft surface and proceeding inward to the designated equipment. Program inputs specify flight conditions, aircraft structural classes, equipment weight, equipment locational coordinates, and mounting categories in order to characterize vibration inputs of fighter aircraft equipments during flight attitudes ranging from straight and level states to a variety of significant flight maneuvers and phases. Program outputs, digital and graphical, are designed to provide the direct spectral information necessary to assemble sequential vibration histories corresponding to fighter aircraft mission profiles.

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FOREWORD

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This joint report was prepared by the Vehicle Equipment Division, Air Force Flight Dynamics Laboratory (FEE) and by the ASD Computer Center (ADDS), Wright-Patterson Air Force Base, Ohio. The report contains the results of an in-house research program to develop a computer program for the utilization of a vibration prediction technique applied to equipments mounted in fighter aircraft.

This work was conducted from 21 March 1976 to 15 April 1977 under Task 61460412 with Robert W. Sevy as project engineer and under Problem Number D760078 with Mark N. Haller as mathematician.



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## SYMBOLS

$\theta$	angle (rads)
$\beta$	slope factor, low frequency rolloff
$\beta'$	slope factor, high frequency rolloff
$\alpha$	form factor for low frequency rolloff segment of flex function
$\alpha'$	form factor for high frequency rolloff segment of flex function
$\omega_o$	locator frequency, low frequency rolloff (rads/sec)
$\omega_o'$	locator frequency, high frequency rolloff (rads/sec)
$f_o$	locator frequency, low frequency rolloff (Hz)
$f_o'$	locator frequency, high frequency rolloff (Hz)
$f_x$	frequency value at $x$ (given $f_o$ ) (Hz)
$f_{x'}$	frequency value at $x'$ (given $f_o'$ ) (Hz)
$f_n$	first fuselage bending mode, vertical, symmetric (Hz)
$f_{2n}$	second fuselage bending mode, vertical, symmetric (Hz)
$f_c$	center, or resonance frequency of $Y(f)$
$a$	acceleration, rms (ft/sec <sup>2</sup> )
$x$	normalizing frequency ratio, low frequency rolloff; also aerodynamic distance downstream from A/C nose (ft)
$x_E$	aerodynamic distance downstream - from A/C nose to equipment location (ft)
$x_{BT}$	value of $x$ to A/C mid chord at wing - fuselage junction (ft)
$x_L, x_T$	value of $x$ to main landing gear strut (ft)
$x'$	normalizing frequency ratio, high frequency rolloff
$I$	integral of the flex function

## SYMBOLS (CONTINUED)

$\delta_o$	boundary layer thickness, zero altitude (ft)
$\delta_b$	boundary layer thickness at altitude (ft)
H	altitude (ft)
C	speed of sound (ft/sec)
q	dynamic pressure (PSF)
U	free stream velocity (ft/sec)
M	mach number
$\rho_o$	density of air at zero altitude (slug/ft <sup>3</sup> )
$\rho$	density of air at altitude (slug/ft <sup>3</sup> )
P(f)	pressure spectral density (dynes/cm <sup>2</sup> ) <sup>2</sup> /Hz
$\phi_n(x)$	normalized mode shape (fuselage)
L(f)	low frequency transfer function of primary structure
$L_m(f)$	maximum value of L(f)
M(f)	medium frequency transfer function of primary structure
$M_m(f)$	maximum value of M(f)
H(f)	high frequency transfer function of primary structure (aircraft skin)
G(f)	primary structure response, (g <sup>2</sup> /Hz)
Y(f)	transfer function of equipments mounted on secondary structure
$Y_m(f)$	maximum value of Y(f)
$Y_{I(a)}$	Y(f) for equipment mounting category, I(a)
R(f)	response of secondary structure (g <sup>2</sup> /Hz)
e	load offset distance from maximum response location on secondary structure (in)

## SYMBOLS (CONTINUED)

$R_e(f)$	adjusted value of $R(f)$ due to $\epsilon$ ( $g^2/Hz$ )
$S_{BT}(f)$	special function for the buffet turn flight phase
$P_{BT}(f)$	pressure spectral density spectrum of a fighter aircraft during buffet turn ( $PSF^2/Hz$ )
$S_T(f)$	special function for the takeoff phase
$P_T(f)$	equivalent pressure spectral density spectrum of an aircraft during the takeoff phase ( $PSF^2/Hz$ )
$S_L(f)$	special function of an aircraft during the landing phase
$P_L(f)$	equivalent pressure spectral density spectrum of an aircraft during the landing phase ( $PSF^2/Hz$ )
$R_s$	distance in from the skin (inches)
$W_E$	equipment weight (lbs)
$W_s$	surface density of skin ( $lbs/ft^2$ )
$P_m(f)$	maximum value of $P(f)$ ( $dynes/cm^2$ ) <sup>2</sup> /Hz
$H_m(f)$	maximum value of $H(f)$
$P_{mBT}$	maximum value of $P(f)$ during buffet turn ( $dynes/cm^2$ ) <sup>2</sup> /Hz
$Re_x$	$U x/\nu$ = Reynolds number at distance $x$
$\nu$	kinematic viscosity at altitude ( $ft^2/sec$ )
$m$	modal mass (slugs)
$E$	Young's modulus ( $lbs/in^2$ )
$I$	plate moment of inertia ( $bt^3/12$ )
$t$	plate thickness (inches)
$L$	length of aircraft fuselage (inches)
$\lambda$	length of first bending mode, secondary structure (inches)
$f_c$	center frequency of transfer functions for equipment categories and of special functions



SYMBOLS (CONTINUED)

$D_f$	nominal fuselage diameter at $x = x_E$ (inches)
$L_M(f)$	maximum value of low frequency transfer function, first bending mode (dB)
$L_2(f)_M$	maximum value of low frequency transfer function, second bending mode (dB)

## SECTION I

### INTRODUCTION

From the equipment design and the functional test and analysis viewpoint, it is important that the predicted vibration spectra of fighter aircraft equipments emulate the real vibration histories as closely as the forecasting technology will allow. To do this, it is necessary to be able to portray the variform vibration spectra as the aircraft cycles through a variety of flight conditions, attitudes, and phases that, when seen in terms of their sequential assembly, constitutes a vibrational representation of the mission flight profile. Spectral fidelity is important not only from the viewpoint of the reversible<sup>\*</sup>, functional failure -- a failure that underlines the interrelationship between the vibration spectral details and the concomittant equipment malfunction -- its importance is stressed again when vibration test inputs are chosen for the long-time test spectra associated with various reliability test philosophies. Here, premature fatigue failure often results because the vibration test spectrum exceeds the in situ spectrum; or more explicitly, fails to adequately mirror the real vibration environment relative to the spectral details, and to the real time of exposure.

#### 1.0 Approach

The detailed development of the vibration prediction method utilized in this program is found in Reference 1. However, for review purposes, it is useful to briefly survey major elements of the technique.

---

\* change the spectrum and the equipment resumes operation

### 1.1 Fuselage Vibration Behavior

The aircraft fuselage response is subdivided into three regimes: the low frequency region, dominated by the fuselage body bending modes; the medium frequency region, determined by the response of the internal structure; and the high frequency domain, which is established by the aircraft skin contributions. Three transfer functions  $L(f)$ ,  $M(f)$ , and  $H(f)$  are assigned to these regions: low, medium, and high, respectively.

The boundary layer pressure spectral density  $P(f)$  is transferred through  $L(f)$ ,  $M(f)$ , and  $H(f)$  to produce a structural response spectrum,  $G(f)$ , which, in turn, is attenuated and further transformed by other functions as one progresses into the aircraft interior.  $P(f)$  and the three transfer functions are variants of the same basic function, the derivation of which is developed fully in Section II. Other special variants of this same function are employed to account for a variety of equipment mounting methods. A further variation is invoked to simulate a number of aircraft phases and maneuvers -- all are discussed in Section III and all are detailed in their applicable Appendices. Section III describes the computer program and its operating procedures, taken from the viewpoint of the user. Section IV demonstrates the applications of the prediction method and the program as it is applied to a number of aircraft equipment mounting methods and flight conditions. Appendix F contains the complete computer program in FORTRAN IV.

## SECTION II

### FLEX FUNCTION

#### 1.0 Derivation

A rather detailed discussion of the flex function and its derivation is found in reference 1. But since we intend to expand on the earlier work and, moreover, since the function operates as the central mechanism of the computer program, a review of the main elements is essential.

Consider the following function and its mirror image:

$$\theta = \arctan A \quad (1)$$

$$\theta = \pi - \arctan A \quad (2)$$

where:  $\theta$  = angle (rads)

$$A = 2\beta(\omega/\omega_o)/1-(\omega/\omega_o)^2$$

$\omega$  = angular frequency (rads/Hz)

$\omega_o, \omega_o'$  = locator frequency (rads/Hz)

$\beta, \beta'$  = slope factor

Equations (1) and (2) combine graphically to form a bandpass characteristic (Figure 1a). Equation (1) describes the low frequency roll-off; equation (2) the high frequency roll-off. Note that in this form, frequency translation occurs by control of  $\omega_o(\omega_o')$ . Slope control is readily obtained by adjustment of  $\beta(\beta')$ . These flexible



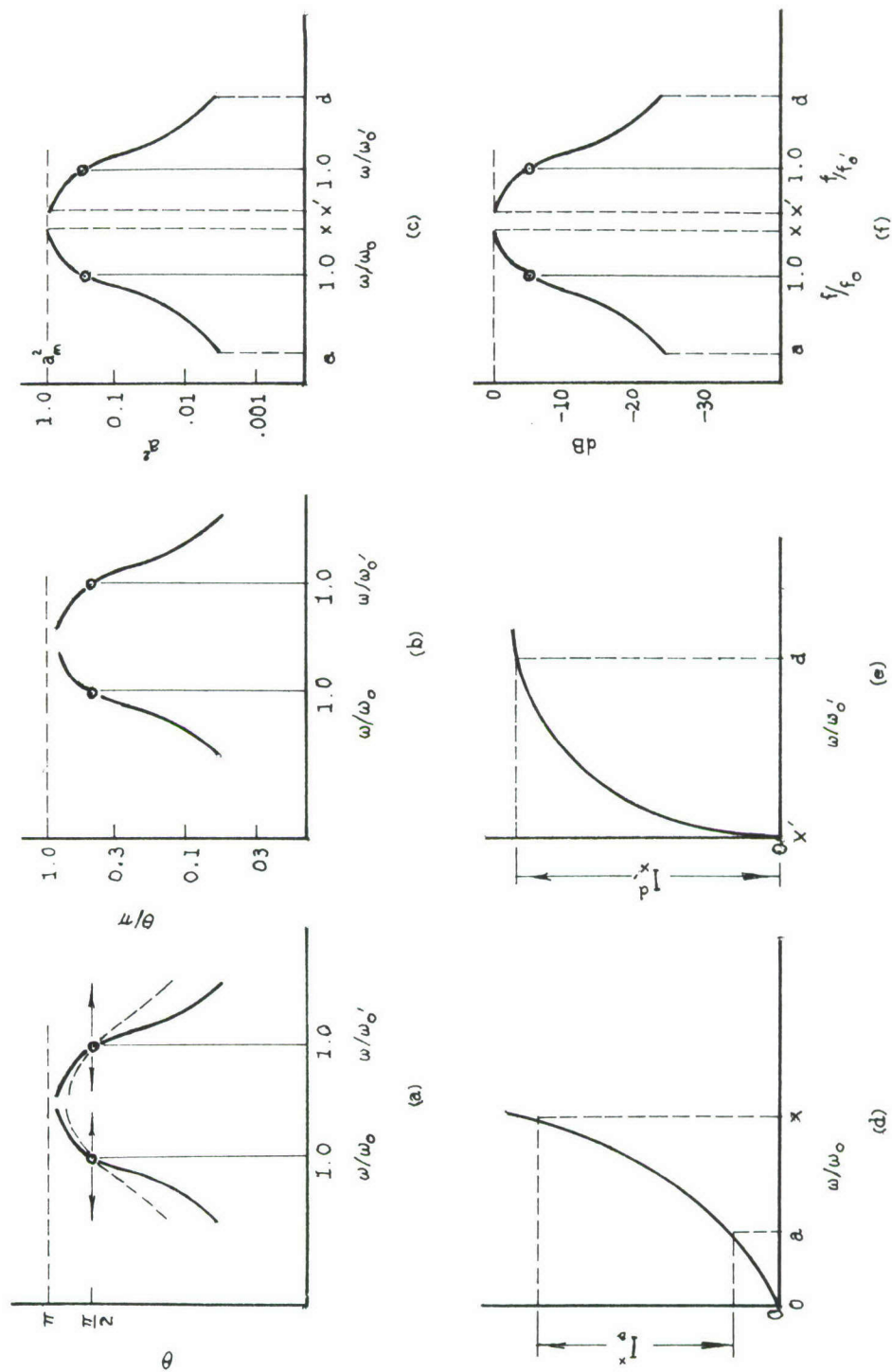


Figure 1. Derivation of the Flex Function and Associated Integral

and useful properties, by which response functions may be described using only four notations, will become more obvious a little later on.

### 1.1 Further Adjustments

However, there remains an objection to the curve in this form owing to the asymptotic properties of the function. That is,  $\omega/\omega_0$  must approach infinity in order that  $\theta \rightarrow \pi$ . Since  $\pi$  represents the curve maxima, and it is the maxima that we intend to reference when utilizing the functions, we must readjust the curves vertically to obtain a value of  $\theta = \pi$  at a real, finite value of  $\omega/\omega_0$ . This we do as follows:

$$\theta/\theta_x = (\arctan A)/\theta_x \quad (3)$$

$$\theta/\theta_{x'} = (\pi - \arctan A)/\theta_{x'} \quad (4)$$

$$\text{where: } \theta_x = \arctan [2\beta x / 1 - (x)^2]$$

$$\text{and: } \theta_{x'} = \pi - \arctan [2\beta' x' / 1 - (x')^2]$$

The curves are now shown as Figure 1(b) and appear in normalized form, that is, the maximum value is unity at  $\theta = \theta_x$  and  $\theta = \theta_{x'}$ .

We may let the functions represent a pertinent variable, say acceleration (a), by the following substitutions.

$$\text{Let: } \theta/\theta_x = K a$$

$$\text{and: } a = 1/K(\arctan A)/\theta_x \quad (5)$$

$$\text{where: } (\arctan A)/\theta_x = g(\omega/\omega_0)$$

when:  $\omega = x\omega_o$ , then  $g(x) = 1.0$

and  $a = a_{\max}$

From inspection of (5),  $1/K = a_{\max}$ . If we substitute this into (5), we have a generalized form for the independent variable,  $a$ :

$$a = a_{\max} [(\arctan A)/\theta_x] \quad (6)$$

$$0 \leq \omega/\omega_o \leq x$$

Operating similarly for the high frequency roll-off portion of the flex function we have:

$$a = a_{\max} [(\pi - \arctan A)/\theta_{x'}] \quad (7)$$

$$x' \leq \omega/\omega_o$$

A good deal of the time we will be concerned with mean squared values of the acceleration and the acceleration power spectral densities. Thus, (6) and (7) may be squared as follows:

$$a^2 = a_{\max}^2 [(\arctan A)/\theta_x]^2 \quad (8)$$

$$a^2 = a_{\max}^2 [(\pi - \arctan A)/\theta_{x'}]^2 \quad (9)$$

The squared curves are shown in Figure 1(c). When using power spectral densities, we will also be concerned with overall mean squared acceleration, thus the integrals of (8) and (9) appear as follows:

$$I_a^x = a_{\max}^2 \int_a^x [(\arctan A)/\theta_x]^2 d(\omega/\omega_o) \quad (10)$$

$$I_a^{x'} = a_{\max}^2 \int_c^{x'} [(\pi - \arctan A)/\theta_{x'}]^2 d(\omega/\omega_o) \quad (11)$$

Figures 1(d) and (e) show the integrals of the low and high frequency curves, respectively. And since most of the time we will use the log of the independent variable  $a^2$  (referred to  $a_{\max}^2$ ) we present (8) and (9) as follows:

$$dB = 10 \log_{10} [(\arctan A)/\theta_x]^2 \quad (12)$$

$$dB = 10 \log_{10} [(\pi - \arctan A)/\theta_{x'}]^2 \quad (13)$$

Also, since we will be using hertz for the frequency variable, we substitute  $f$  in lieu of  $\omega$  and  $180^\circ$  for  $\pi$ . The final set of curves are shown in Figure 1(f).

## 2.0 Flex Function Display

Values of  $x$  and  $x'$  were chosen for the low and high frequency functions as were values of  $\beta$  and  $\beta'$ . Since  $x$  and  $x'$  represent the frequency ratios of the low and high frequency function at which normalization of the ordinate value occurs, they are identified, in truncated computerese, as NORM. FREQ. Both parametrics were selected to cover the range of vibration spectra that one associates with the primary structure of aircraft viewed over a wide range of structural locations and flight conditions. Figures 2 and 3 show a typical low and high frequency curve for  $x = \text{NORM. FREQ.} = 2.00$  and  $x' = \text{NORM. FREQ.} = 0.500$ , respectively. The  $\beta(\beta')$  parameters are shown also on the figures as curve families having  $\beta$  and  $\beta'$  in the following graduations: 0.1, 0.2, 0.4, 0.6, 0.8 and 1.0.



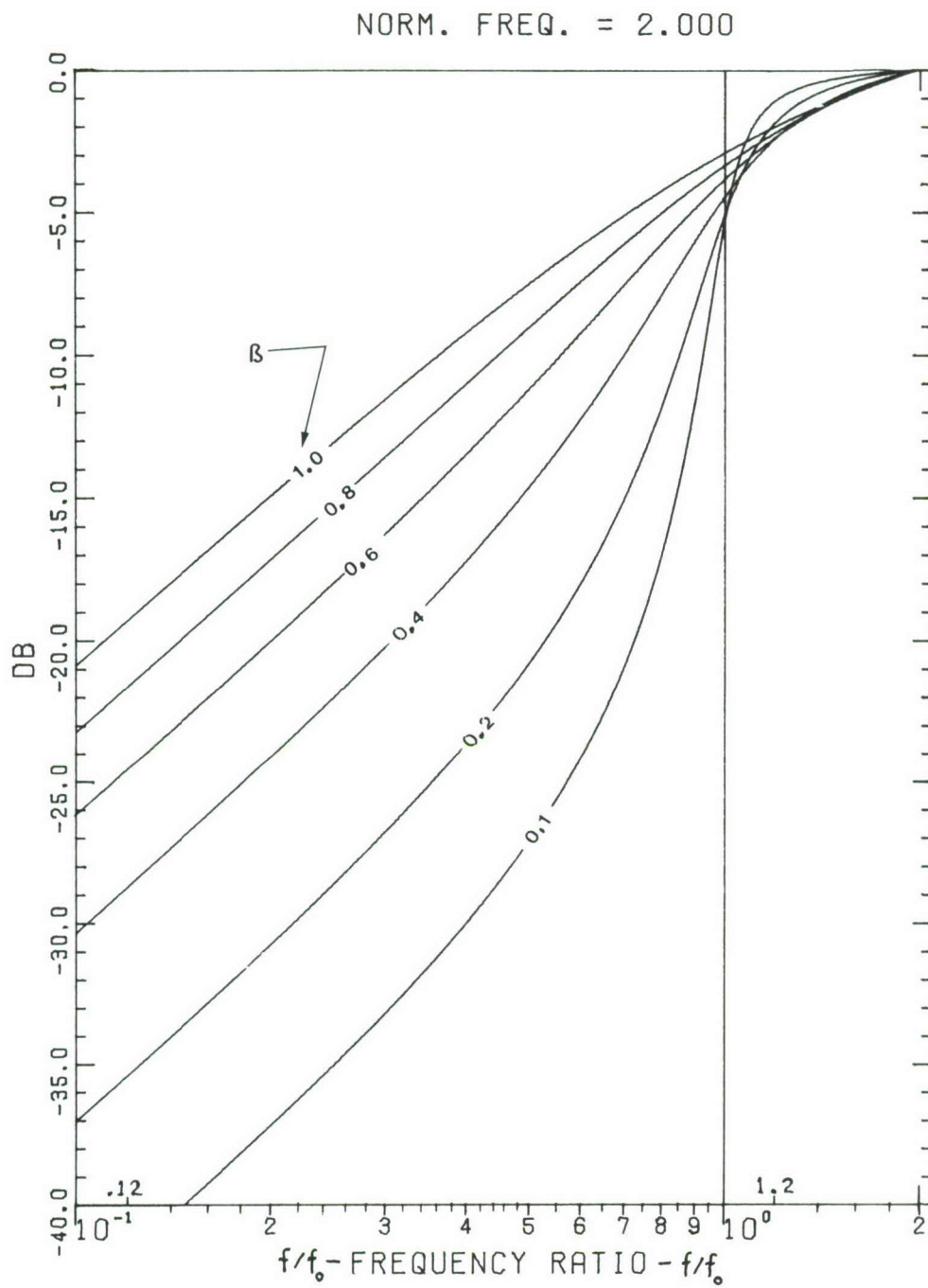


Figure 2. Typical Flex Function for Low Frequency Rolloff

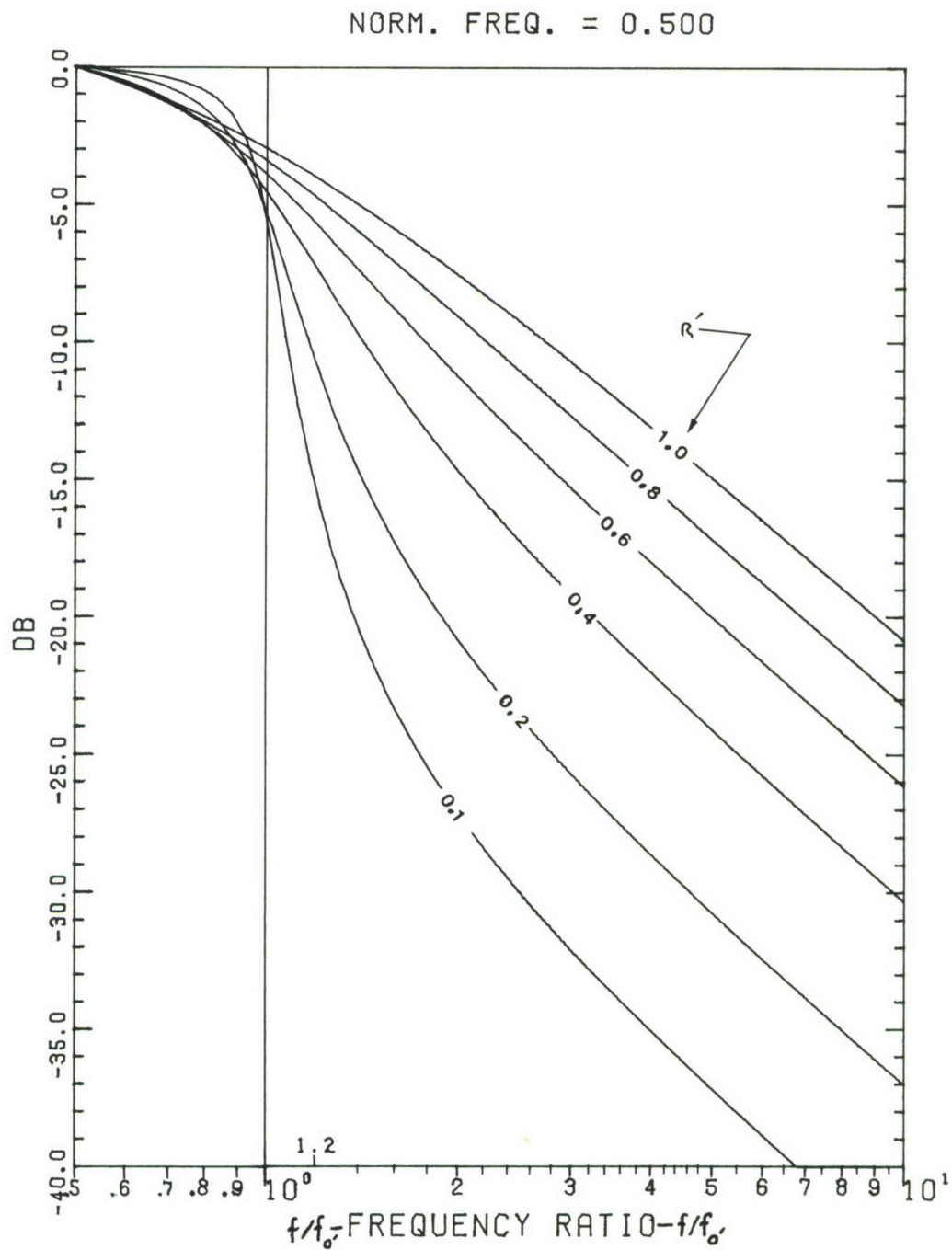


Figure 3. Typical Flex Function for High Frequency Rolloff

## 2.1 Low Frequency Boost

If we examine the arctan portion of, say, equation (1), we note that the numerator is of the form  $2\beta(\omega/\omega_0)^\alpha$ , where  $\alpha = 1$  for the functions represented by Figures 2 and 3. However, by allowing  $\alpha$  to go to zero a novel but useful low frequency pre-emphasis results (Figure 4). In short, the curves (in the low frequencies) are raised; given bass boost, as the audiophiles are fond of saying. Such a phenomena corresponds to what happens to the aircraft vibration spectra as the aircraft passes through certain stages of its flight profile -- for example, during taxi, takeoff roll, the dumping of speed brakes, or flaps; and during gunfire or inflight refueling phases. Note that we may make  $\alpha$  a function of time and, operating within the limits of  $\alpha = 1$  and  $\alpha = 0$ , we are able, in a gradual, continuous, and reversible way, to effect the smooth transition from one state to the other. This property is of significance when we view the function as a programmable system capable of describing a useful variety of flight vibration phases.

Notice that identical variations can be reflected into the high frequency rolloff curve (equation 13) by assigning an  $\alpha'$  within the interval of 1 and 2. Figure 5 shows a set of functions for  $\alpha' = 2.00$ . From here on out, alpha will follow the same diacritic symbolism as has been assigned to the other high and low frequency rolloff parameters. Thus,  $\alpha$  is assigned to the low frequency rolloff equation and  $\alpha'$  refers to the exponent for the high frequency rolloff case. Also, note that unless  $\alpha$  and  $\alpha'$  are specifically stated, their values are always presumed to be unity.

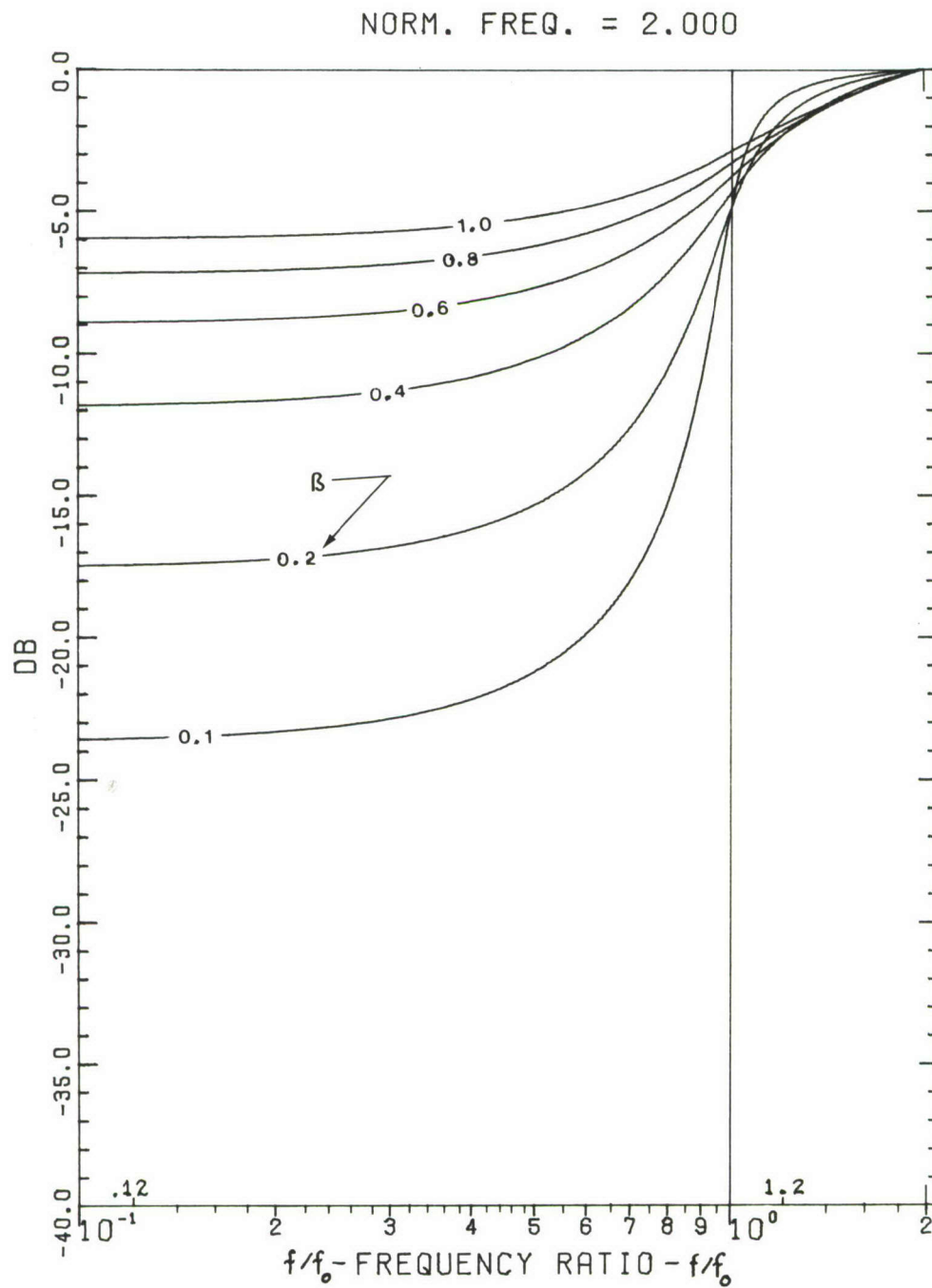


Figure 4. Flex Function with Low Frequency Boost



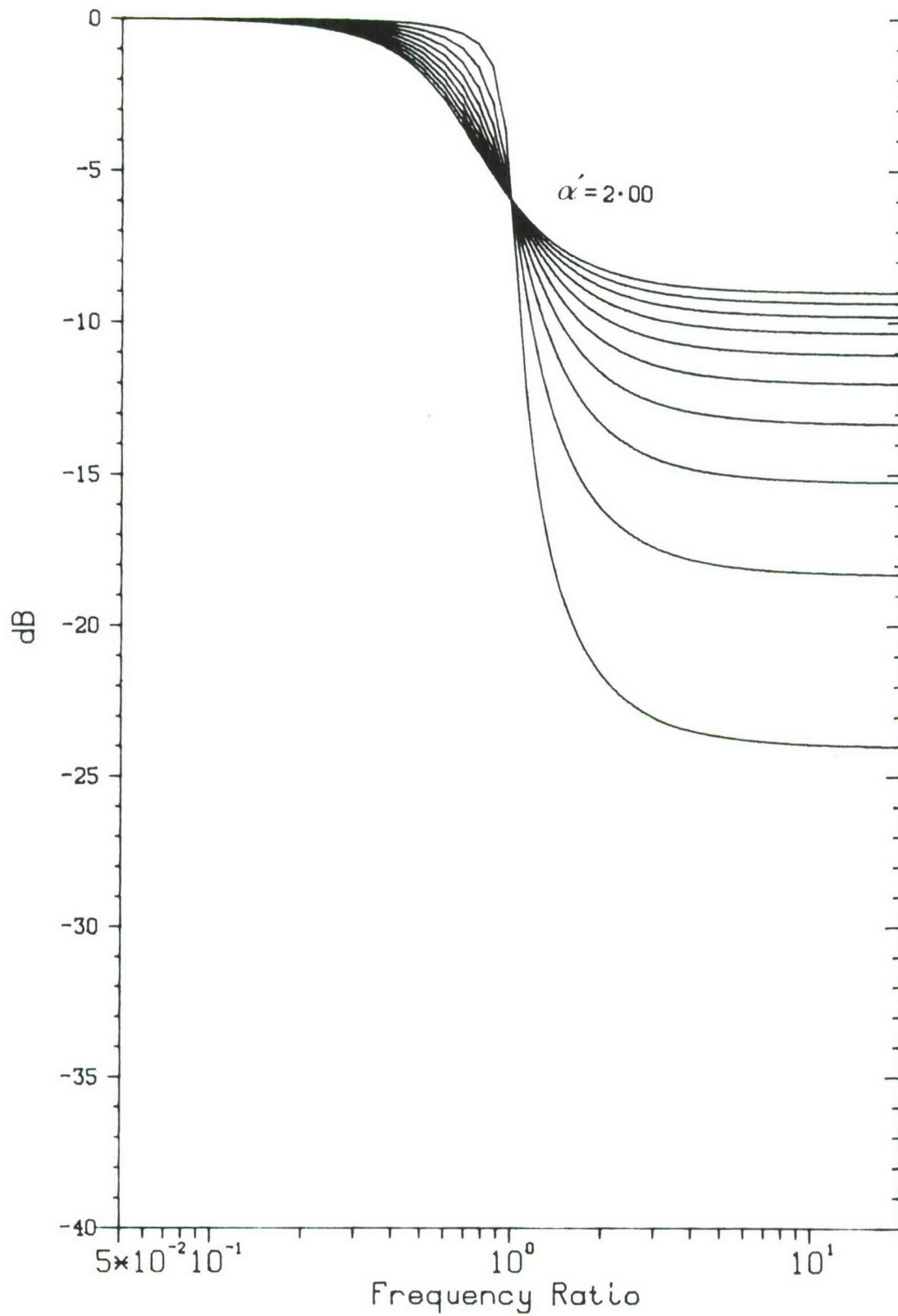


Figure 5. Flex Function with High Frequency Boost

## 2.2 Boundary Layer Spectra

If we choose  $x' = .01$  for the high frequency rolloff function we will obtain a form characterized by a relatively expansive, flat spectrum in the lower frequency part of the curve. Moreover, if we select somewhat different values of  $\beta'$  (0.2, 0.3, 0.4, 0.6, 0.8, 1.0, 1.5) we will have defined a family of curves that will serve to provide a good fit for the pressure spectral density of the boundary layer for a large number of aircraft flight conditions. The boundary layer curves are shown as Figure 6.

## 3.0 Prediction Equations

The flex function is broken out into the forms and relationships to be used in the computer program. First, the equations are stated in order of progression.

$$P(f) [\phi_n(x)L(f), M(f), H(f)] = G(f) \quad (14)$$

where:

- $P(f)$  = the boundary layer pressure spectral density at some downstream distance ( $x$ ) on the aircraft surface.
- $\phi_n(x)L(f)$  = the product of the bending mode shape,  $\phi_n(x)$ , at downstream distance,  $x$ , and the low frequency transfer function,  $L(f)$ , of the aircraft fuselage.
- $M(f)$  = the medium frequency transfer function of the aircraft fuselage internal structure.
- $H(f)$  = the high frequency transfer function of the fuselage skin.
- $G(f)$  = the PSD response of the aircraft primary structure ( $g^2/Hz$ ).

NORM. FREQ. = 0.010

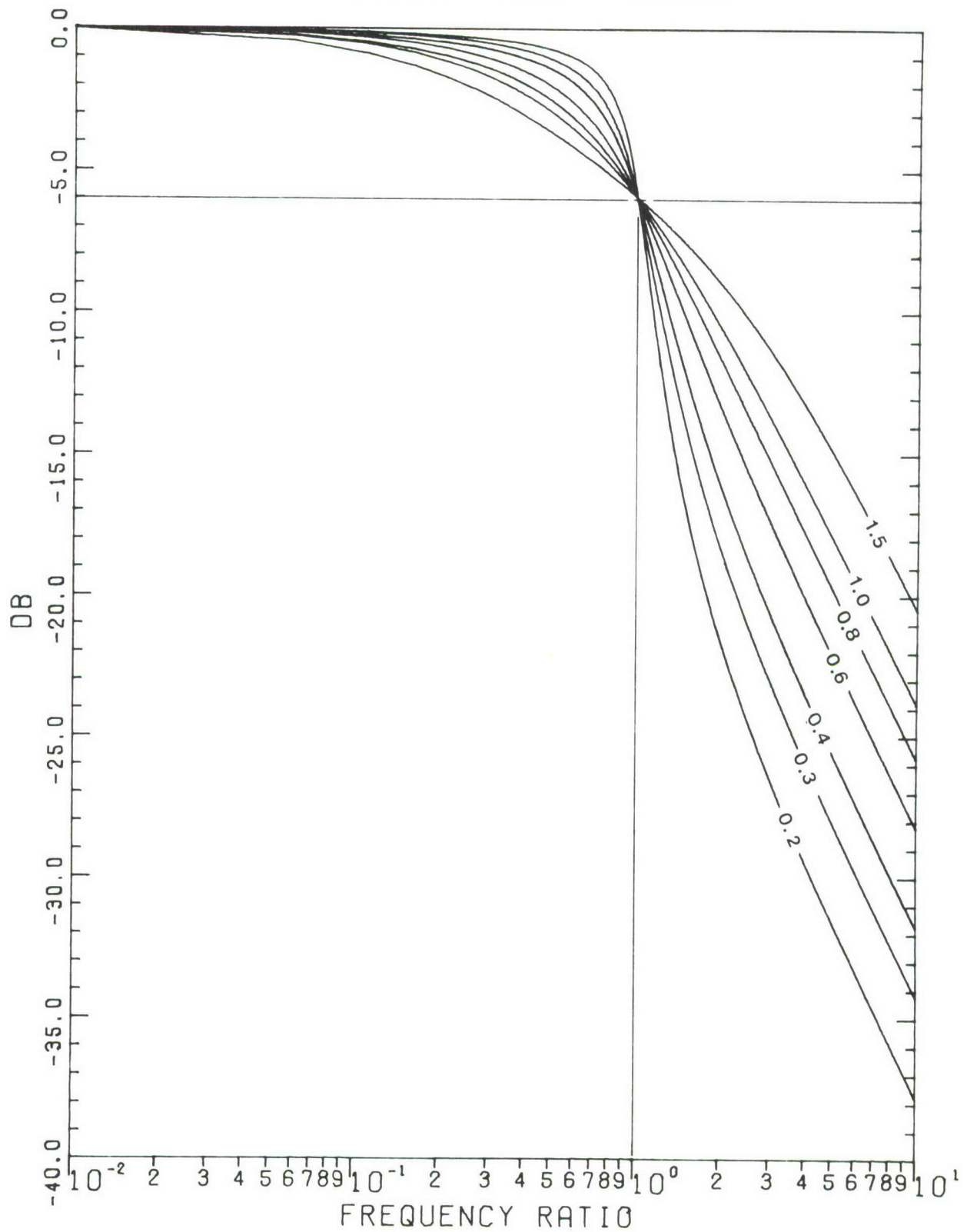


Figure 6. Flex Function Applied to the Aircraft Boundary Layer

The term, primary structure, is defined as that structure of the aircraft which comprises the main load carrying members or elements of the aircraft. Examples of primary structure are skin, frames, rings, bulkheads (periphery), stringers and includes those consoles structurally integrated with the aircraft outer walls.

The working forms for  $P(f)$  are described in Appendix A and are listed as equations A-1, A-2, A-3, and A-4.

The mode shape,  $\phi_n(x)$ , is a function of aircraft type and is included in Appendix B for typical aircraft. The aircraft structural transfer functions  $L(f)$ ,  $M(f)$ , and  $H(f)$  are listed in Appendix C together with appropriate tables.

### 3.1 Special Functions

Certain flight phases, that deviate from the straight and level condition, are introduced by operating on  $P(f)$  with special functions designated,  $S(f)$ .

$$P(f)S_{BT}(f) = P_{BT}(f) \quad (15)$$

$$P(f)S_{TB}(f) = P_{TB}(f) \quad (16)$$

$$P(f)S_T(f) = P_T(f) \quad (17)$$

$$P(f)S_L(f) = P_L(f) \quad (18)$$

where:

$S_{BT}(f)$  = Special function for the buffet turn flight phase.

$P_{BT}(f)$  = Pressure spectral density spectrum of a fighter aircraft during buffet turn ( $\text{PSF}^2/\text{Hz}$ ).



- $S_T(f)$  = Special function for the takeoff phase.  
 $P_T(f)$  = Equivalent pressure spectral density spectrum of an aircraft during the takeoff phase ( $\text{PSF}^2/\text{Hz}$ ).  
 $S_L(f)$  = Special function of an aircraft during the landing phase.  
 $P_L(f)$  = Equivalent pressure spectral density spectrum of an aircraft during the landing phase ( $\text{PSF}^2/\text{Hz}$ ).  
 $S_{TB}(f)$  = Special function for low frequency atmospheric turbulence.

These special functions together with their appropriate tables, curves, and explanations are found in Appendix D.

The second set of basic equations is as follows:

$$G(f) Y(f) = R(f) \quad (19)$$

where:

- $Y(f)$  = the transfer function for equipments mounted on secondary structure.  
 $R(f)$  = the PSD response of the secondary structure, or the input to the aircraft equipment, mounted thereon ( $g^2/\text{Hz}$ ).

Secondary structure is defined as that structure to which equipment is attached onto or contained in and whose mounting points terminate at the outer frame, skin, stringers, bulkheads, floors, spars or cast framing of the primary structure. Examples of secondary structure are instrument panels, trays, racks, brackets, shelves, trusses, beams, and consoles.

The final equations apply to those equipment mounting configurations in which isolated equipment are mounted on secondary structure:

$$R(f) Y_{I(a)}(f) = a(f) \quad (20)$$

where:

$a(f)$  = The response of the isolated equipments ( $g^2/Hz$ ).

$Y_{I(a)}(f)$  = Transfer function for equipment mounted on isolators.

$R(f)$  = Response of secondary<sub>2</sub> structure (instrument panels, shelves, or racks) ( $g^2/Hz$ ).

### 3.2 Equipment Mounting Categories

How and when  $G(f)$ ,  $Y(f)$ , and  $a(f)$  are used depends upon what, how, and where the equipment is mounted in the aircraft -- and this is established by reference to equipment mounting categories and their associated transfer functions which are classified as follows:

#### Category I - Equipment(s) attached to primary structure

- a. Isolated. Equipment(s) attached to primary structure through vibration isolators.
- b. Non-Isolated. Equipment(s) directly attached to primary structure.

#### Category II - Equipment attached to instrument panels

- a. Isolated. Equipment(s) whose instrument panel is attached to primary structure through vibration isolators.
- b. Non-Isolated. Equipment(s) whose instrument panel is directly attached to primary structure.

#### Category III - Equipment(s) mounted on shelves or in racks

- a. Isolated. Equipment(s) attached to shelves or in racks - with shelf or rack isolated.

- b. Non-Isolated. Equipment(s) attached to shelves or racks -  
with shelf or rack non-isolated.

Category IV - Equipment(s) that is isolated and mounted on shelves  
or in racks.

- a. Category III(a) with equipment(s) isolated.
- b. Category III(b) with equipment(s) isolated.

Category V - Lightweight equipment items directly attached to pri-  
mary structure via light bracketry.

Category VI - Equipment(s) mounted to or on the bulkhead of the for-  
ward looking radar (FLR).

The categories of transfer functions, their tables, curves,  
and applications are found in Appendix E.

## SECTION III

## PROGRAMMING

The equations shown in Paragraph 3 of Section II for predicting power spectral density inputs to aircraft equipment are laborious to evaluate - given many selected frequencies over a relatively wide band. And, even though these equations are few in number and are not of themselves complex, a digital computer program was, nonetheless, strongly suggested. Such a program, therefore, was prepared to evaluate the prediction equations at a frequency resolution sufficiently fine to produce quality plots and in the combinations and sequences required by the particular set of input data which describes the aircraft flight profile.

Conceptually, the program is so designed that a minimum of information on flight conditions is required as input for predicting the vibration profiles of the aircraft structure and equipments. The input data consists, chiefly, of numerical values and descriptive information concerning such flight parameters as aircraft type, altitude, Mach number, equipment weight, mounting categories, and flight maneuvers.

For output, the values of the particular transfer and response functions, which were a part of the prediction process, are printed in tabular form and presented as a function of frequency. If desired, plots of these results can be produced on peripheral plotters.

## 1.0 Program

The program consists of a relatively large main section which, in its operation, "calls" approximately a dozen subroutines. The structure is simple.

## 2.0 Program Preparation

The program is prepared for execution by first punching numerical and alpha-numeric descriptive information for key aircraft and flight profile parameters on cards, in specified field locations; then inserting these cards in the program deck at its end.

### 2.1 Execution

On program execution, tabulations of the input, the transfer and the response functions are printed (dB as a function of frequency). The information necessary for producing plots of these tabulated values is transferred in a device-independent, standard form from central memory to a permanent file located in mass storage.

In the final step, plots of all or selected transfer functions are obtained by executing a small post-processor program containing a plot-directive card which is inserted by the user. This program provides for transfer of the plot information from the permanent file to central memory and also provides a "write", on magnetic tape, of information necessary for a plot of each of the functions specified on the plot-directive card. This tape is mounted on a CALCOMP plotter to produce the plots.



Before we proceed to the program deck card order -- the plot, the keyboard instructions, and, finally, the card preparation -- it is useful to note that the basic language and format of the program (Appendix F) is Fortran IV and as such may be readily adapted to other computer facilities. However, certain address characteristics of the card arrays, the plotting, the display instructions reflect the needs of the individual computer facility; and the demands of its terminals. In this report, the ASD Computer Facility and Terminals are invoked -- elsewhere, the reader is invited to consult local computer services.

## 2.2 Functions<sup>\*</sup> Available for Plotting

	<u>Categories Ia, IIa, IIb, IIIa, IIIb, V, VI</u>
Straight and Level	$P(f), G(f), Y(f), R(f)$
Buffet-Turn	$P_{BT}(f), G_{BT}(f), Y(f), R_{BT}(f)$
Takeoff	$P_T(f), G_T(f), Y(f), R_T(f)$
Landing	$P_L(f), G_L(f), Y(f), R_L(f)$
Turbulence	$P_{TB}(f), G_{TB}(f), Y(f), R_{TB}(f)$
	<u>Categories IVa and IVb</u>
Straight and Level	$P(f), G(f), Y(f), R(f), Y_{1A}(f), A(f)$
Buffet-Turn	$P_{BT}(f), G_{BT}(f), Y(f), R_{BT}(f), Y_{1A}(f), A_{BT}(f)$
Takeoff	$P_T(f), G_T(f), Y(f), R_T(f), Y_{1A}(f), A_T(f)$
Landing	$P_L(f), G_L(f), Y(f), R_L(f), Y_{1A}(f), A_L(f)$
Turbulence	$P_{TB}(f), G_{TB}(f), Y(f), R_{TB}(f), Y_{1A}(f), A_{TB}(f)$

\* See Appendices D and E

	<u>Category Ib</u>
Straight and Level	$P(f)$ , $G(f)$
Buffet-Turn	$P_{BT}(f)$ , $G_{BT}(f)$
Takeoff	$P_T(f)$ , $G_T(f)$
Landing	$P_L(f)$ , $G_L(f)$
Turbulence	$P_{TB}(f)$ , $G_{TB}(f)$

Execution is essentially sequential -- the only important branch is a loop from the program end back to the beginning in order to repeat the process whenever the aircraft flight parameters change. All other branches terminate at nearby statements.

Transfer and response functions can be plotted on a CALCOMP (incremental) plotter. Calls are made to selected subroutines in the DISSPLA<sup>\*</sup> software system for the desired data display.

Salient features of program design are summarized below.

Language:	FORTRAN IV
Digital Computer:	Control Data Corp., 6600 and Cyber 73 computers
Central Memory Requirements:	120,000 (octal) words for compiler; program, and plot subroutines
Word Size:	10 characters
Variable Name Size:	6 characters, maximum
Input Data:	Punched on 80-column cards

---

\* The acronym for "Display Integrated Software System, and Plotting Language," developed and sold by the Integrated Software Systems Corp., San Diego, CA.

Output: 135-column printed tabulations and  
off-line plots

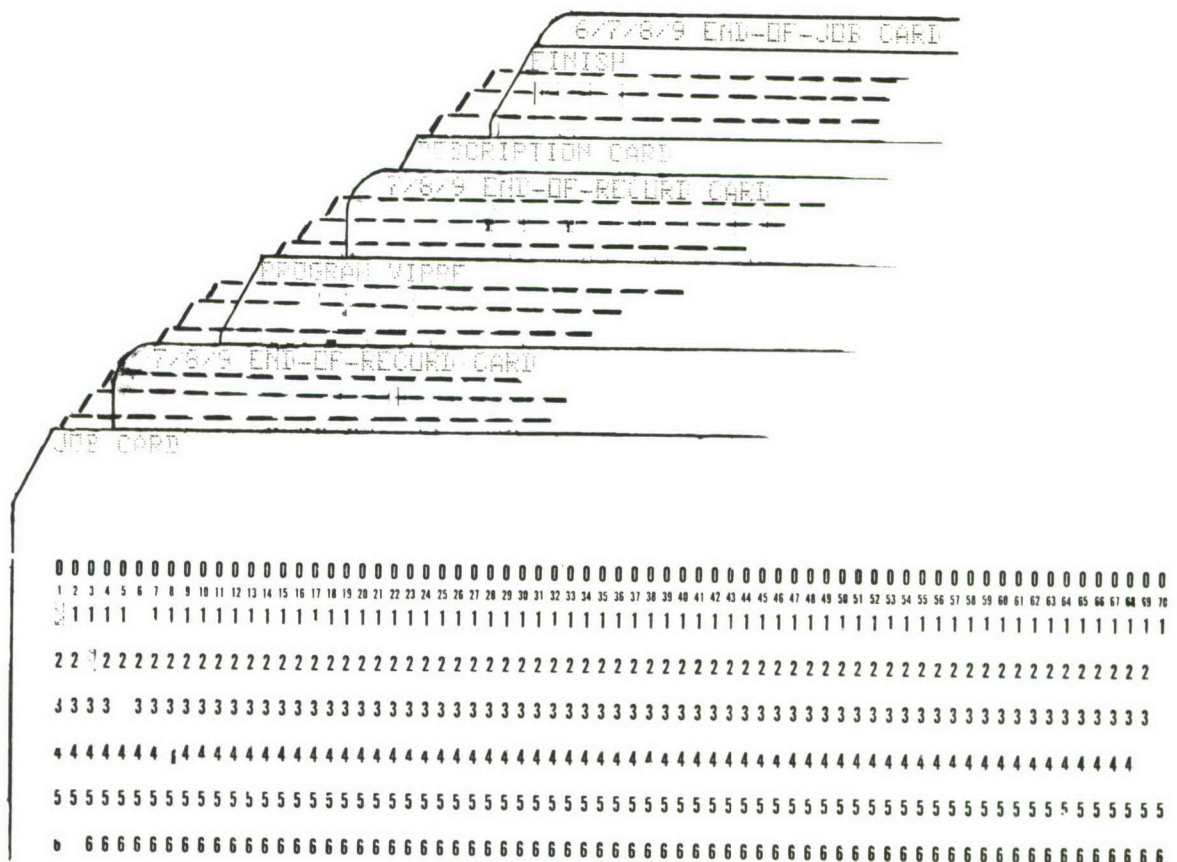
Library Mathe-  
 matical Functions: Common logarithm and arc-tangent  
 (double argument)

### 3.0 Program Deck Setup and Card Preparation

### 3.1 Job Deck Setup

The first step in the procedure to obtain plots of the predicted vibration spectra requires the execution of the program, VIPRF. Upon execution, a printed output is produced; likewise, the plot information is transferred to a permanent file.

The following illustration shows the structure of the card deck setup for program execution.



The second and final step in the procedure involves execution of either the ONLINE or the OFFLINE, DISSPLA, post-processor plot program. In this phase, plot information is obtained from the permanent file (previously generated); then, plots are produced either on-line or off-line, in this case, utilizing a CALCOMP plotter.

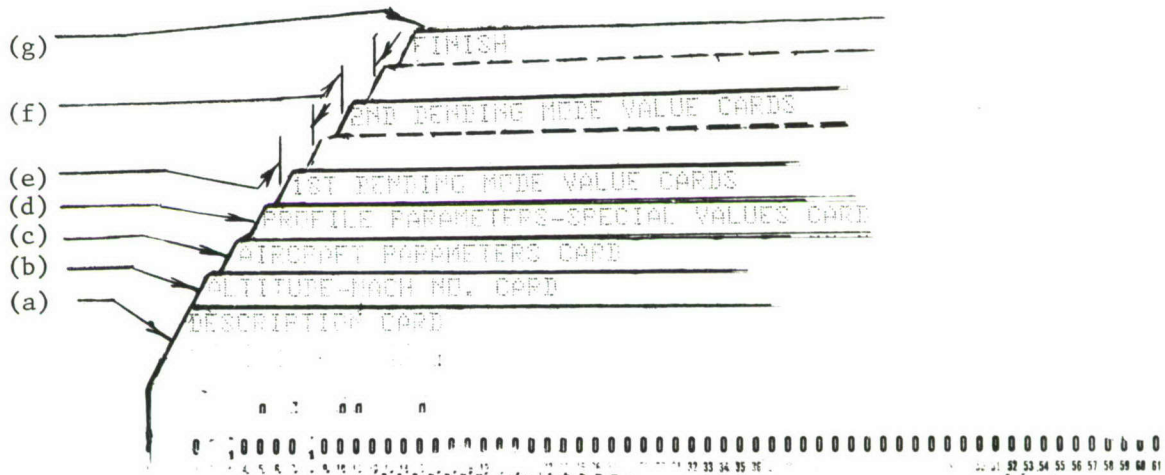
The structure of the deck setup is shown in the following illustration.





### 3.1.1 Input Data Deck Setup

Program input data is entered on the cards shown in the next illustration. Note that the cards must be inserted in the deck in the indicated order.



The Description, the Altitude-Mach Number, and the Aircraft Parameter cards must always be prepared and inserted in the deck.

The Profile Parameters and Special Values cards must always be inserted. If the values are already stored in the program (as is, currently, the case for the F-4, F-15, F-16, F-111, and the A-7), then a blank card must be inserted. Any profile parameter or special value can be changed, however, by entering the desired value on the normally blank card. This feature permits the user to "write over" the stored values as the situation requires. If an aircraft different from the stored group is chosen, then a Profile Parameters and Special Values card must be inserted with appropriate entries. Note that in either case, a card must be inserted, blank or not.

The procedural mechanics are more complex when dealing with the first and second bending mode value cards. Here, the combination of orders of proper card usage are such that special guidance must be provided in the form of a summary aid and a table, both of which now follow.

#### 3.1.1.1 Summary of Input Data Card Structure

We return to the last illustration to summarize the rules of order and procedure concerning the card structure of the input data. The summary also makes reference to special guidance in the form of Table I.



<u>Cards</u>	<u>Remarks</u>
a,b,c	These cards must always be prepared and inserted in the deck.
d	A blank card is normally inserted in the deck if aircraft is of the previously stored group (see 3.1.1). Stored values may be written-over by inserting desired values on the blank card. For aircraft not of the stored group, enter appropriate values on the blank card (see Table I).
e,f	Both card sets are normally omitted if the aircraft is of the previously stored group; however, if data changes are required, see Table I.
g	The FINISH card must always be inserted at the end of a set of data cards.

TABLE I  
Card Usage Guidance -- Bending Mode Data

1st Mode		2nd Mode			Insert Cards:	Special Entries In Card (d)
Stored Data Cards	Read From Input Data Cards	Stored Data Cards	Read From External Input Data Cards	Unavailable		
X		X			(a) thru (d) followed by (g)	enter $f_{2n}=0$
X			X	X	(a) thru (d) followed by (g)	
X					(a) thru (d) followed by a blank card, followed by a set of 2nd bending mode cards (f); followed by (g)	
	X	X			(a) thru (d) followed by a set of 1st bending mode cards (e); followed by (g)	enter $f_{2n}=0$
	X			X	(a) thru (d) followed by a set of 1st bending mode cards (e); followed by (g)	

### 3.1.2 Card Preparation for Input Data

Each card example is shown in proper sequence, selected and punched with the input data for the program. Included are column identifications, associated nomenclature, and explanatory references.

#### 3.1.2.1 DESCRIPTION Card

[illegible]Aircraft Type

COL. 10    Aircraft Type (center aircraft designation in 10-column field to obtain centering plot titles)

Note that the following aircraft types occupy a specific columnar order because certain of their values (Profile Parameters and Special Values; First and Second Bending Mode values) have been previously stored in the program.

COL. 4-6 F-4 }  
 4-7 F-15 }  
 4-7 F-16 } Enter on card exactly as specified here.  
 4-8 F-111 }  
 4-7 A-7D }

This order requirement also holds for any future aircraft, so stored. For example, the A-10 would occupy columns 4 through 7.

### Equipment Description

COL. 11-30 Name of equipment item or location (center name in 20-column field to obtain centering in plot titles)

### Flight Condition

COL. 31-35 SANDL, straight and level

COL. 31-32 BT, buffet-turn\* (see Appendix D)

COL. 31-37 TAKEOFF, takeoff (see Appendix D)

COL. 31-37 LANDING, landing (see Appendix D)

COL. 31-32 TB, turbulence\* (see Appendix D)

\*Requires a straight and level reference flight condition that must be entered in the Altitude-Mach Number card (see 3.1.2.2).

### Plot Selection

COL. 41-50 Leave all columns blank if only the plot of the final response function is desired [ $G(f)$ ,  $R(f)$ , or  $A(f)$ ].

COL. 41-43 Enter ALL, if plots of all of the special, transfer, and response functions are desired.

### 3.1.2.2 Altitude-Mach Number Card

2000.		.77																																																					
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0				
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1				

COL. 1-8 Altitude, H, feet, of 1st altitude-mach number combination.

COL. 9-13 Mach no., M, of 1st altitude-mach number combination.

COL. 14-21 Altitude, H, feet, of 2nd altitude-mach number combination.

COL. 22-26 Mach no., M, of 2nd altitude-mach number combination.

COL. 27-34 Altitude, H, feet, of 3rd altitude-mach number combination.

COL. 35-39 Mach No., M, of 3rd altitude-mach number combination.

COL. 40-47 Altitude, H, feet, of 4th altitude-mach number combination.

COL. 48-52 Mach no., M, of 4th altitude-mach number combination.

COL. 53-60 Altitude, H, feet, of 5th altitude-mach number combination.

[illegible]

Center Frequency,  $f_c$ , of Transfer Function,  $Y(f)$

COL. 51-60      Center frequency of specified category,  $f_c$ , (Hz)  
 (leave blank if unknown).

COL. 61-70      Blank.

30



If Category is IVa or IVb\*

COL. 51-60	Center frequency for Category Ia, $f_{cIA}$ (Hz) (leave blank if unknown).
COL. 61-70	Center frequency, $f_c$ (Hz) for Category IIIa, if Category IVa is specified; Category IIIb, if Category IVb is specified (leave blank if unknown).
COL. 71	<u>Skin material</u> A for aluminum T for titanium S for steel M for magnesium

TABLE II

Recommended Center Frequencies of  
 $Y(f)$  When  $f_c$  is Either Unknown or Unspecified

<u>Category</u>	<u><math>f_c</math></u>
Ia	25 Hz
IIa	43 Hz
IIb	40 Hz
IIIa	25 Hz
IIIb	35 Hz
V	200 Hz

\*For selection guidance, see Table II. Also, note that Category I(b) has a transfer function (previously built into the program) that is automatically invoked when I(b) is selected (see Figure E-1(b)).



- COL. 61-70 Distance to main landing gear strut,  $x_T$  or  $x_L$  (feet)  
(see Appendix D).
- COL. 71-80 Multiplication constant, K. Unless otherwise specified,  
K=1 (leave blank if straight-and-level flight condition  
(SANDL) is specified).

### 3.1.2.5 FIRST BENDING MODE VALUES Cards

#### Card 1

- COL. 1-2 No. of ordinal (dB) values, N
- COL. 3-8 Interval,  $\Delta x$ , along abscissa
- COL. 9-14 Value 1, db
- COL. 15-20 Value 2, db
- COL. 75-80 Value 12, db

#### Card 2

- COL. 1-6 Value 13, db
- COL. 7-12 Value 14, db
- COL. 73-78 Value 25, db

#### Card 3

- COL. 1-6 Value 26, db
- COL. 7-12 Value 24, db
- COL. 73-78 Value 38, db

#### Card 4

- COL. 1-6 Value 39, db
- COL. 7-12 Value 40, db
- COL. 73-78 Value 51, db

The above values of  $dB(x)$ ,  $db(x_I)$ , correspond to values of downstream distance  $x$ , which are uniformly spaced,  $\Delta x$  apart:

$$dB(x_I) = db [(I-1)\Delta x], I = 1, 2, \dots, N$$

If  $N \geq 52$ , prepare additional cards, as required, with 12 values per card, following the format of card 2.

3.1.2.6 SECOND BENDING MODE VALUES Cards  
(Omit these cards if no entry is made for  $f_{2n}$ ).

Card 1

COL. 1-2 No. of ordinal (db) values,  $n$   
COL. 3-8 Interval,  $\Delta x$ , along abscissa  
COL. 9-14 Value 1, dB  
COL. 15-20 Value 2, dB  
COL. 75-80 Value 12, dB

Card 2

COL. 1-6 Value 13, dB  
COL. 7-12 Value 14, dB  
COL. 73-78 Value 25, dB

Card 3

COL. 1-6 Value 26, dB  
COL. 7-12 Value 27, dB  
COL. 73-78 Value 38, dB

Card 4

COL. 1-6 Value 39, dB  
COL. 7-12 Value 40, dB  
COL. 73-78 Value 51, dB

For  $n \geq 52$  and for an explanation of the origin of the decibel values, refer to the remarks made for the first bending mode values.

### 3.1.2.7 FINISH Card\*

COL. 1-6 FINISH

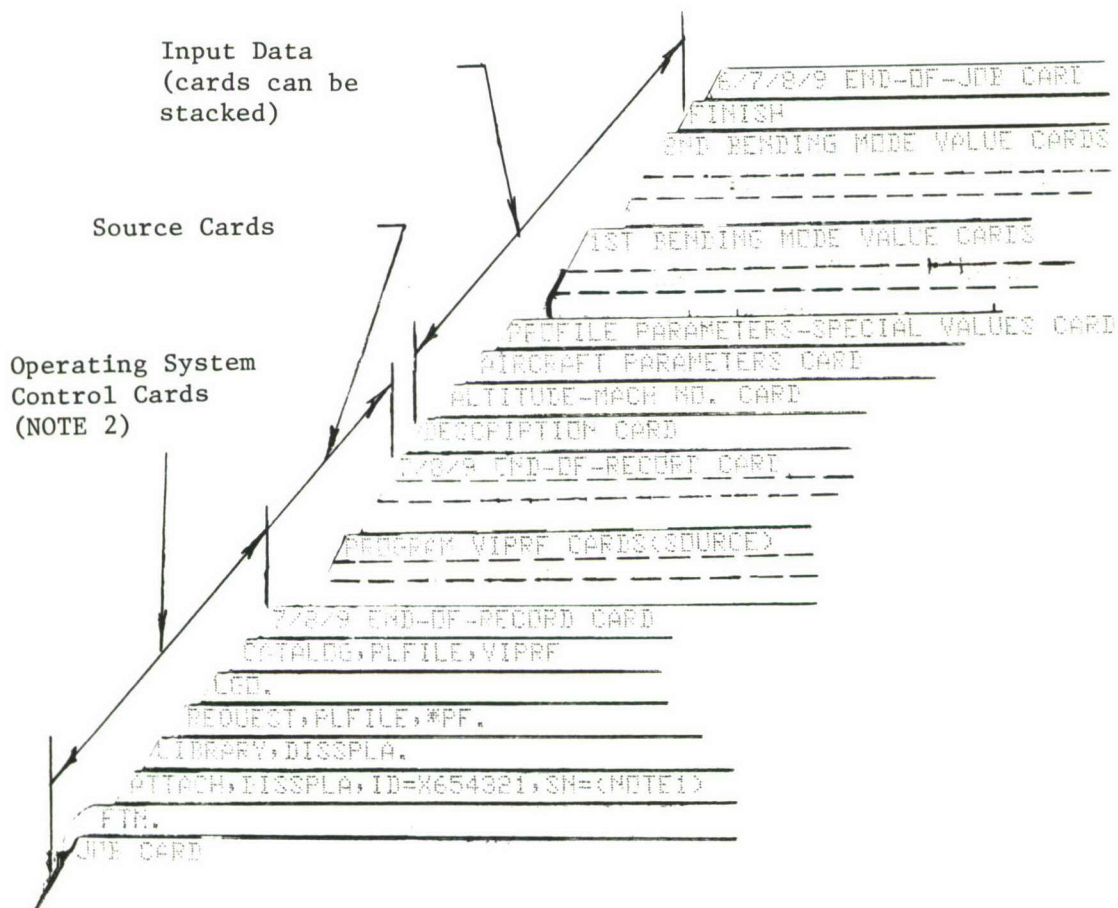
### 3.1.3 Deck Setup Card Forms ("Source" and "Binary")

In the following illustrations, deck setups are shown for execution of the program in both the source and the binary card form (Control Data Corp. 6600 and Cyber 74 Computer System, using the NOS/BE operating system).

The DISSPLA plot file (PLFILE) is copied to the permanent file, VIPRF.

Both illustrations refer to notes that are found at the end of 3.1.4.3.

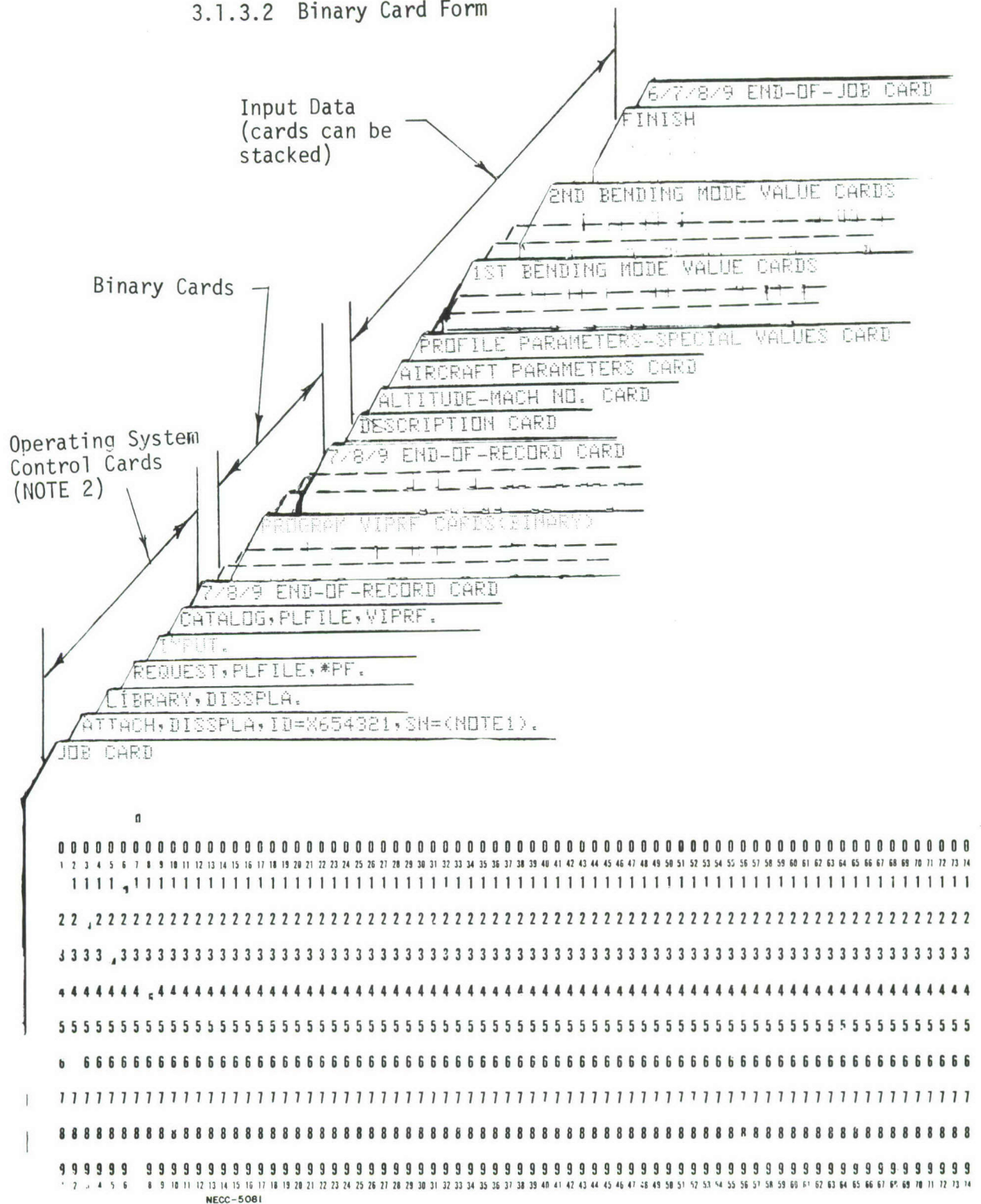
### 3.1.3.1 Source Card Form

[illegible]

\*Must be last card in every set of input data cards -- cannot be omitted.



### 3.1.3.2 Binary Card Form



### 3.1.4 Plot Programs ("On-line" and "Off-line")

In the following illustrations, deck setups are shown for executing the "on-line" and "off-line," DISSPLA, post processor plot programs.

#### 3.1.4.1 "On-line" Plot Program

CALCOMP plotter. DISSPLA plots are produced on-line, on a

```

/6/7/8/9 END-OF-JOB CARD
DRAW=1-ENDS
7/8/9 END-OF-RECORD CARD
RETURN,DISSPLA,PLFILE.
ONLINE.
ATTACH,PLFILE,VIPRF,CY=(NOTE 3),ID=(NOTE 3).
LIBRARY,DISSPLA.
ATTACH,DISSPLA,ID=X654321,SN=(NOTE 1).
JOB CARD

```

#### 3.1.4.2 "Off-line" Plot Program

Final plot information is copied to file on magnetic tape (Tape 99). Then, this tape is transferred to an off-line plotter system for graphical recording. However, before any of this can be done, it is necessary to request (Computer Operations) the desired tape to be assigned to Tape 99. In the case illustrated here, the tape number is L02391. Note that if the job deck is submitted at the ASD Computer Center, Operations must be so instructed through submission of card form ASD-59, "Magnetic Tape Transaction Request." On this form the tape number and associated problem number is entered; whereupon the form is submitted together with the job deck. Finally, subsequent to plot program execution, Operations must be directed to mount the tape on the off-line plotter through submission of card form ASD-227, "Data Preparation Request." This card must include the tape and associated problem number as well as identification and plot information obtained from the day file of the computer program listing.

```

6/7/8/9 END-OF-JOB CARD
TRAU=1-END$
7/8/9 END-OF-RECORD CARD
OFFLINE.
ATTACH,PLFILE,VIPRF,CY=(NOTE 3),ID=(NOTE 3).
LIBRARY,DISSPLA.
ATTACH,DISSPLA,ID=X654321,SN=(NOTE 1).
LABEL,TAPE99,W,D=HI,L=MYTAPE,MSN=L02391,RING.
JOB CARD

```

### 3.1.4.3 Keyboard Visual Display

#### Keyboard Commands

LOG-IN INFORMATION (see ASD Computer Center Inter-  
com Guide)

ATTACH,PLFILE,VIPRF,CY=(NOTE3),ID=(NOTE3)

ATTACH,DISSPLA,ID=X654321,SN=(NOTE1)

XEQ,LIBLOAD=DISSPLA,TEK4010

DRAW=1-END\$

LOG-OUT

#### NOTES:

1. SN = ASD for computer system A.  
SN = AFIT for computer system B.
2. Refer to ASD computer center handbook, CDC NOS/BE USER'S GUIDE (latest revision).
3. CY = Permanent file cycle number shown in dayfile of computer listing.  
ID = Problem number under which permanent file was catalogued (shown in dayfile of computer listing).



## SECTION IV

### APPLICATIONS

#### 1.0 Examples

To illustrate the applications of the prediction program, a number of fighter aircraft are selected for a variety of equipment locations, categories, and flight conditions.

##### 1.1 F-4 (skin)

The inputs (card entries) are:

	SKIN RESPONSE	SANDL
H =	2000.0	ALTITUDE (FT.)
M =	.77	MACH NO.
X <sub>E</sub> =	32.60	DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE AERODYNAMIC PROFILE (FT.)
R <sub>S</sub> =	0.00	DISTANCE FROM SKIN (IN.)
W <sub>E</sub> =	0.00	EQUIPMENT WEIGHT (LBS.)
T =	.0400	THICKNESS OF SKIN MATERIAL (IN.)
D <sub>F</sub> =	54.0	DIAMETER OF FUSELAGE (IN.)
MATERIAL =	ALUMINUM	TYPE SKIN MATERIAL
CATEGORY =	1B	EQUIPMENT MOUNTING CATEGORY

The input, as it is entered on the input data cards, is shown in Figure 7. (Each of the five examples in this section are accompanied by their respective array of input data cards.) Note that five cards per array are shown -- in agreement with the guidelines provided by Table I and 3.1.1.

As an illustration, this example is rather special. It is interesting because the results describes the response of the unloaded



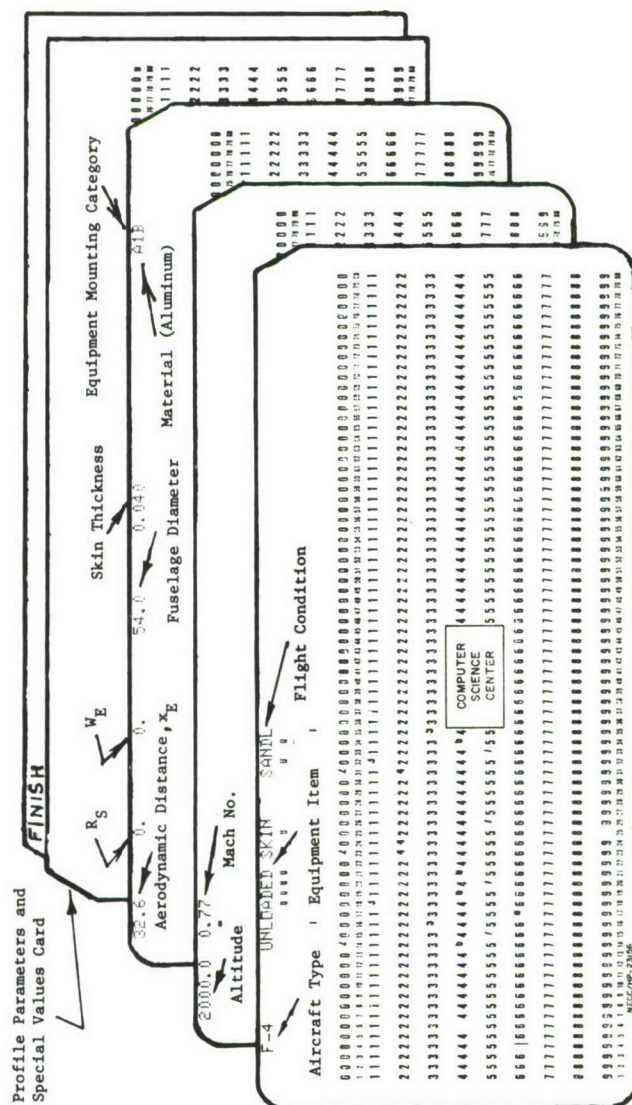


Figure 7. Input Data Cards, RF-4C Skin

skin ( $R_S$  and  $W_E = 0$ ) for straight and level (SANDL) flight. See Figures 8 and 9. The low frequency hump in Figure 9 represents the vibration contributions of the first and second fuselage bending modes.

### 1.2 F-16 (FCC)

Here, the prediction program describes the vibration input to the Flight Control Computer (FCC) of the F-16 (Figures 11 and 12) during straight and level flight. This example introduces the equipment configuration in which  $R_S$  and  $W_E$  are greater than zero -- as will be the case from here on out.

F-16	FCC	SANDL
H =	13000.0	ALTITUDE (FT.)
M =	1.55	MACH NO.
$X_E$ =	7.50	DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE AERODYNAMIC PROFILE (FT.)
$R_S$ =	3.00	DISTANCE FROM SKIN (IN.)
$W_E$ =	31.20	EQUIPMENT WEIGHT (LBS.)
$t$ =	.0360	THICKNESS OF SKIN MATERIAL (IN.)
$D_F$ =	40.0	DIAMETER OF FUSELAGE (IN.)
MATERIAL =	ALUMINUM	TYPE SKIN MATERIAL
CATEGORY =	1B	EQUIPMENT MOUNTING CATEGORY

### 1.3 F-4 (Instr. Panel, non-isolated)

This prediction problem describes the vibration spectrum of the radar altimeter indicator (RAI) located on the left side of the instrument panel, aft cockpit (Figures 14 and 15). The instrument panel is hard mounted (non-isolated). Flight conditions are straight and level (SANDL).

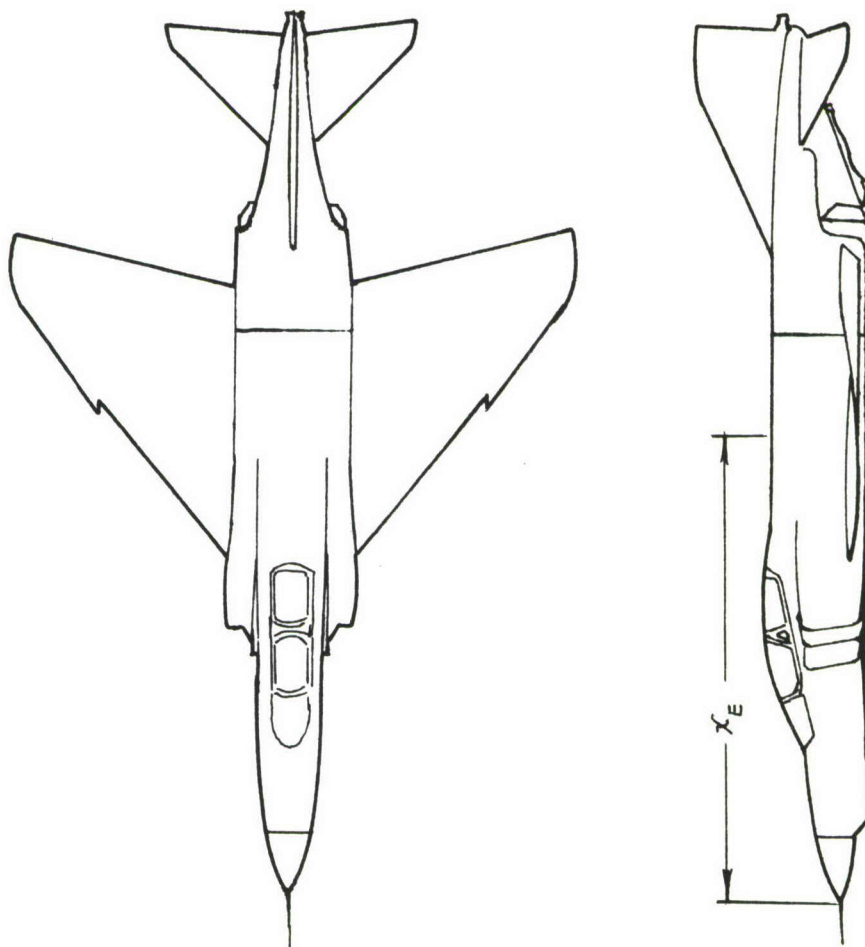


Figure 8. Location of Skin Response, RF-4C

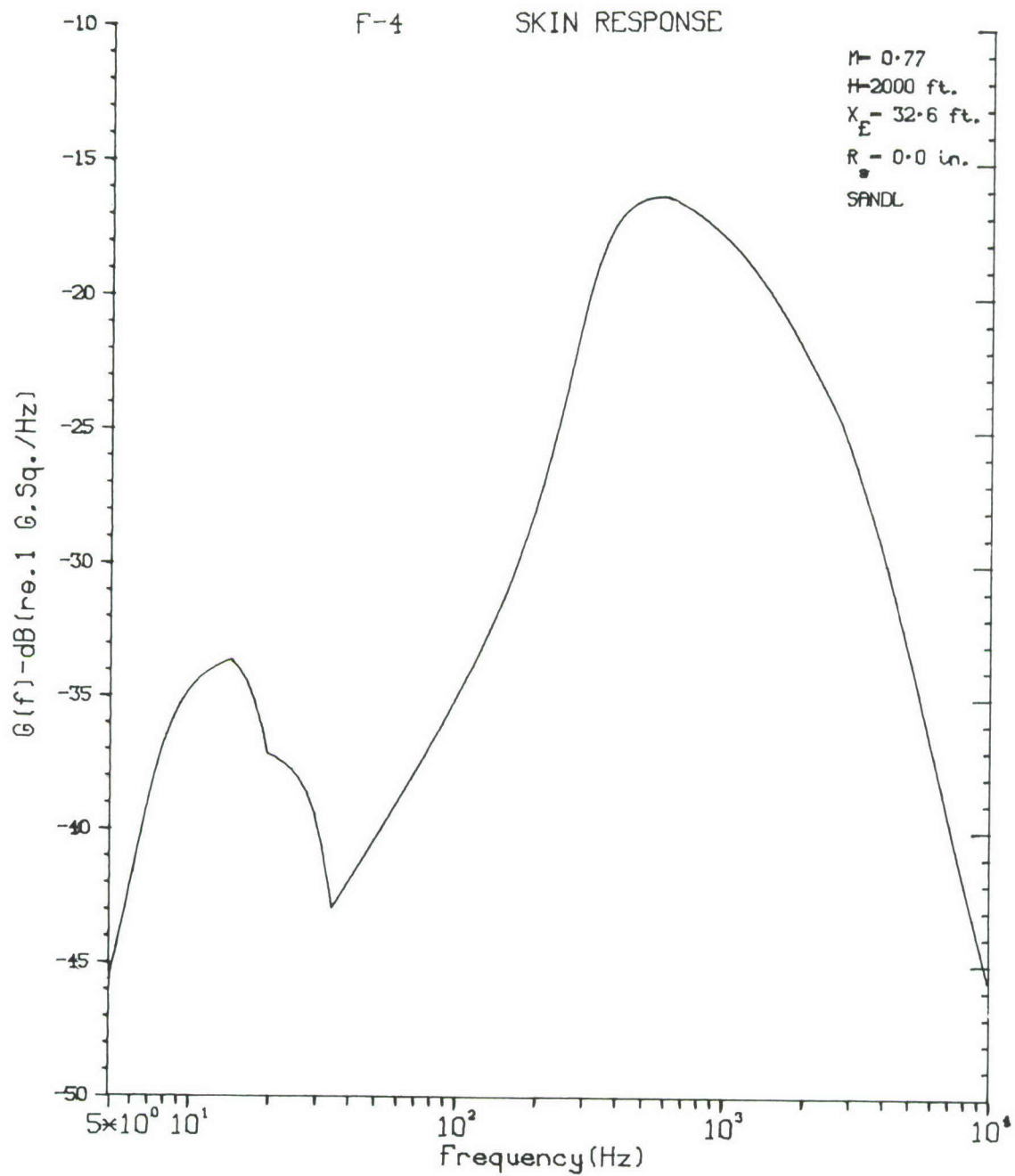


Figure 9. Predicted Response of Skin, RF-4C

[illegible]

Figure 10. Input Data Cards, FCC, F-16



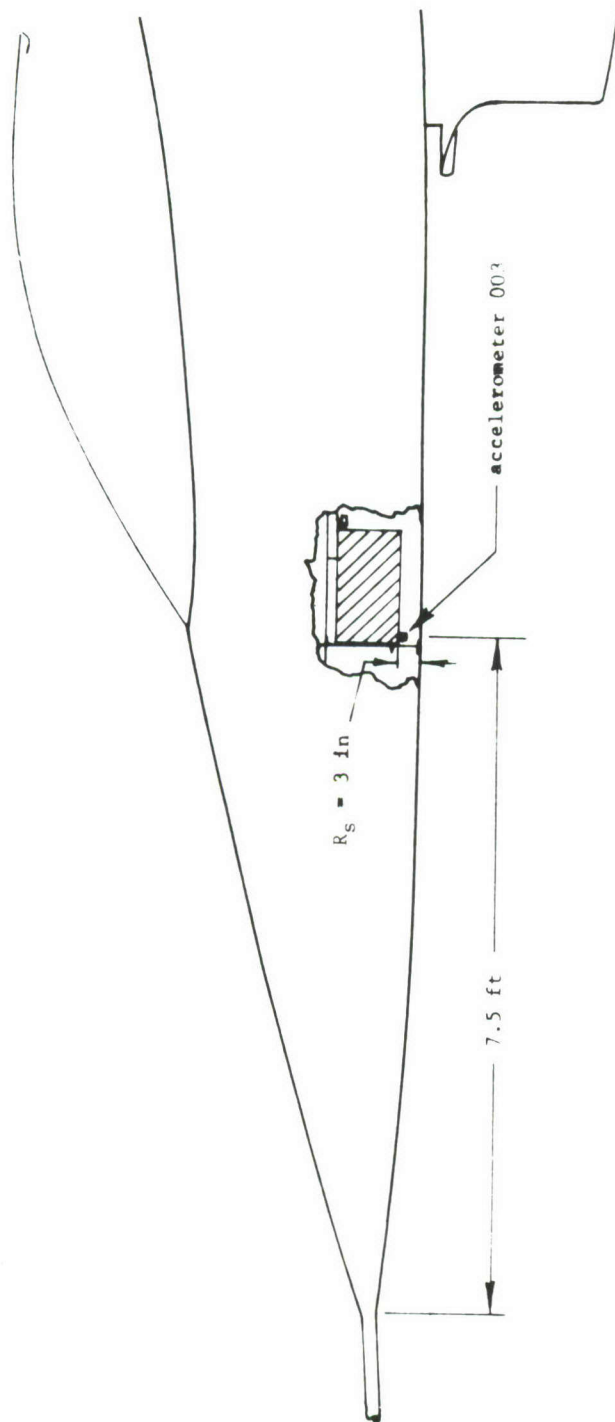


Figure 11. Location of Vibration Input to FCC, F-16

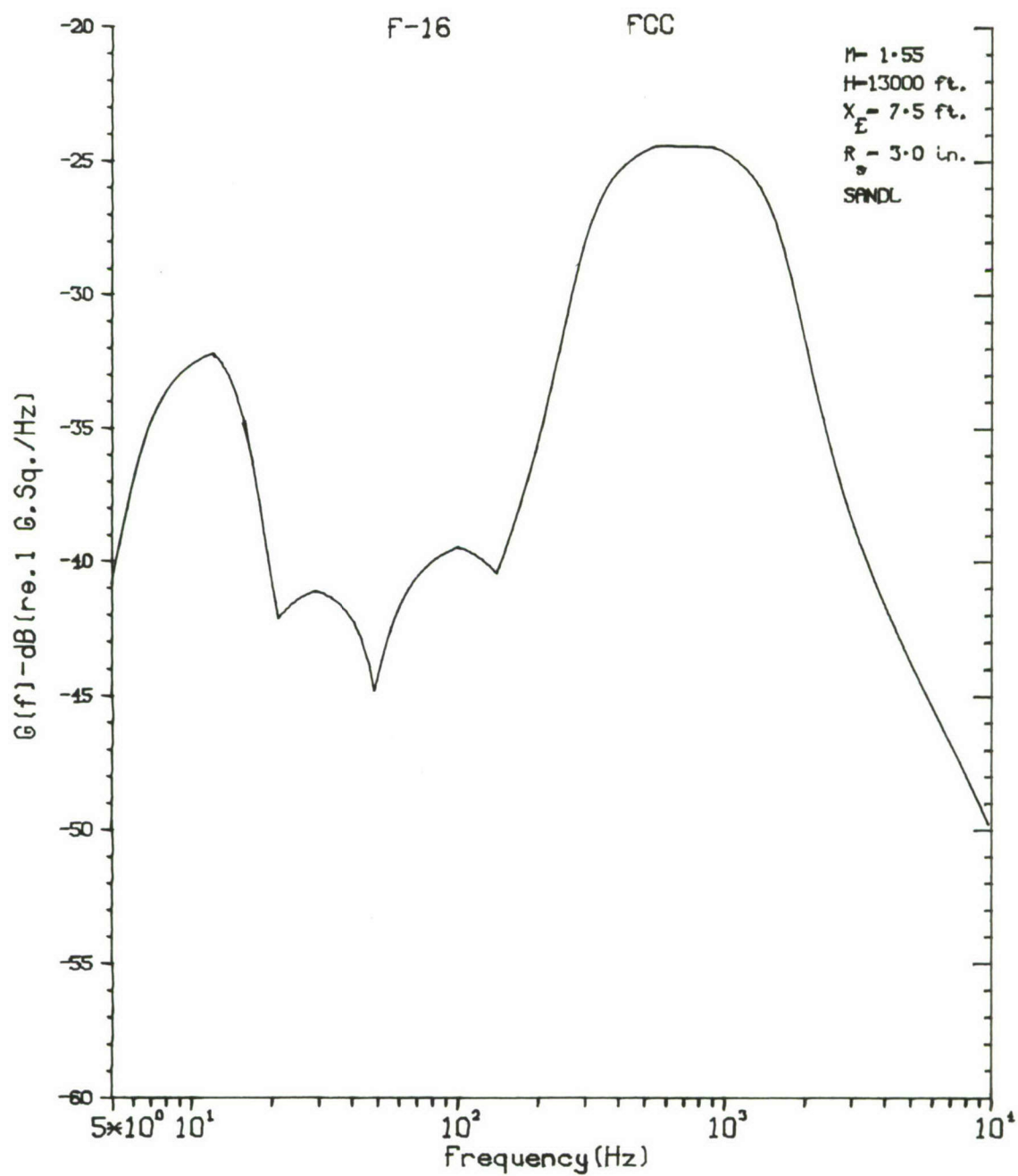


Figure 12. Predicted Vibration Input to FCC, F-16

[illegible]

Figure 13. Input Data Cards, RAI, RF-4C

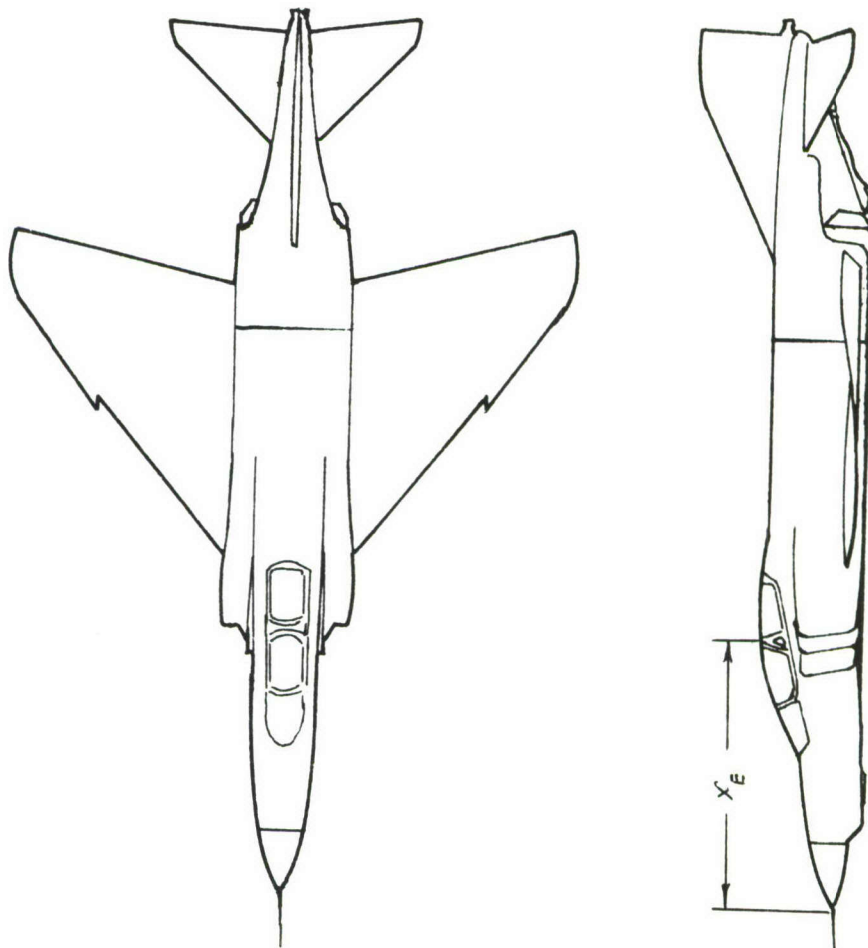


Figure 14. Location of RAI, Aft Instrument Panel, RF-4C

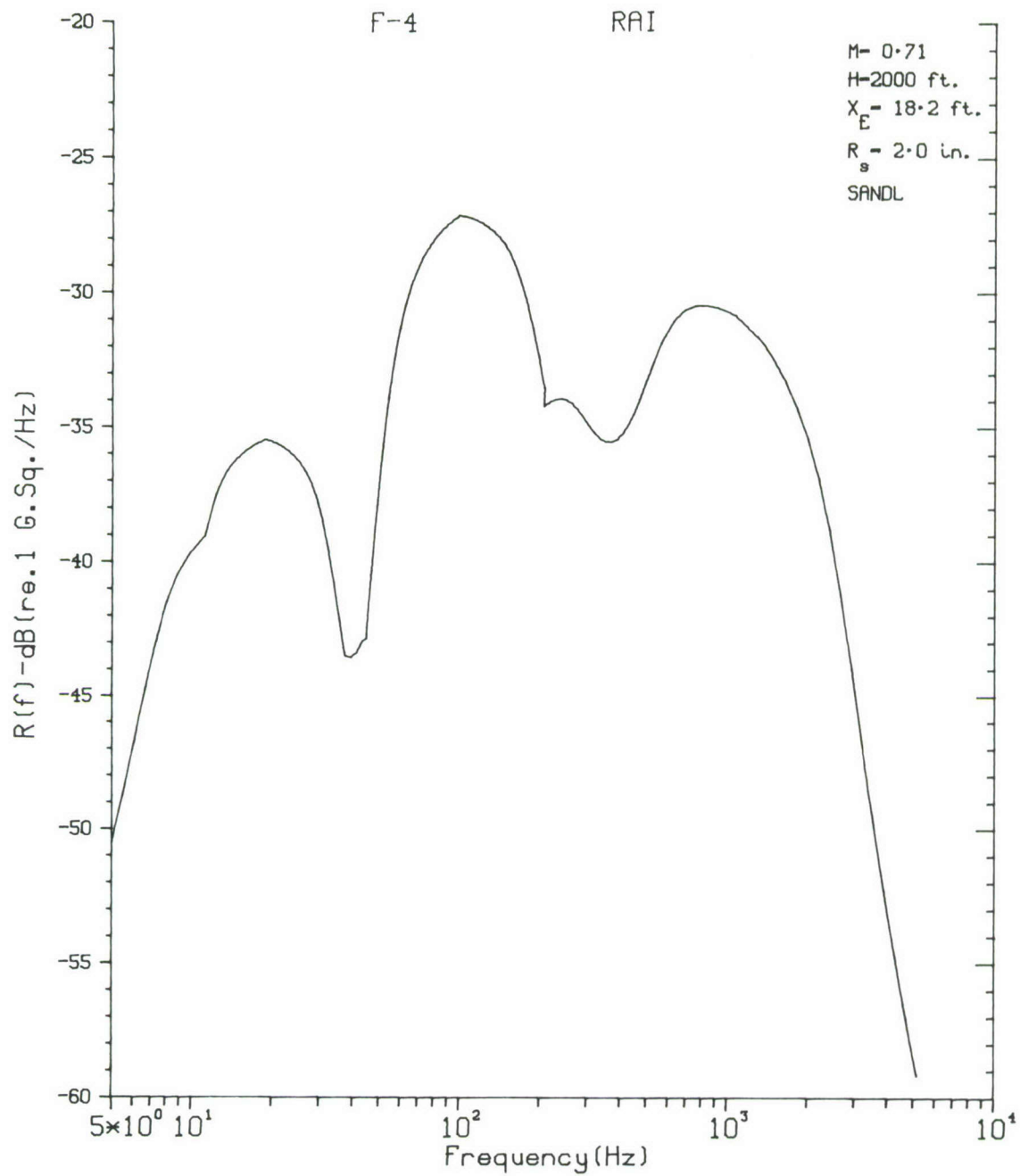


Figure 15. Predicted Vibration Input to RAI, Instrument Panel,  
Non-Isolated, RF-4C



F-4	RAI	SANDL
H =	2000.0	ALTITUDE (FT.)
M =	.71	MACH NO.
X <sub>E</sub> =	18.20	DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE AERODYNAMIC PROFILE (FT.)
R <sub>S</sub> =	2.00	DISTANCE FROM SKIN (IN.)
W <sub>E</sub> =	2.00	EQUIPMENT WEIGHT (LBS.)
T =	.0400	THICKNESS OF SKIN MATERIAL (IN.)
MATERIAL =	ALUMINUM	TYPE SKIN MATERIAL
CATEGORY =	2B	EQUIPMENT MOUNTING CATEGORY
D <sub>F</sub> =	57.0	DIAMETER OF FUSELAGE (IN.)

All hard mounted secondary structures, of which non-isolated instrument panels are a member, involve decision criteria concerning the location of the equipment item along the mode shape of the instrument panel (see para 1.2 of Appendix E and Figure E-6). As it turns out  $\epsilon \geq \lambda/4$ ; so  $R(f)$  has been selected, plotted and the results are shown in Figure 15. Note that if the user does not have a suitable estimate for the first bending mode frequency of the panel ( $f_{cIIb}$ ) then he may refer to the recommended values in Table II, Section III.

#### 1.4 A-7D (Instr. Panel, isolated)

The A-7D features an isolated instrument panel (isolator natural frequency,  $f_{cIIa}$ , is 45 Hz). This problem involves a Radio Frequency Indicator (RFI) mounted on the instrument panel (Figures 17 and 18). We wish to predict the indicator response during SANDL flight.

The inputs are:

[illegible]

Figure 16. Input Data Cards, RFI, A-7D

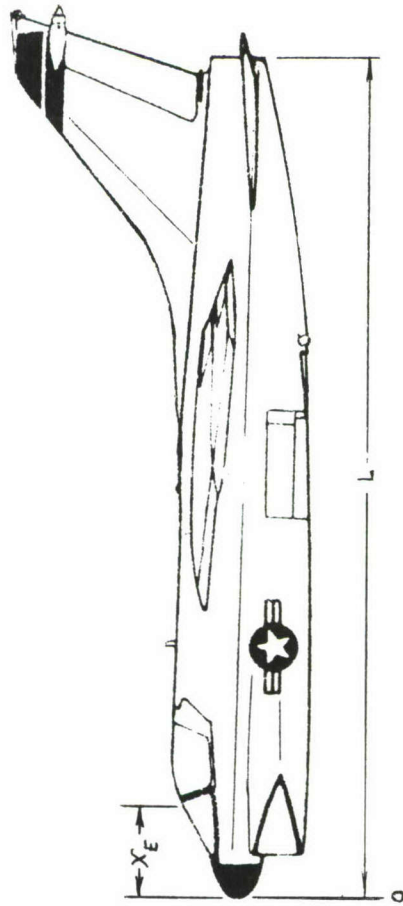


Figure 17. Location of RFI, Instrument Panel, Isolated, A-7D

A-7D	RFI	SANDL
H =	10000.0	ALTITUDE (FT.)
M =	.80	MACH NO.
X <sub>E</sub> =	4.80	DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE AERODYNAMIC PROFILE (FT.)
R <sub>S</sub> =	1.50	DISTANCE FROM SKIN (IN.)
W <sub>E</sub> =	1.20	EQUIPMENT WEIGHT (LBS.)
T =	.0400	THICKNESS OF SKIN MATERIAL (IN.)
MATERIAL =	ALUMINUM	TYPE SKIN MATERIAL
CATEGORY =	2A	EQUIPMENT MOUNTING CATEGORY
D <sub>F</sub> =	46.0	DIAMETER OF FUSELAGE (IN.)

The predicted response of the instrument panel, or the input to the RFI, is shown in Figure 18.

#### 1.5 F-15 (Black Box Input, Shock Mounted)

A black box assembly, consisting of the TACAN and the APX-76, is located in the nose region of the F-15 (Figure 20). The assembly is shock mounted. The isolator natural frequency is 25 Hz. We wish to predict the vibration input to the shock mounts for the SANDL case as well as for the buffet turn (BT).

The inputs are:

F-15	APX-76	BT
H =	25000.0	ALTITUDE (FT.)
M =	.90	MACH NO.
X <sub>E</sub> =	10.1	DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE AERODYNAMIC PROFILE (FT.)
R <sub>S</sub> =	5.00	DISTANCE FROM SKIN (IN.)
W <sub>E</sub> =	54.00	EQUIPMENT WEIGHT (LBS.)
T =	.0400	THICKNESS OF SKIN MATERIAL (IN.)
MATERIAL =	ALUMINUM	TYPE SKIN MATERIAL
CATEGORY =	1B	EQUIPMENT MOUNTING CATEGORY
D <sub>F</sub> =	40.0	DIAMETER OF FUSELAGE (IN.)

The entry condition for buffet turn is M=0.90 and H=25,000 ft. Note that the entry condition, or reference straight and level,

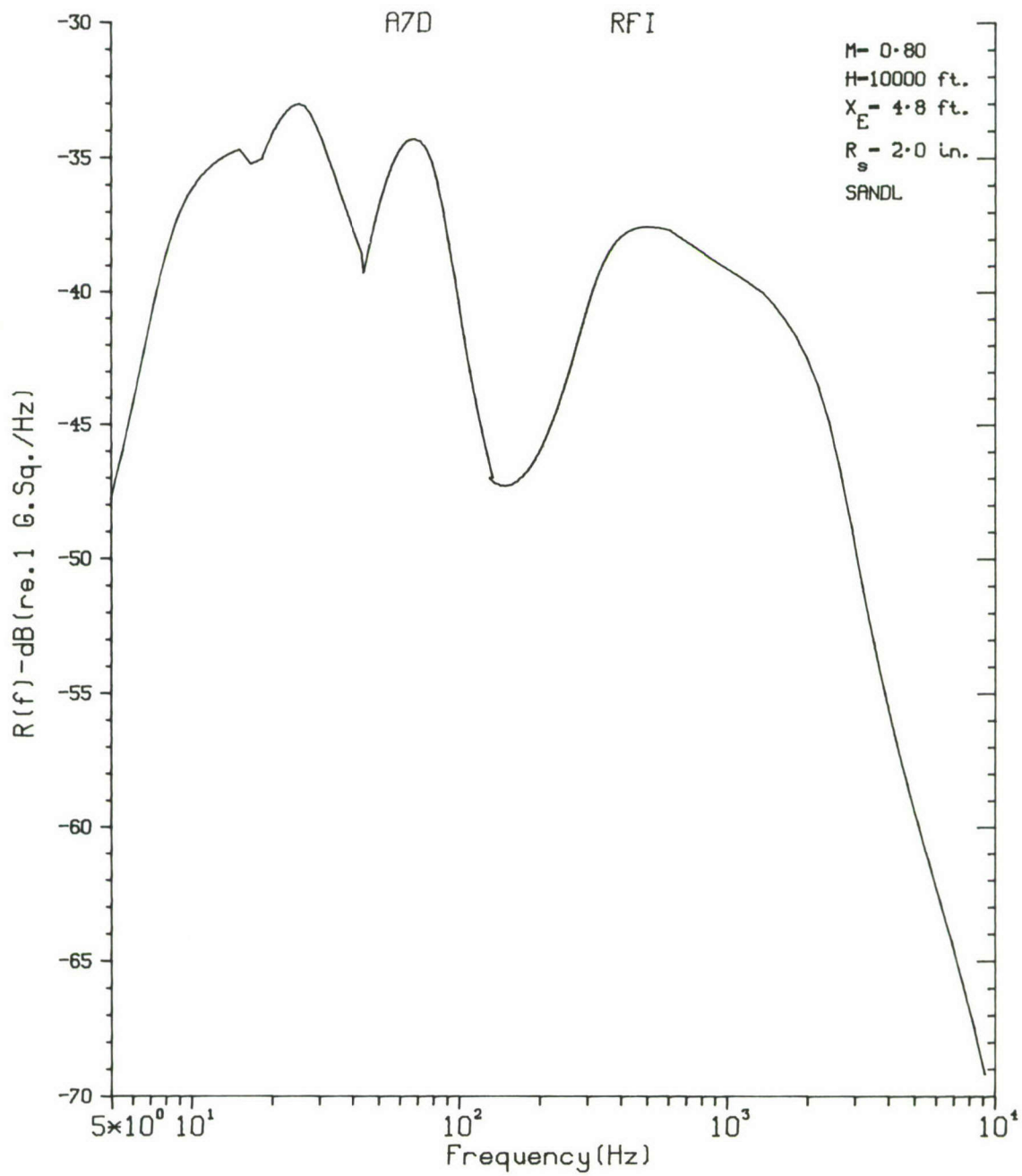


Figure 18. Predicted Vibration Input at RFI, Instrument Panel, Isolated, A-7D



[illegible]

Figure 19. Input Data Cards, APX-76, F-15

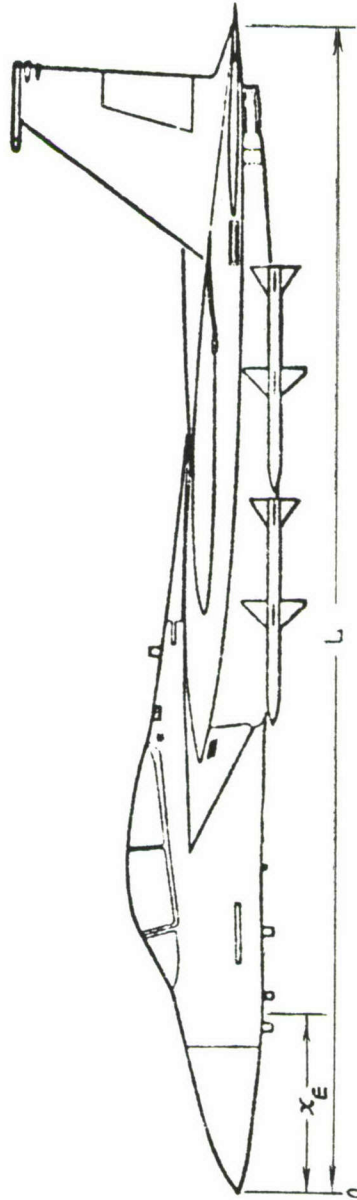


Figure 20. Location of APX-76, Isolated, F-15

is automatically plotted in the program along with the buffet turn curve (see para 3.1.2.1 of Section III). The resultant plots are shown as Figures 21 and 22. The impressive rise of the vibration level in the region of 35 Hz during buffet turn reminds us that severe spectral levels, though brief in duration, can be encountered ... and we add here, that they often go unnoticed by the vibration engineer.

#### 1.6 F-15 (Black Box Response, Shock Mounted)

We repeat para 1.5, except now we wish to predict the response of the assembly mounted on the isolator. If we change category I(b) to I(a) and enter the isolator natural frequency as  $f_{cIa}=25\text{Hz}$ , we may then add the remaining inputs of para 1.5 to complete the program (Figure 23). The equipment response for entry (reference) SANDL and, finally, for BT is shown as Figures 24 and 25. Here, we see the equipment response -- an excitation magnified significantly by the isolator transfer function.

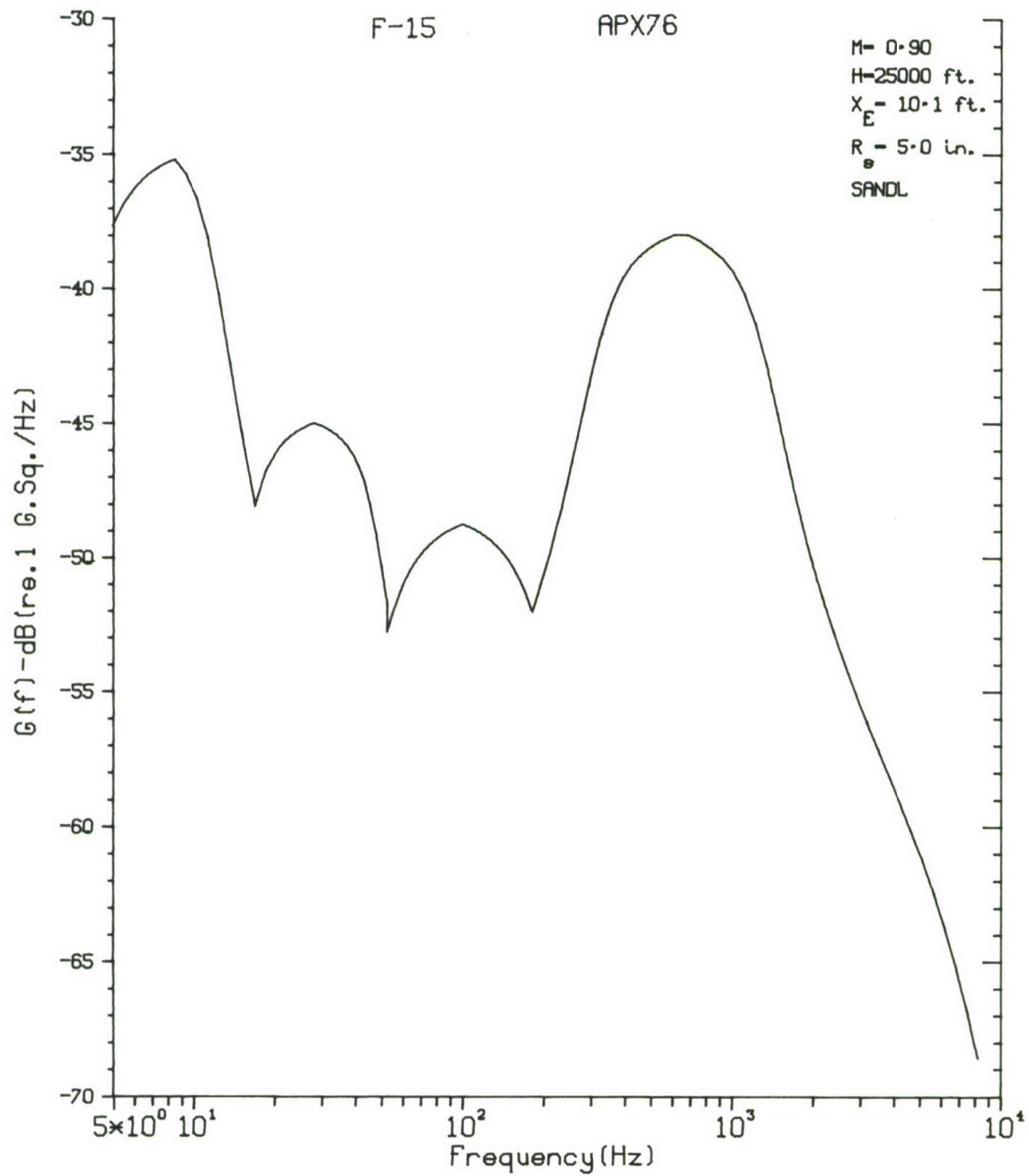


Figure 21. Predicted Input to APX-76, Isolated, F-15, for SANDL Flight

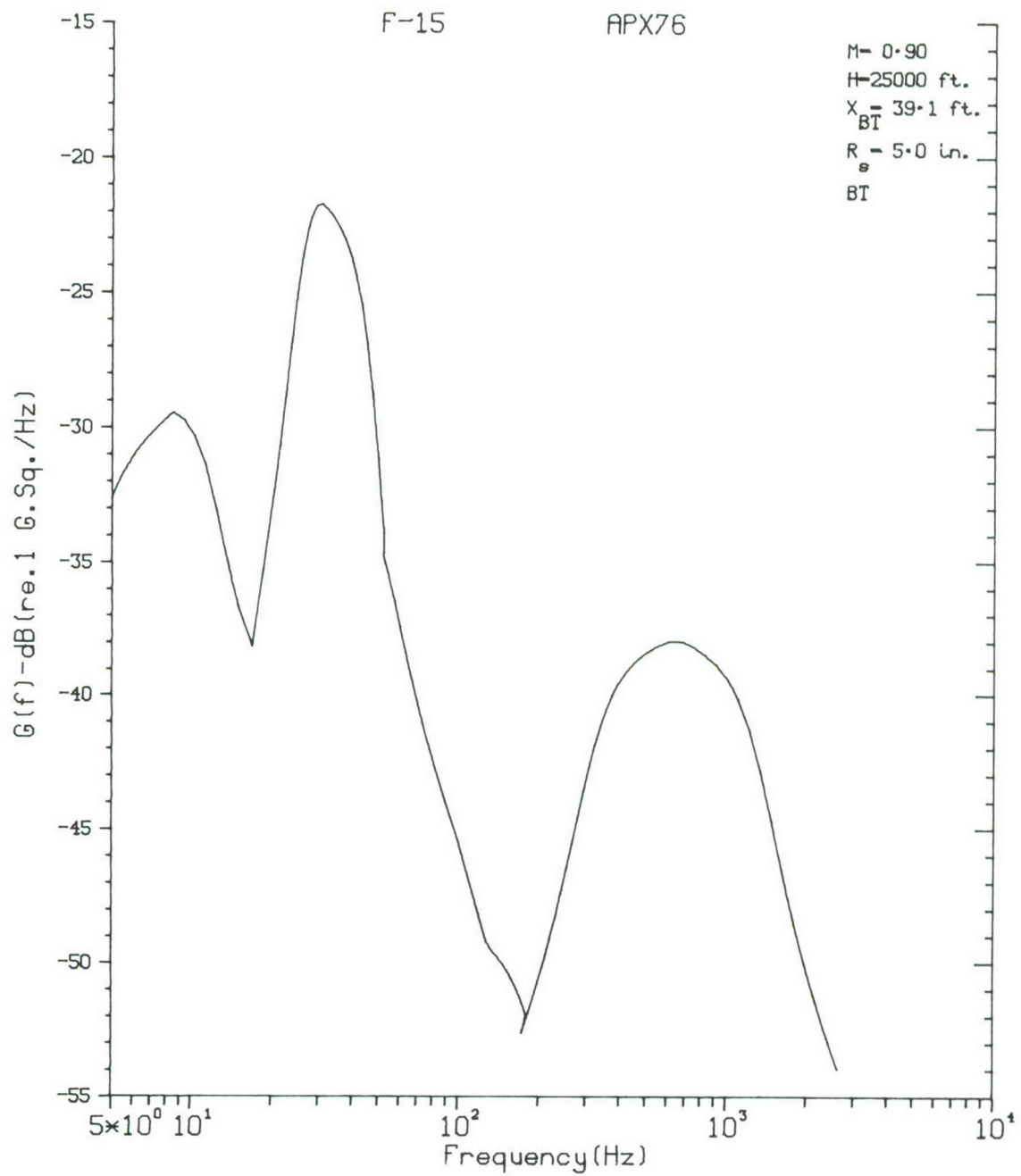


Figure 22. Predicted Input to APX-76, Isolated, F-15, for Buffet Turn



[illegible]

Figure 23. Input Data Cards, APX-76 Response, F-15

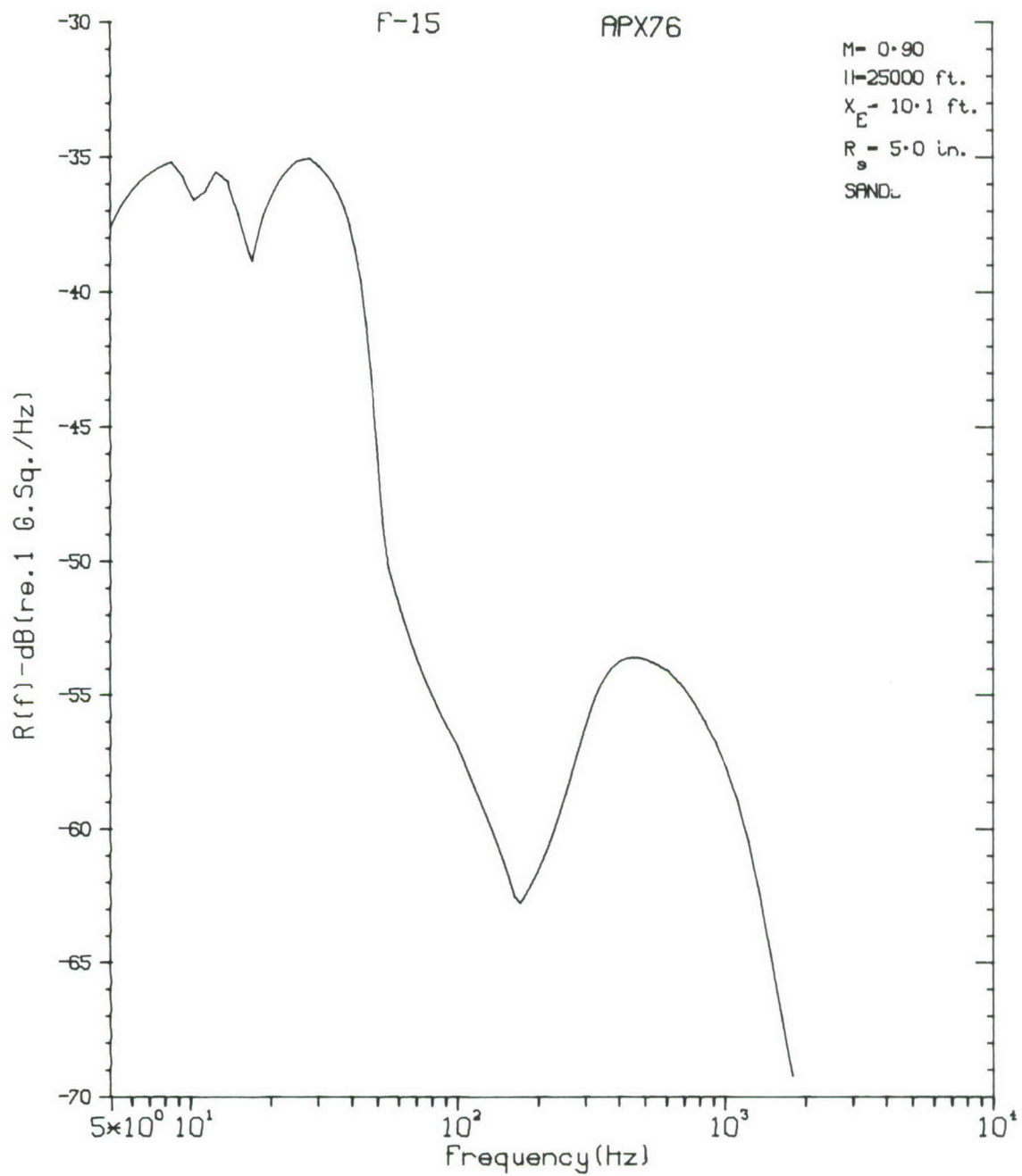


Figure 24. Predicted Response of APX-76, F-15, for SANDL Flight

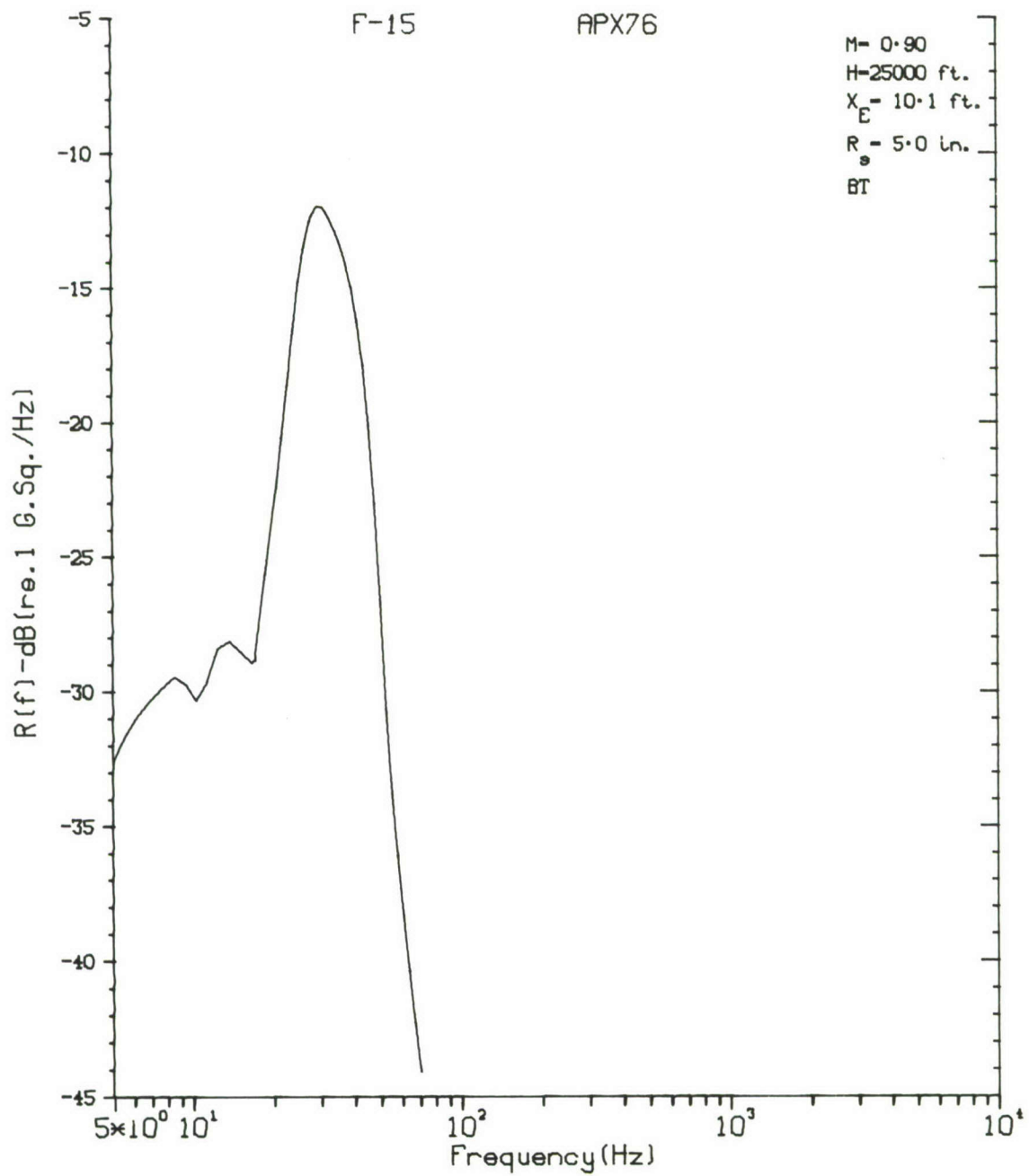


Figure 25. Predicted Response of APX-76, F-15 for Buffet Turn

## SECTION V

## REVIEW

## 1.0 Discussion

This work concludes with a discussion that briefly reviews the general philosophy of the prediction method, summarizes results thus far obtained, underlines some remnant problem areas or shortcomings, and finally, terminates with recommendations for future studies. Sections II and III show that, in the main, this prediction method employs the cross product of input and transfer functions both of which are utilized as variants of a basic equation whose curve is fundamentally sigmoidal in form and plastic in temperament. Indeed, in this approach to vibration prediction, functions of a consummate virtuosity are all but mandatory -- and thus far, the flex function, thought often distended in the application, has yet to be breached in the trial. It will remain for future applications (probably involving other special flight conditions and physical configurations) to determine the ultimate limits of its adaptability; in the meantime, it seems to be working reasonably well.

But this prediction approach is not solely preoccupied with the manipulation of an abstruse function. The process is also shaped and otherwise supplemented with large doses of empiricism, chiefly in the form of vibration data which is looped back into the various functions (most notably, the special functions) to provide corrective

information resulting in readjustments of the function parameters. In general, the more relevant, the more detailed, and the more perceptive the data choice; the more accurate the results. We go further: the more details that are known about the aircraft skin, of the equipment mounting method, of the equipment size, shape, function, and weight, of the class of the equipment support structure used, of the equipment proximity to special and significant physical configurations (guns, flaps, speed brakes, landing gear, refueling doors, cavities) -- the more that is known of these specifics, the more readily transfer and special functions can be shaped, sized, and integrated into the prediction format to further the advance of a more realistic prediction end.

With these guidelines in mind, it is useful to review some deficient areas of the vibration data process and reflect on its consequences concerning the results of this prediction technique.

#### 1.1 Instrument Panels

Extant vibration data covering instrument panels is relatively scarce, especially data from pickups that measure the input-output properties of the panel or data from response pickups that are located in the central one-third of the panel (central one-third of the half panel, if the panel is tied down at the center). Data indicating the panel weight, the mounting method (isolated or non-isolated) and the isolation frequency, if isolated, is nearly always unspecified and must be ascertained separately -- often at considerable difficulty. From these observations, it is easy to deduce that the



instrument panel transfer functions for the isolated and non-isolated case (Categories IIa and IIb) will, in all probability, be adjusted as additional suitable data becomes available. Finally, it is worth noting that instrument panel vibration, because of the severe levels, should be recorded, wherever possible, during violent flight phases such as buffet turn; especially for those aircraft whose cockpits are located near to, or over the wing areas.

## 1.2 Skin

Pickups on the skin are, sometimes, not skin mounted -- being mounted on adjacent frames, for example, and if they are placed at the central panel area, they are often of a size (mass) to roll off the high frequencies and so one must apply adjustments to the data in order to derive the transfer function (see Ref. 8). Despite these problems, the skin transfer function derived and used for this prediction process seems to be reasonably accurate for curved aluminum skin surfaces, forty thousandths of an inch thick. Suitable measurements on other type aircraft surfaces (including the wings) should be obtained, however, and much useful transfer function information can be developed for surfaces of greater thicknesses, and for that matter, surfaces of different geometry and composition. Boundary layer microphones remain a problem. They are usually massy; and, if anything, they (rather than accelerometers) are the ones to be moved over near the frame to reduce mass loading. Boundary layer microphone data are rarely accompanied with information indicating whether or not the data has been corrected for the boundary layer thickness and

the microphone effective diameter. The diameter is almost never indicated; but it should be. Sufficient spatial information (fuselage station, for example) should always be included with the microphone data in order that the down stream distance can be determined.

### 1.3 Buffet Turn

Vibration data covering the buffet turn (BT) maneuver is also rather hard to come by, thus the special function  $[S(f)]$  derived for the BT maneuver should be viewed as tentative; subject to future adjustments, if and when new data indicates. The general spectral characteristics occasioned by this maneuver, it is interesting to note, are similar to those generated during pullups; and if we are careful not to push the comparison too far, they are rather similar to such flight phases as lowered speed brakes, flaps, landing gears, and for that matter, open refueling doors and cavities. Processed data and extant vibration records should be sought and examined whenever opportunities arise to obtain valuable parametric information about these flight phases. Because quite apart from their being valuable contributions to the prediction process, the sudden bloom of their spectral peaks (as much as 25 dB!) provides instructive warning to equipment vibration and reliability engineers that straight and level vibration is only a part of the environmental history.

### 1.4 Forward Looking Radar Zones

The high frequency vibration fields of forward looking radar zones tends to be appreciably higher than the norm. The reasons for this seem to be due to the relatively empty air space

provided by the radome in combination with the low internal damping of the radome cover. Without the mass loading and lossy damping attenuations provided by the usual dense equipment packaging, this area, not surprisingly, will exhibit vibration levels (above 150 Hz) in excess of 6 to 10 dB above that of predicted levels. Because of this,  $H_M(f)$  and  $M_M(f)$  have been adjusted (in the program) to cover applications for equipment attached to forward looking radar bulkheads. Future additional data may indicate that further adjustments and improvements are desirable.

### 1.5 Sinusoidals

Sinusoidal-like vibration is present in various regions of the aircraft. It is found in the presence of blowers, pumps, generators, refrigeration units; and, most conspicuously, it is seen as one approaches the engine compartments. Here the vibration content may be fairly described as consisting of predominant sinusoids, superposed on a subordinate, random background. There is no provision in this method for this class of vibration; there should be.

### 1.6 Determining $R_s$

Normally, if the equipment is located on primary structure,  $R_s$  is chosen as the nearest distance from the aircraft skin to the equipment attachment point. Although this criteria may be modified as the method is applied more and more, the interpretation stated appears to be reasonably workable. However, its application to equipments attached to shelves and beams (secondary structure) is not so certain. At present, the author has chosen the nearest distance from the skin to the place (point) where the member attaches to the primary structure.

This criteria, too, could change in the future if repeated applications suggest.

#### 1.7 Future Work Areas

The prediction method and its associated computer program may be readily extended to cover vehicle locations and in-service operations not covered in this report. The following flight conditions and configurations are considered to be sufficiently important from the vibration viewpoint to warrant future considerations, and are listed for review.

- a. Speed brakes, pullups, flaps, landing gears, and open refueling door operations.
- b. Gunfire.
- c. Vertical fin vibration prediction.
- d. Wing locations; including missiles and their launchers.
- e. Cavities (ports and open weapons bay).
- f. Stores and pylons.



# APPENDIX A

## AERODYNAMIC PROPERTIES

### 1.0 Equations

The properties of  $P(f)$  are determined from the following equations and procedures:

$$P_m(f) = \frac{(.007)^2 q^2 \delta_b}{(1+.14M^2)^2 U} \quad (A-1)$$

$$f_{o\prime} = .61 U / \delta_b \quad (A-2)$$

$$\delta_b = \delta_o (\rho / \rho_o) \quad (A-3)$$

$$\delta_o = 0.37 x Re_x^{-1/5} \left[ 1 + \left( \frac{Re_x}{6.9 \times 10^7} \right)^2 \right]^{1/10} \quad (A-4)$$

where:

$P_m(f)$  = max value of  $P(f)$  (PSF<sup>2</sup>/Hz)

$q$  = dynamic pressure,  $\rho U^2/2$  (PSF)

$\delta_b$  = boundary layer thickness (ft)

$M$  = Mach number

$U$  = free stream velocity (ft/sec)

$f_{o\prime}$  = characteristic, or locator frequency of the flex function at the 6 dB down point (Hz)

$\delta_o$  = boundary layer thickness at zero altitude (ft)

$\rho$  = mean density of air at flight altitude (slug/ft<sup>3</sup>)

$\rho_o$  = mean density of air at zero altitude (slug/ft<sup>3</sup>)



$x$  = distance downstream from the leading edge of the  
aerodynamic profile to the equipment location (ft)

$Re_x = U x / \nu$  = Reynolds number at distance  $x$

$\nu$  = kinematic viscosity ( $ft^2/sec$ )

With the mach number and altitude given for straight and level flight (SANDL) the boundary layer parameters  $P_m(f)$  and  $f_0$  are then determined. A graph (Figure A-1) is used to obtain  $\beta'$ . These three parameters, assigned to the flex function of Figure 6 of the main text, completely defines  $P(f)$ . To obtain  $P(f)$ , in dB, refer to the graph shown in Figure A-2. A typical example of a boundary layer pressure spectral density curve ( $P(f)$  as a function of frequency) is shown in Figure A-3.

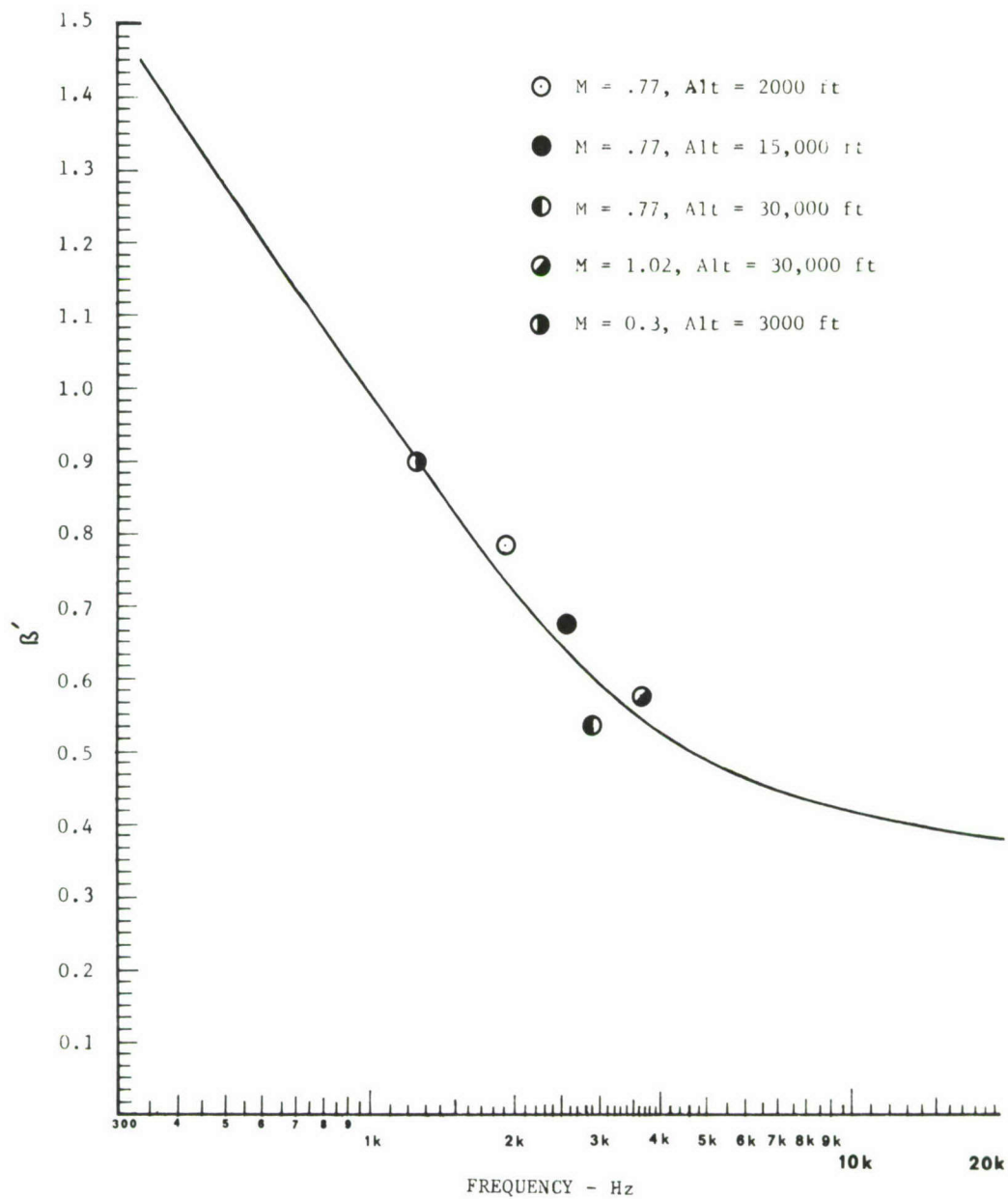


Figure A-1. The slope Factor,  $\beta'$ , as a Function of  $f_o$ .

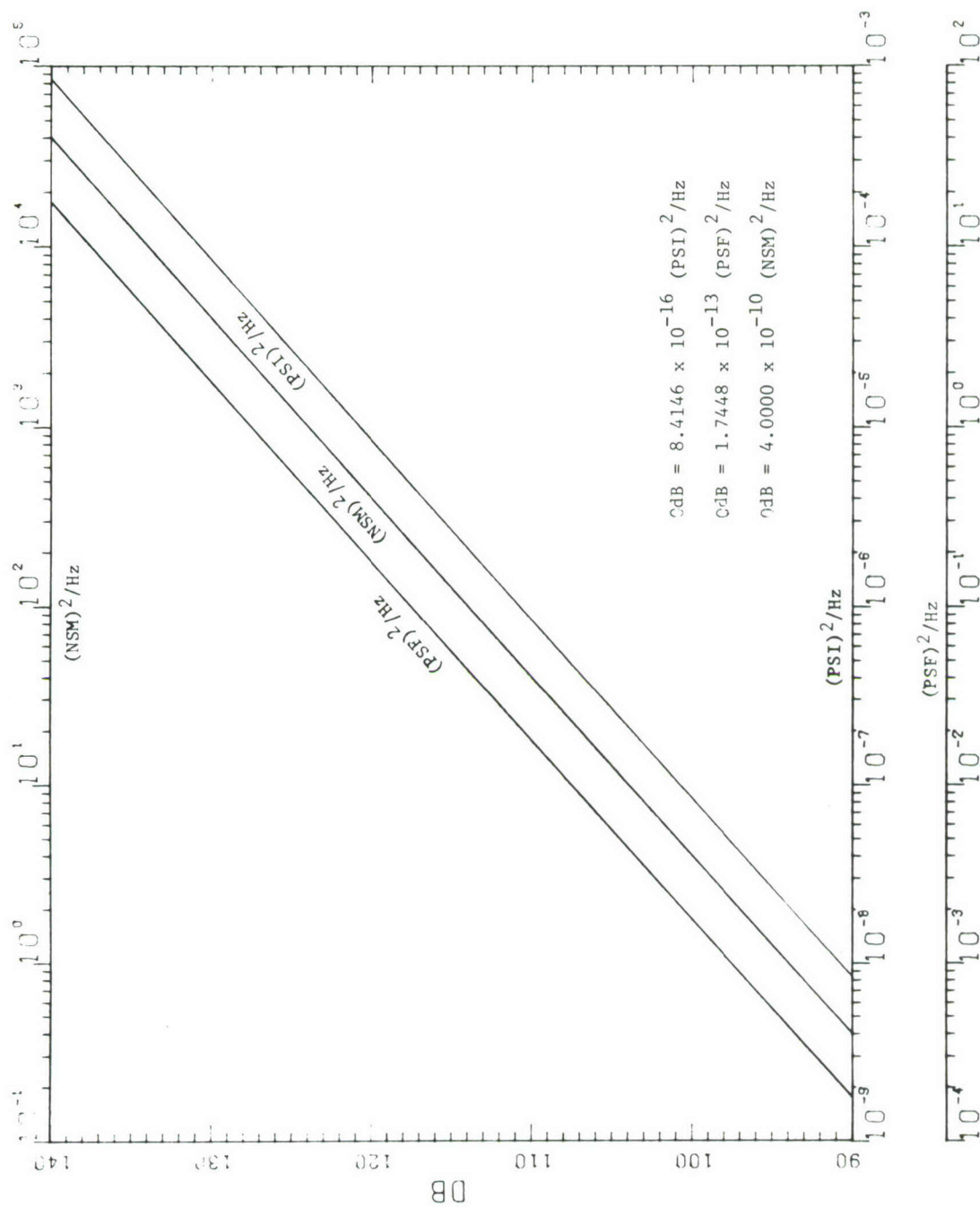
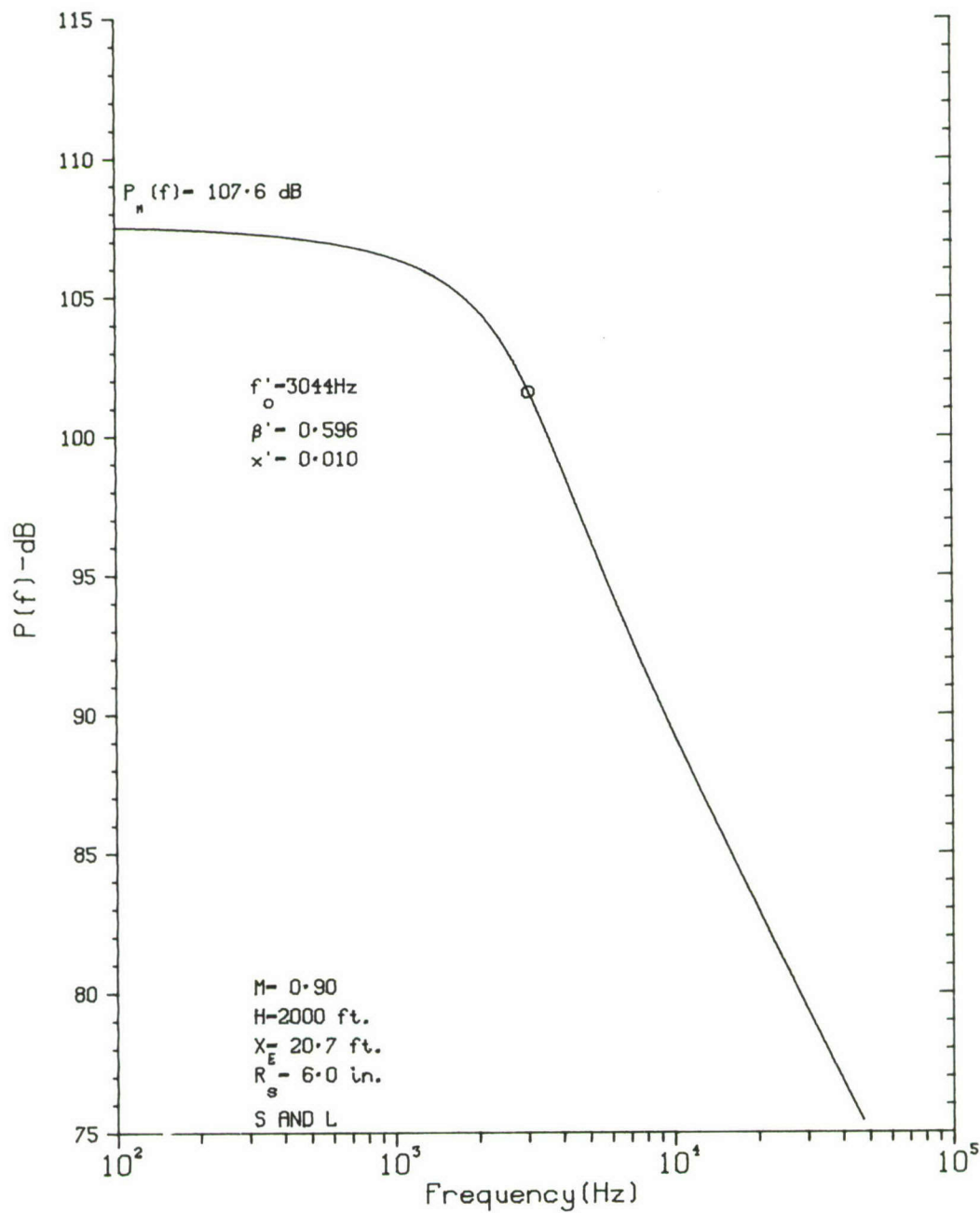


Figure A-2. Conversion Chart (dB as a Function of  $P(f)$ )

PREDICTED PRESSURE SPECTRAL DENSITY- $P(f)$ 

F-4 NAV.COMP.+SIG.CONV.

Figure A-3. Example of  $P(f)$  as a Function of Frequency

## APPENDIX B

## AIRCRAFT MODE SHAPES (FUSELAGE)

## 1.0 Terminology

The fuselage bending mode shapes are identified by the following symbolism:  $f_n$  = mode frequency (Hz)

$\phi_n(x)$  = normalized mode shape

FBBVS = first body bending, vertical, symmetric

SBBVS = second body bending, vertical, symmetric

$x$  = aerodynamic distance downstream (inches)

$L$  = maximum value of  $x$  (inches)

F.S. = aircraft fuselage station (inches)

## 2.0 Modal Shapes

Each deflection curve has been squared and normalized at the forward fuselage location corresponding to  $x=0$ . For some aircraft,  $x$  is approximately the same as the fuselage station; for others, it is not. Immediately following the two graphs of the first and second bending modes is a sideview of each aircraft that identifies the  $x$  and  $L$  parameters. Also included is a notation relating the  $x=0$  coordinate to that of the aircraft fuselage station.

## 3.0 Derivation of Modal Properties

For fighter aircraft types not included in this Appendix, it will be necessary, as stated in Section III, to obtain the required modal properties and enter them into the program deck before the



prediction scheme can be utilized. The required modal shapes and frequencies are usually obtained from data abstracted from the aircraft ground vibration test report (GVT Report). The determination of  $L_M(f)$  requires other stratagems. In the absence of vibration data,  $L_M(f)$  must be estimated. The procedure for this step is found in Reference 8 and is here repeated.

$$L_M(f) = A + 20 \log (L/B) + 40 \log (f_N/C) \quad (B-1)$$

where:

$L_M(f)$  = property to be determined

$A = L_M(f)$  for a known, similar fighter (dB)

$L$  = length of the new aircraft (inches)

$B$  = length of a known, similar aircraft (inches)

$f_n$  = frequency, FBBVS, of the new aircraft (Hz)

$C$  = frequency, FBBVS, of a known, similar aircraft (Hz)

The maximum value of the low frequency transfer function,  $L_2(f)_M$ , may be estimated using the following relationship.

$$L_2(f)_M = L_M(f) - 6 \quad (B-2)$$

where adequate vibration data is available more desirable results may be achieved by noting  $G(f)$  (during SANDL flight) and, through the use of equation 14 (Section II), solving for  $L_M(f)$ .

$$P(f) [\phi_n(x) L_M(f)] = G(f)$$

and,

$$L_M(f) = \frac{G(f)}{P(f) \phi_n(x)} \quad (B-3)$$

Note that this procedure requires that the first bending mode shape be determined. Also, best results are obtained if one selects  $G(f)$  proximate to  $x=0$  where the mode response is large and usually conspicuous.  $L_2(f)_M$  may be determined by the response of the second bending mode  $G(f)$ , relative to the first bending mode value.

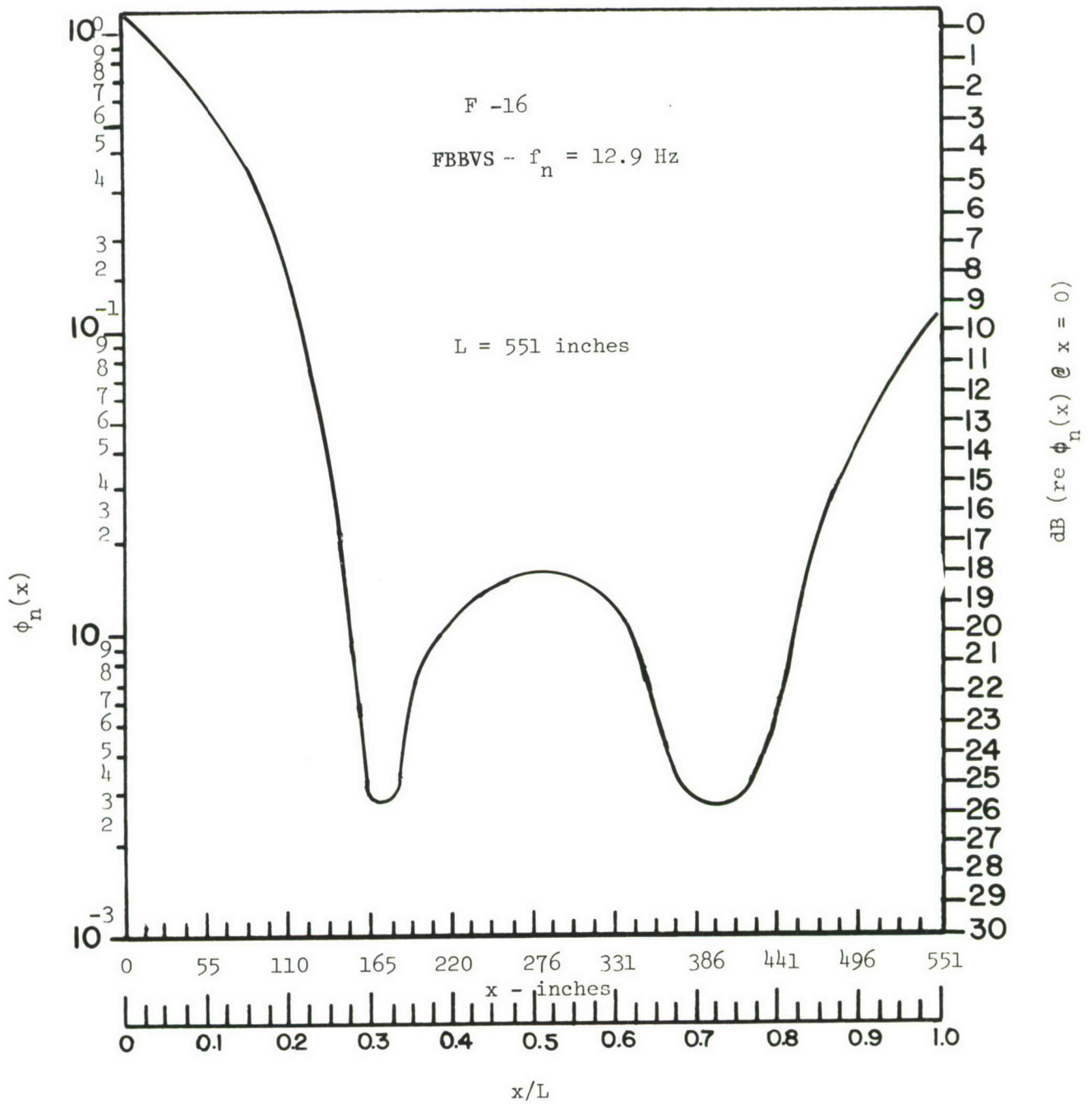


Figure B-1. Mode Shape (FBBVS) of the F-16

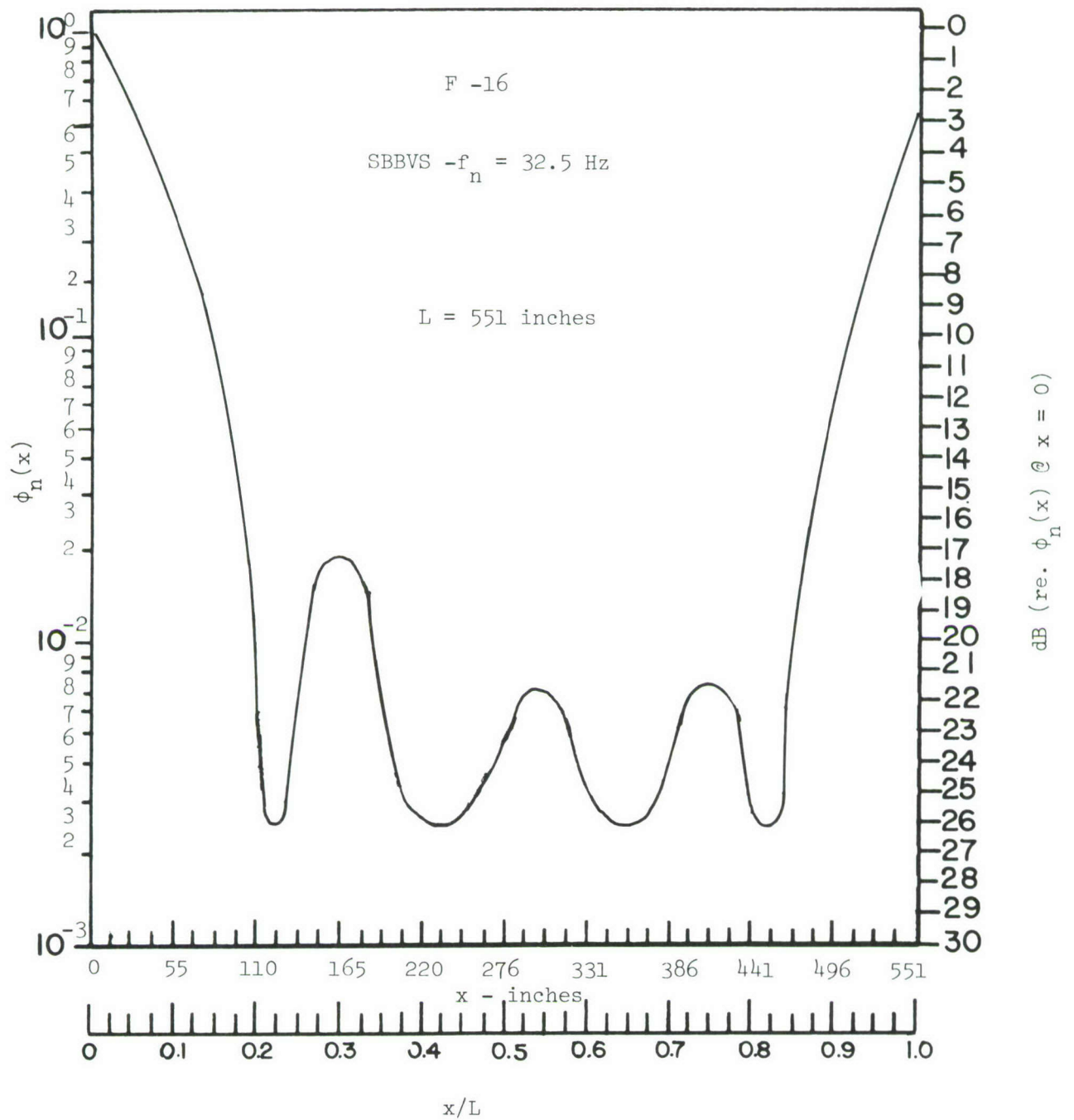
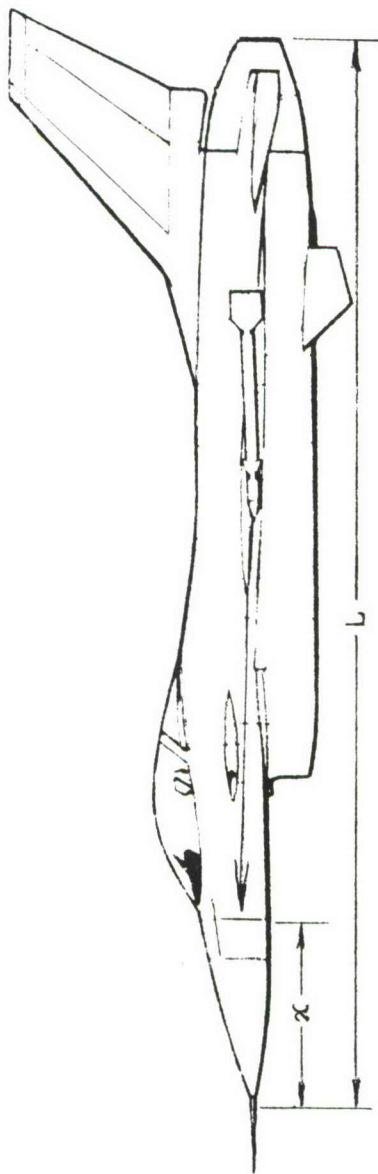


Figure B-2. Mode Shape (SBBVS) of the F-16



Note:  $x=0$  is equivalent to F.S. = 0 inches

Figure B-3. F-16 Aircraft Showing the  $x$  and  $L$  Parameters



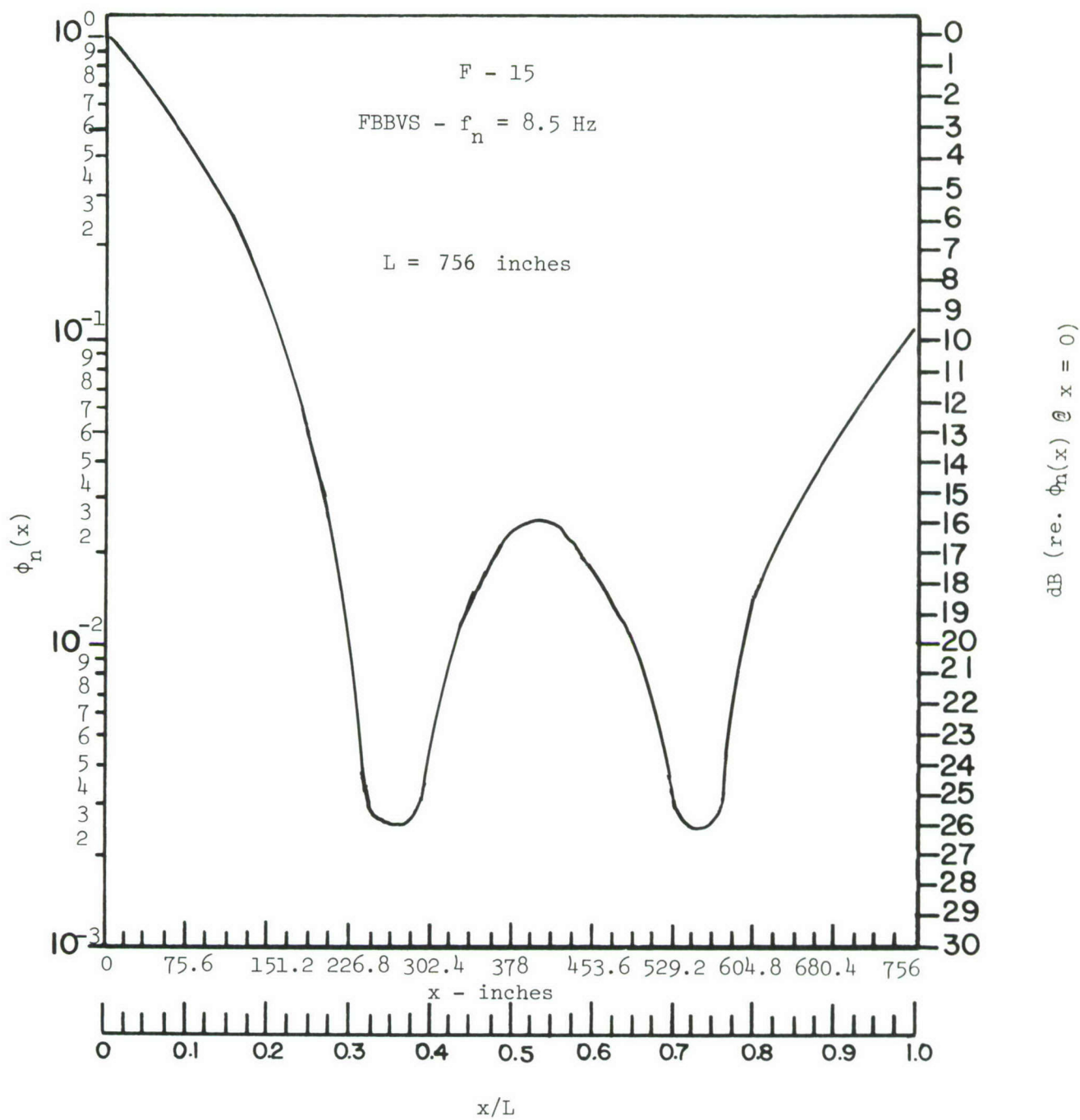


Figure B-4. Mode Shape (FBBVS) of the F-15

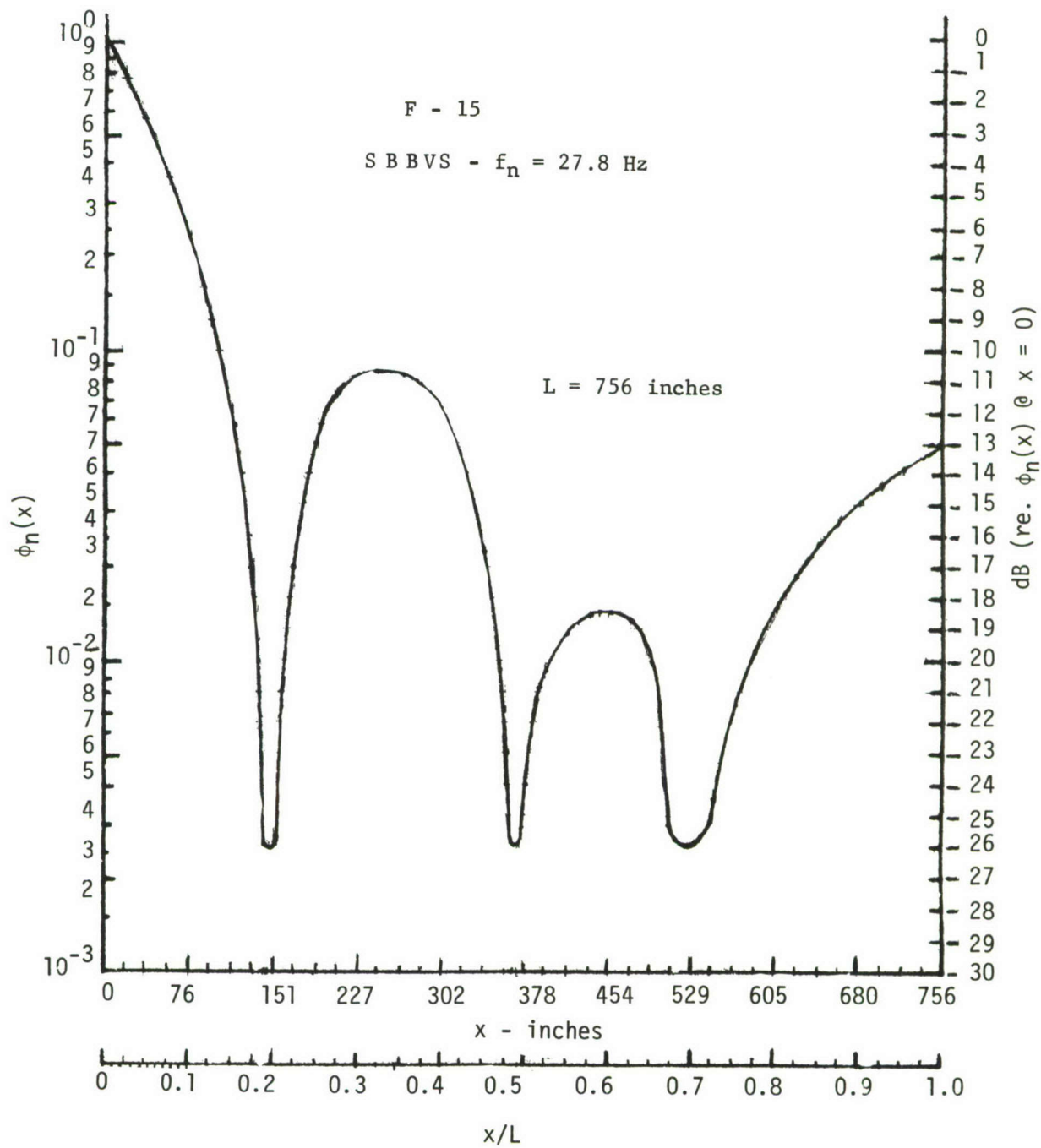
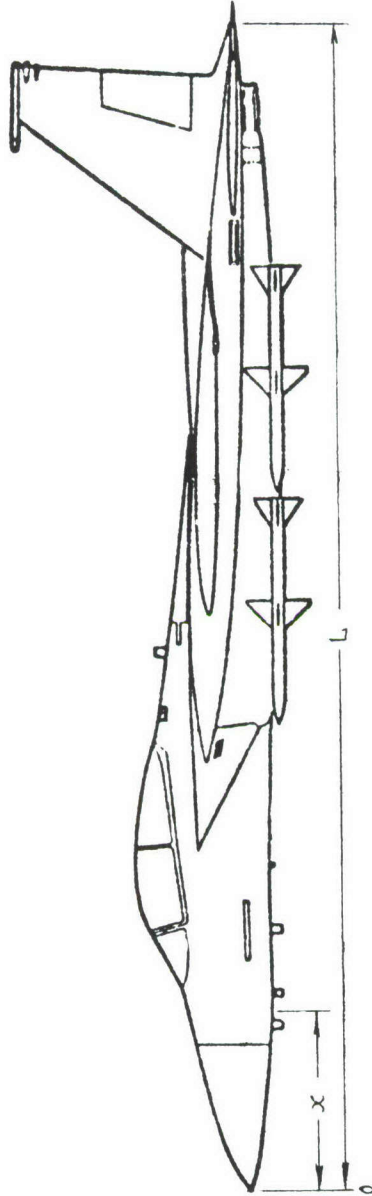


Figure B-5. Mode Shape (SBBVS) of the F-15



Note:  $x=0$  is equivalent to F.S. = 116 inches

Figure B-6. F-15 Aircraft Showing the  $x$  and  $L$  Parameters

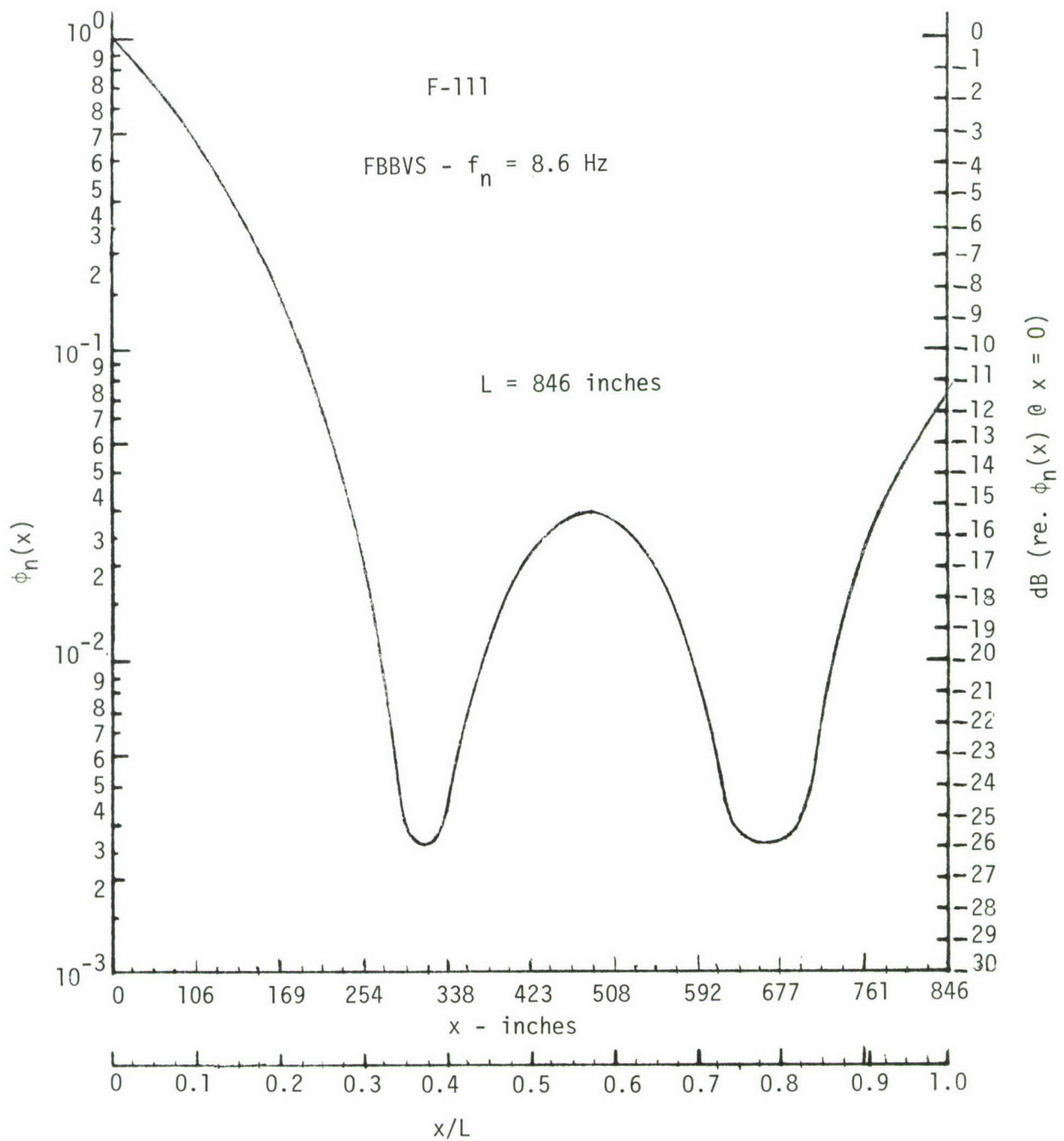
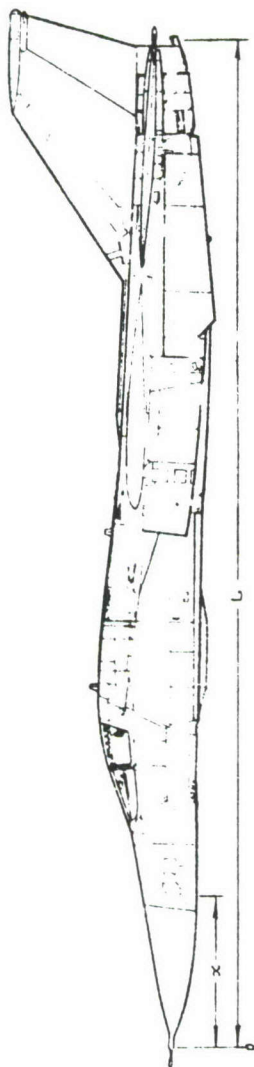


Figure B-7. Mode Shape (FBBVS) of the F-111



Note:  $x=0$  is equivalent to F.S. = 0 inches

Figure B-8. F-111 Aircraft Showing the  $x$  and  $L$  Parameters



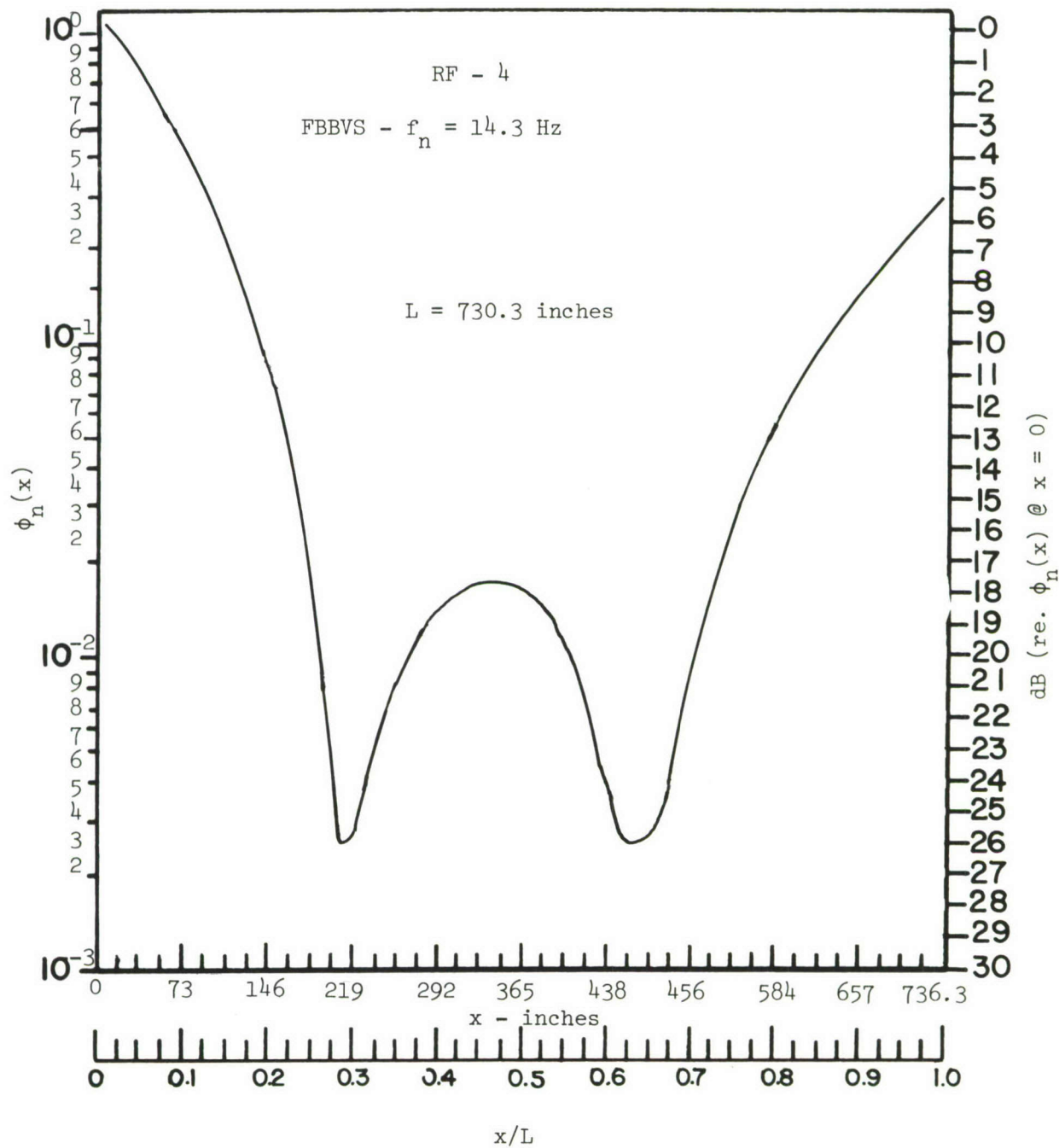


Figure B-9. Mode Shape (FBBVS) of the RF-4C

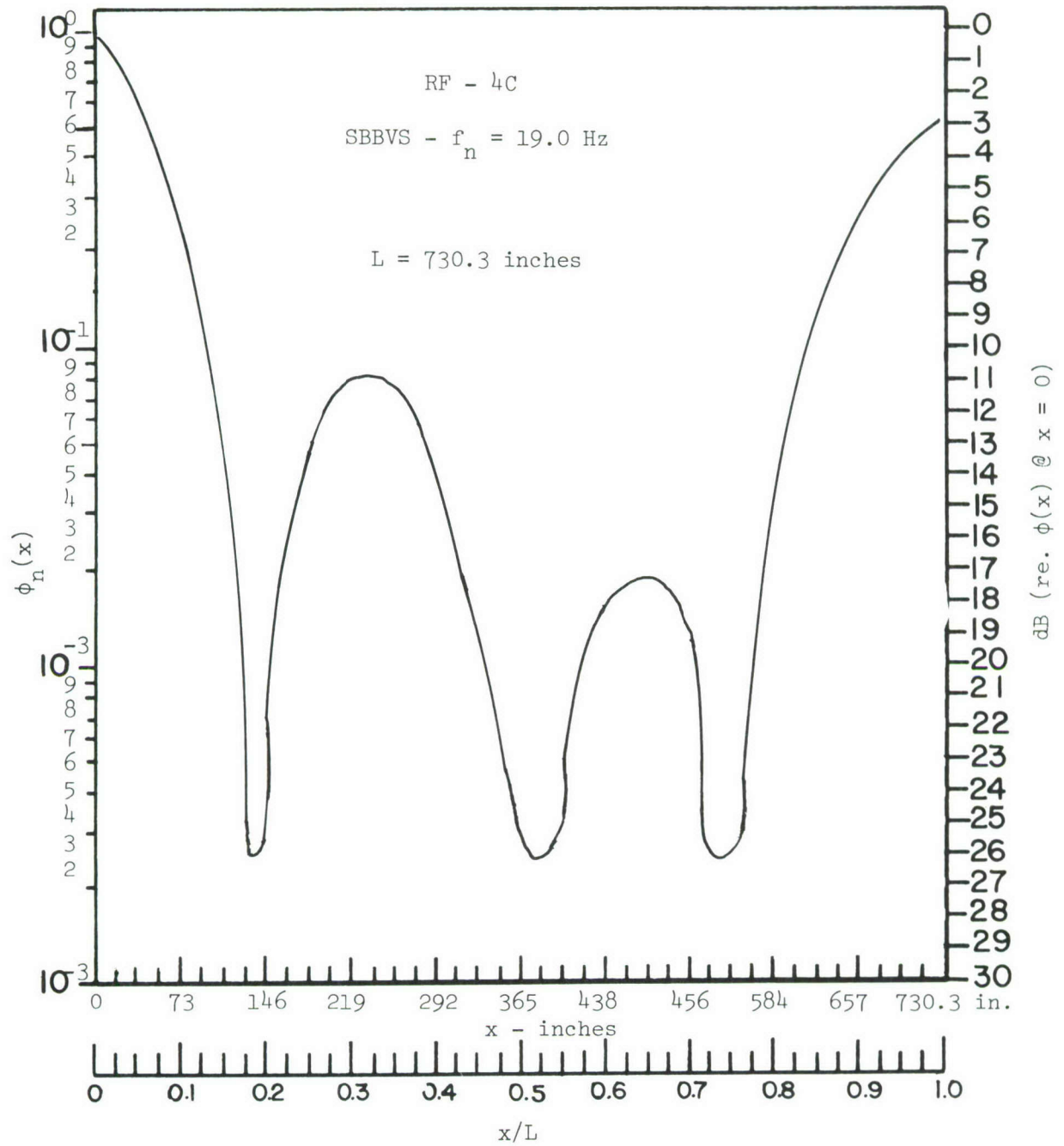
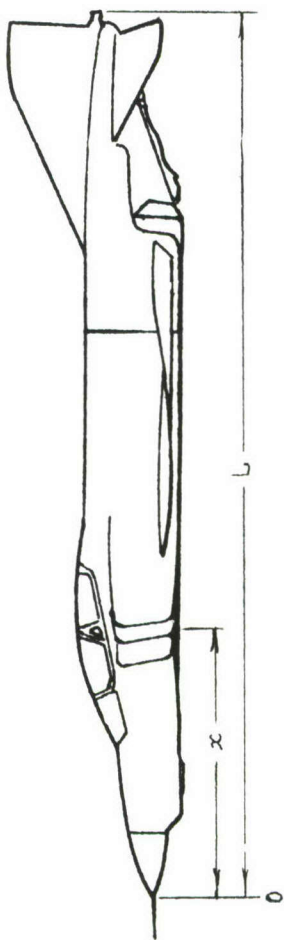


Figure B-10. Mode Shape (SBBVS) of the RF-4C



Note:  $x=0$  is equivalent to F.S. = -59 inches

Figure B-11. RF-4C Aircraft Showing the  $x$  and  $L$  Parameters

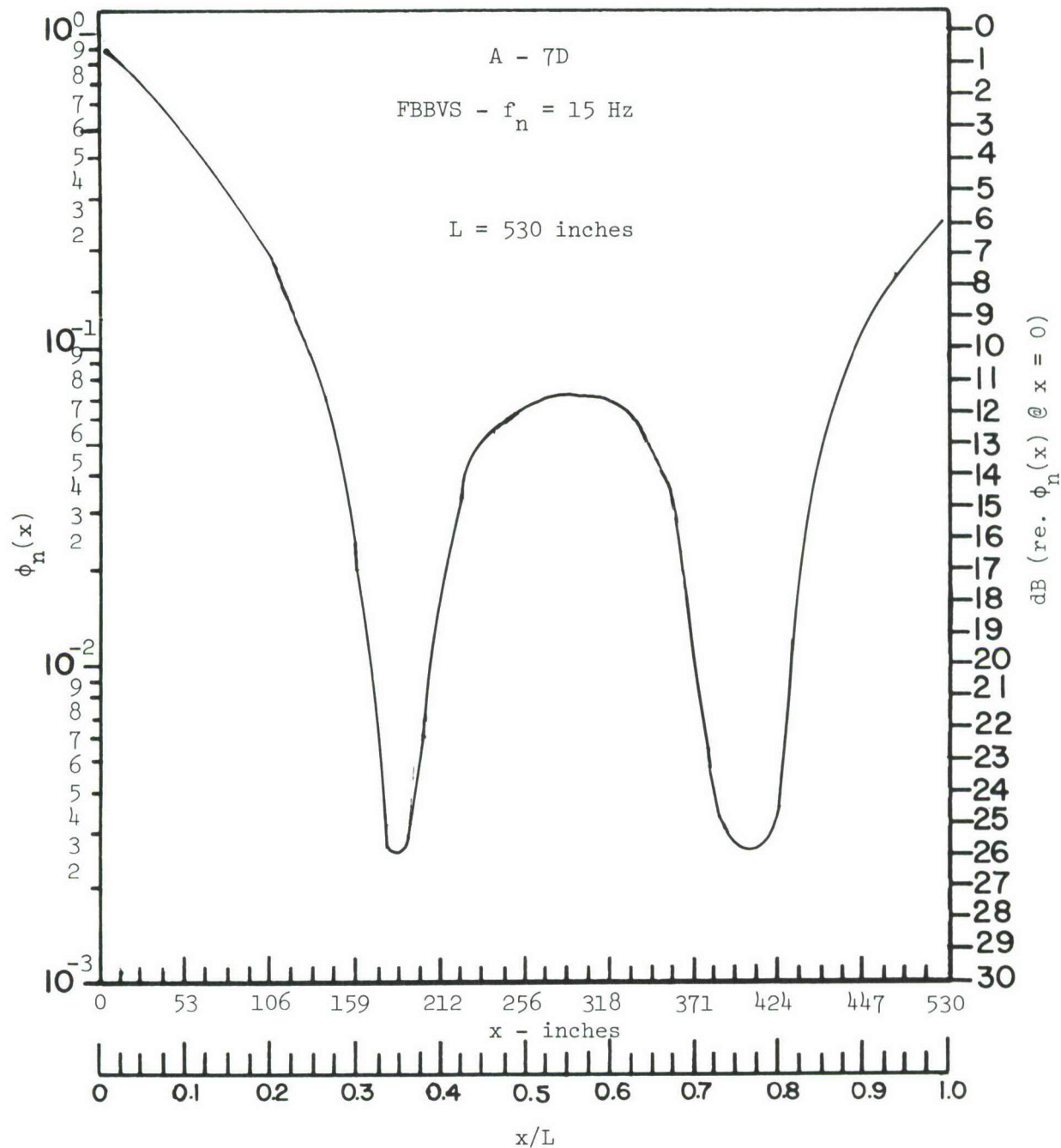


Figure B-12. Mode Shape (FBBVS) of the A-7D

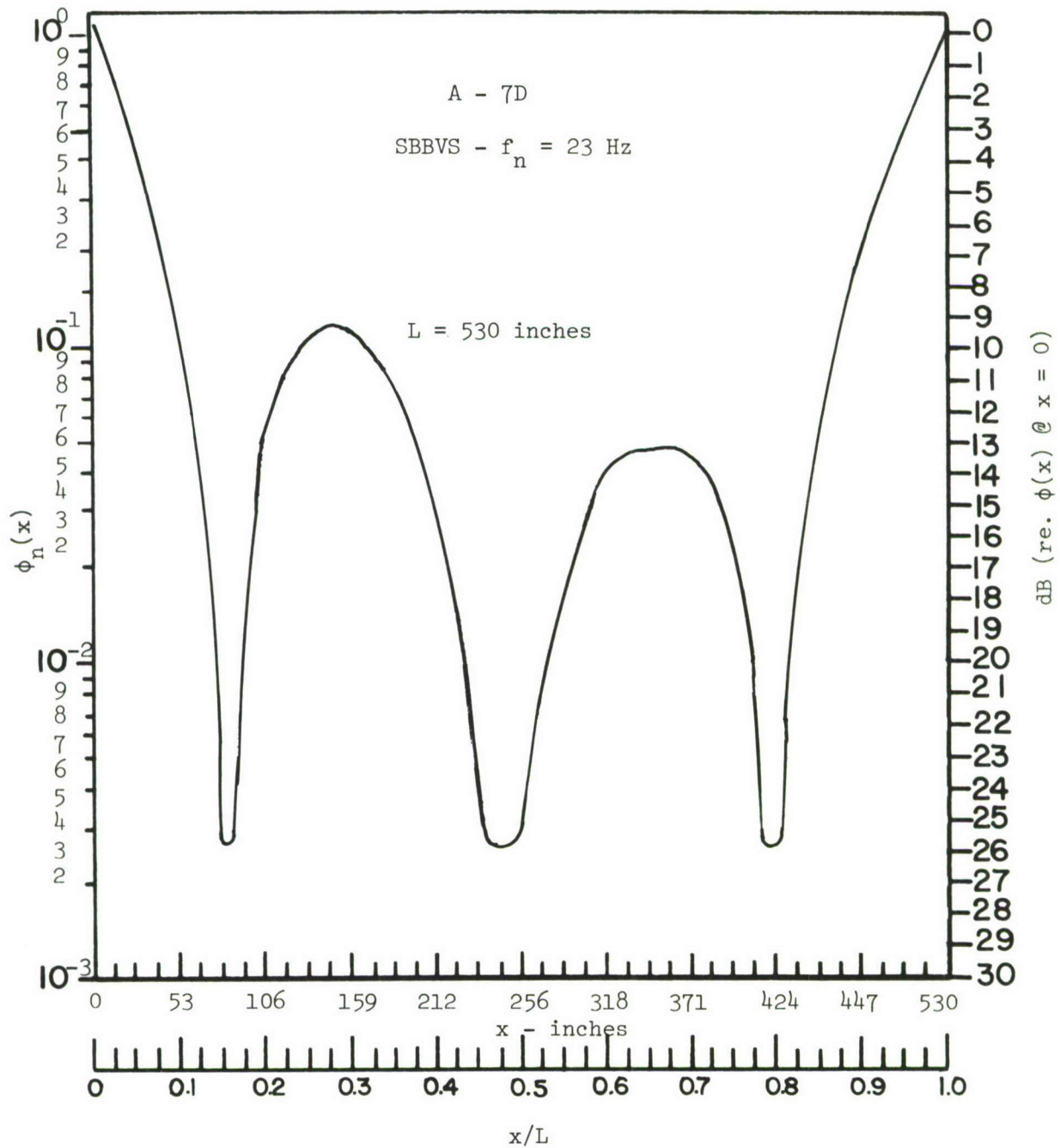
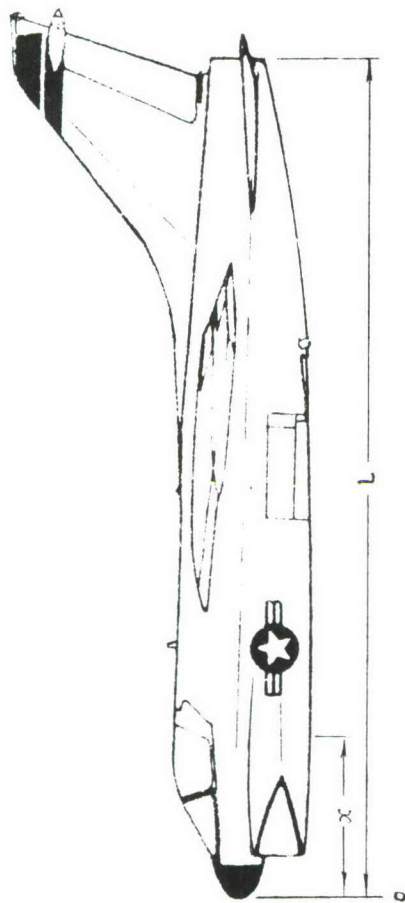


Figure B-13. Mode Shape (SBBVS) of the A-7D





Note:  $x=0$  is equivalent to F.S. = 182 inches

Figure B-14. A-7D Aircraft Showing the  $x$  and  $L$  Parameters

## APPENDIX C

TRANSFER FUNCTIONS --  
LOW, MEDIUM, AND HIGH FREQUENCY

The following comments offer supplementary information to that contained in the parameter blocks of the three transfer functions. Most of the topics discussed have to do with operations that are either stored or computationally integrated into the computer program format.

1.0 Low Frequency Transfer Function,  $L(f)$ 

Note that when the second mode is specified the first bending mode transfer function changes as follows:  $x'$  becomes 0.7,  $\beta'$  is changed to 0.23 and  $f_o$  assumes  $1.54f_n$ . The second bending mode transfer function  $L_2(f)_M$  assumes the following parameters:

$$\begin{array}{ll} f_o = f_{2n}/1.8 & f_{o'} = 1.8 f_{2n} \\ \beta = 0.2 & \beta' = 0.2 \\ x = 1.8 & x' = 0.555 \\ \alpha = 1.0 & \alpha' = 1.8 \end{array}$$

2.0 Medium Frequency Transfer Function,  $M(f)$ 

The maximum value of  $M(f)$ , which is  $M_m(f)$ , is reduced by  $\Delta M_m(f)$  as  $R_s$  approaches the skin; that is, as  $R_s$  approaches zero. This feature, stored in the program, reflects the fact that as the equipment location moves outwardly toward the region near the skin the medium frequency vibration content begins to drop out.

Some fighter aircraft feature large internal panels, the nose avionics bay of the F-111 for example; and to allow for this spectral downshift,  $L(f)$  is translated down frequency by approximately 50 Hz.

### 3.0 High Frequency Transfer Function, $H(f)$

Figure C-3(b), among other things, shows that, contrary to the behavior of  $M_m(f)$ ,  $H_m(f)$  increases as the aircraft skin is approached.

### 4.0 Special Parametric Relationships

The first and second bending modes exhibit a peaked characteristic at their mode frequencies. Whenever this happens, that is, whenever the low and high frequency rolloff segment of the flex function peak at the same frequency, say  $f_n$ , then  $f_o$  and  $f_o'$  may be defined in terms of  $f_n$ . This statement is best demonstrated by use of the following sylloge.

Always,  $xf_o = f_x$  and  $x'f_o' = f_{x'}$

where:  $f_x$  = the frequency at  $x$

and:  $f_{x'}$  = the frequency at  $x'$

Thus,  $x = f_x/f_o$  and  $x' = f_{x'}/f_o'$

Now, for the peaking case in which  $f_x = f_n = f_{x'}$ , it follows that

$$xf_o = f_n = x'f_o',$$

And so,  $f_o = f_n/x$  and  $f_o' = f_n/x'$

As observed earlier, the peaking form of the flex function appears for bending mode applications; it also appears in the description of the medium frequency transfer function,  $M(f)$  -- only to reappear once again as the limiting case for  $H_m(f)$  when  $R_s$  and  $W_E$  are assigned large values.

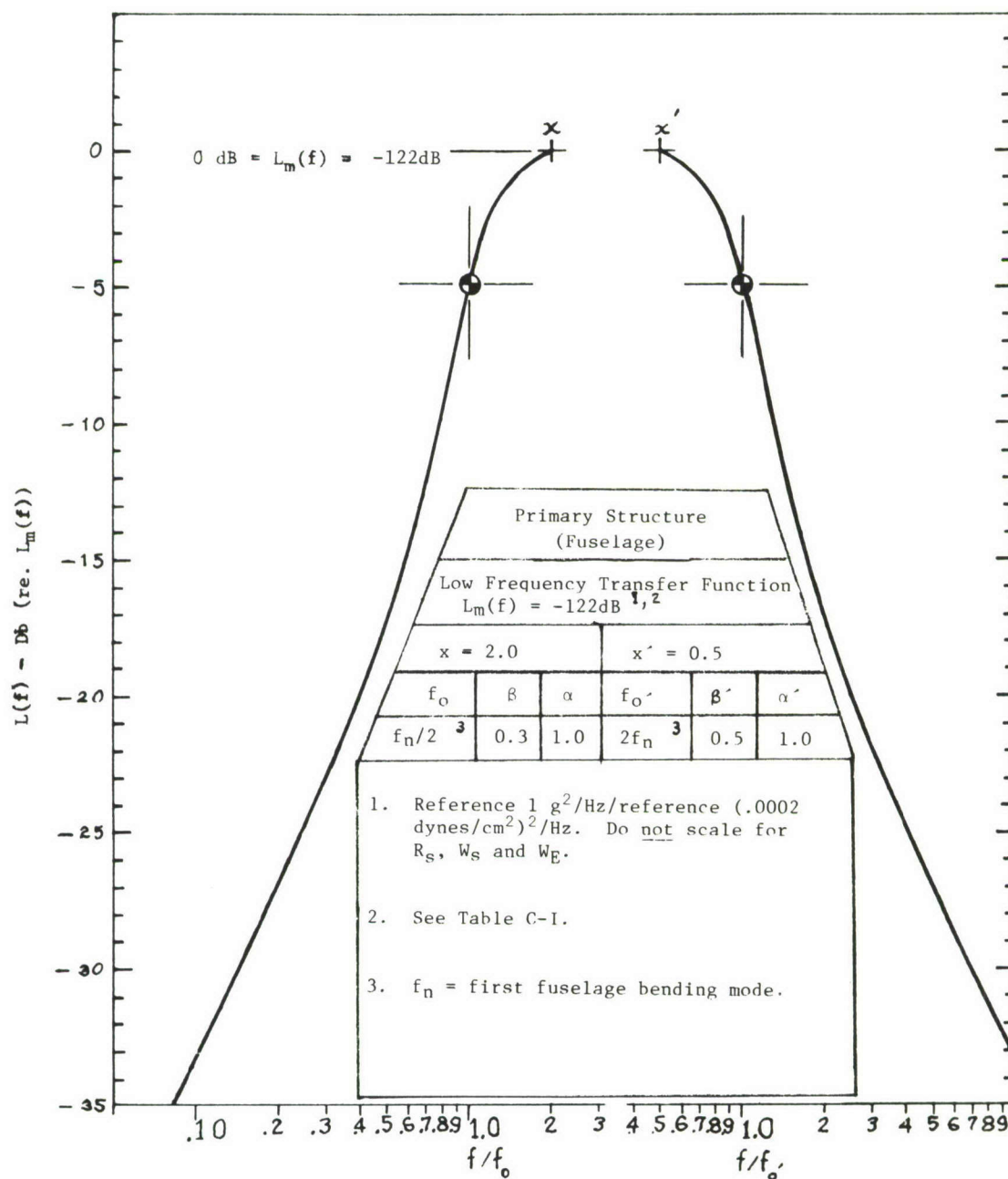


Figure C-1. Low Frequency Transfer Function,  $L(f)$ , for Fighter Aircraft Fuselage

TABLE C-1

PARAMETRIC VALUES FOR FIRST AND SECOND BENDING MODES\*  
(AIRCRAFT FUSELAGE)

## First Bending Mode

<u>Aircraft Type</u>	<u><math>L_m(f)_1</math> (dB)</u>	<u><math>f_n</math> (Hz)</u>
RF-4C	-122	14.3
F-16	-131	12.9
F-111	-134	8.5
A-7D	-129	15.2
F-15	-127	8.5

## Second Bending Mode

<u>Aircraft Type</u>	<u><math>L_m(f)_2</math> (dB)</u>	<u><math>f_{2n}</math> (Hz)</u>
RF-4C	-129	19.0
F-16	-133	32.5
F-111	----	----
A-7D	-140	23.0
F-15	-131	27.8

\*See Appendix B



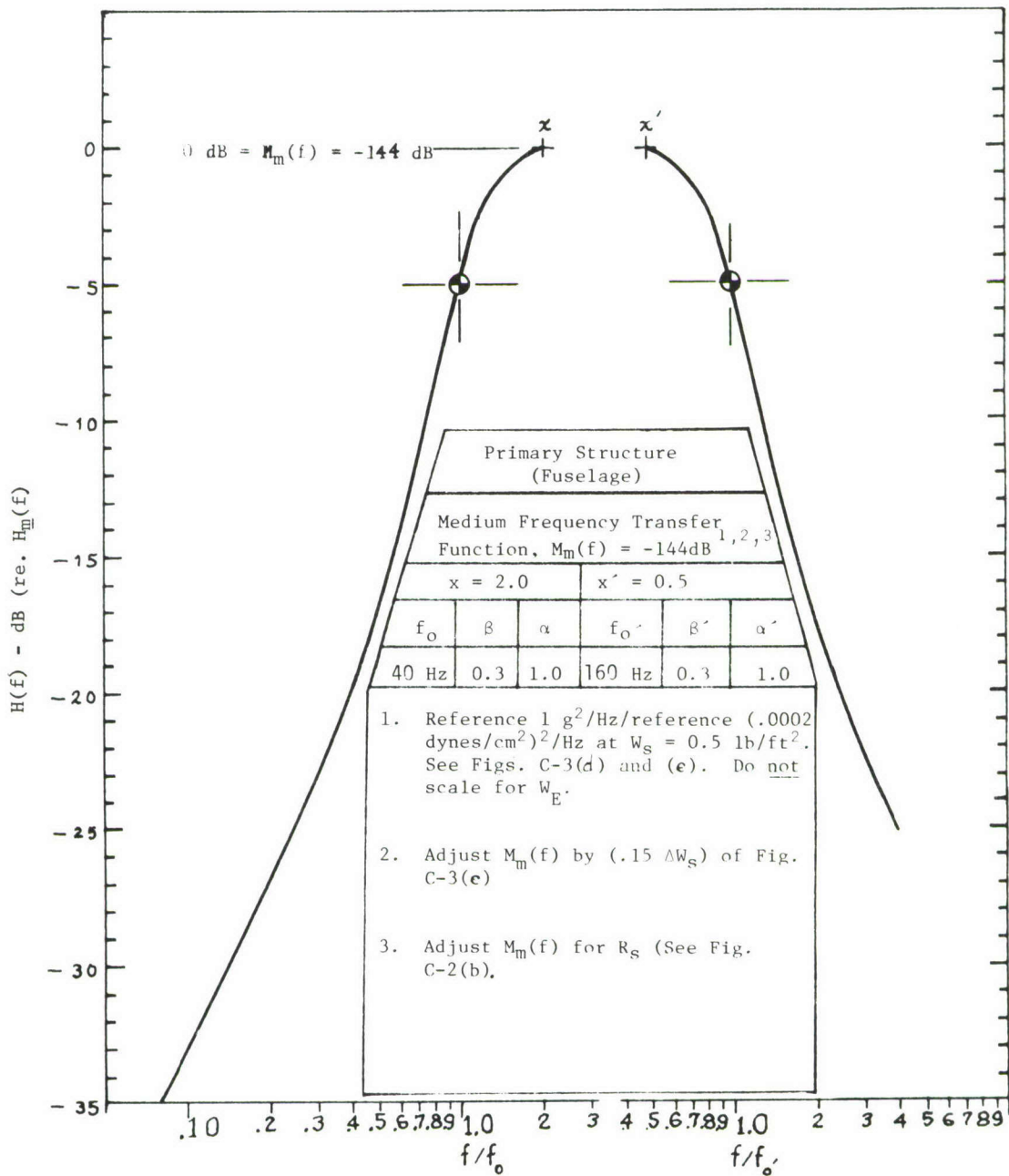


Figure C-2a. Medium Frequency Transfer Function,  $M(f)$ , for Fighter Aircraft

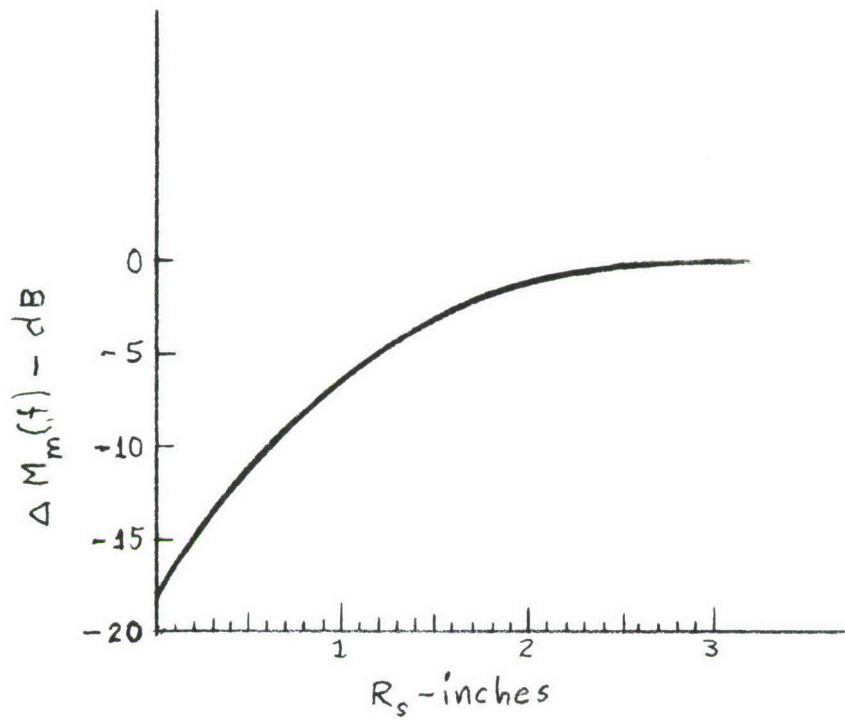
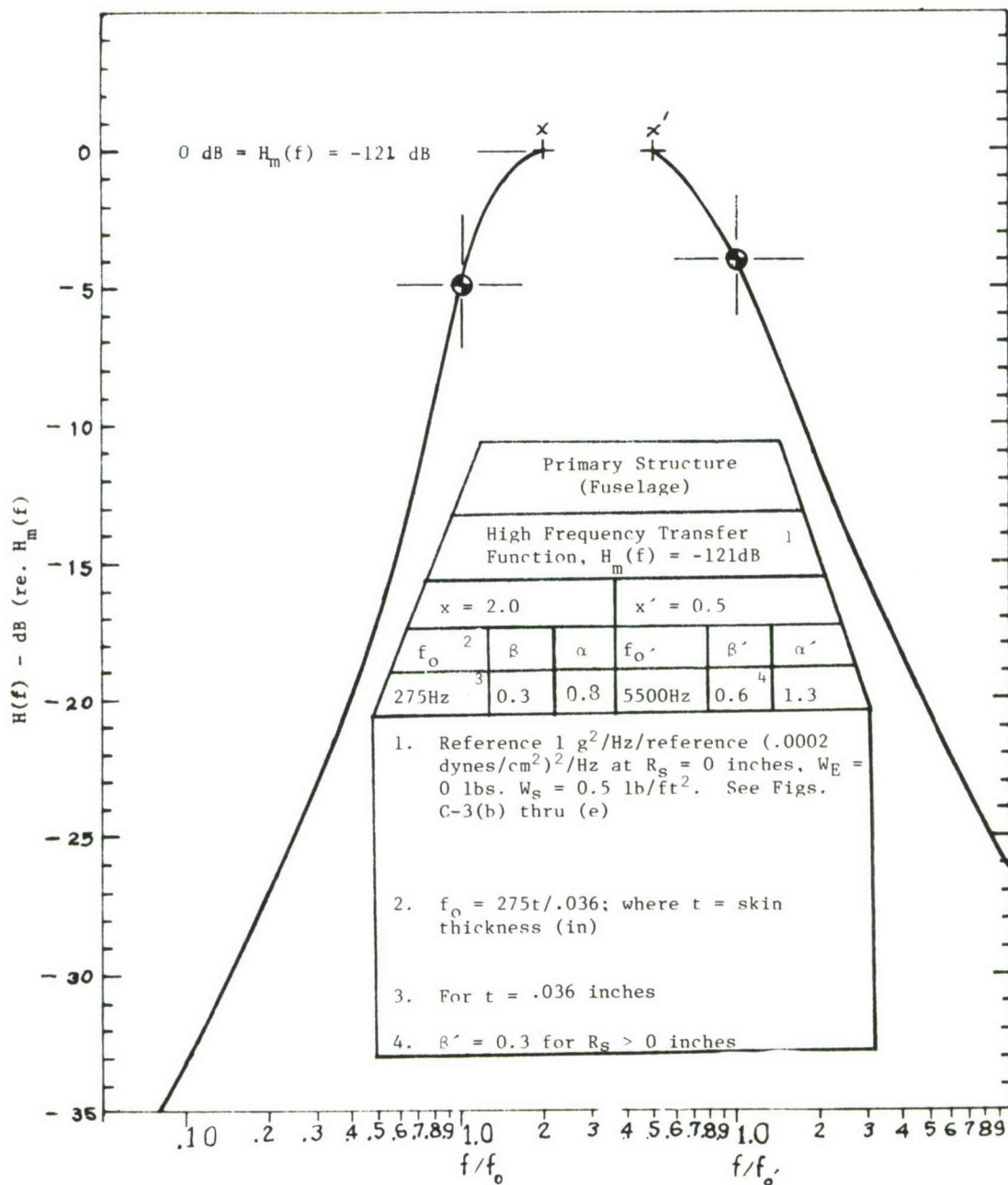


Figure C-2b. Attenuation of  $M_m(f)$  as a Function of  $R_s$

Figure C-3a. High Frequency Transfer Function,  $H(f)$ , for Fighter Aircraft

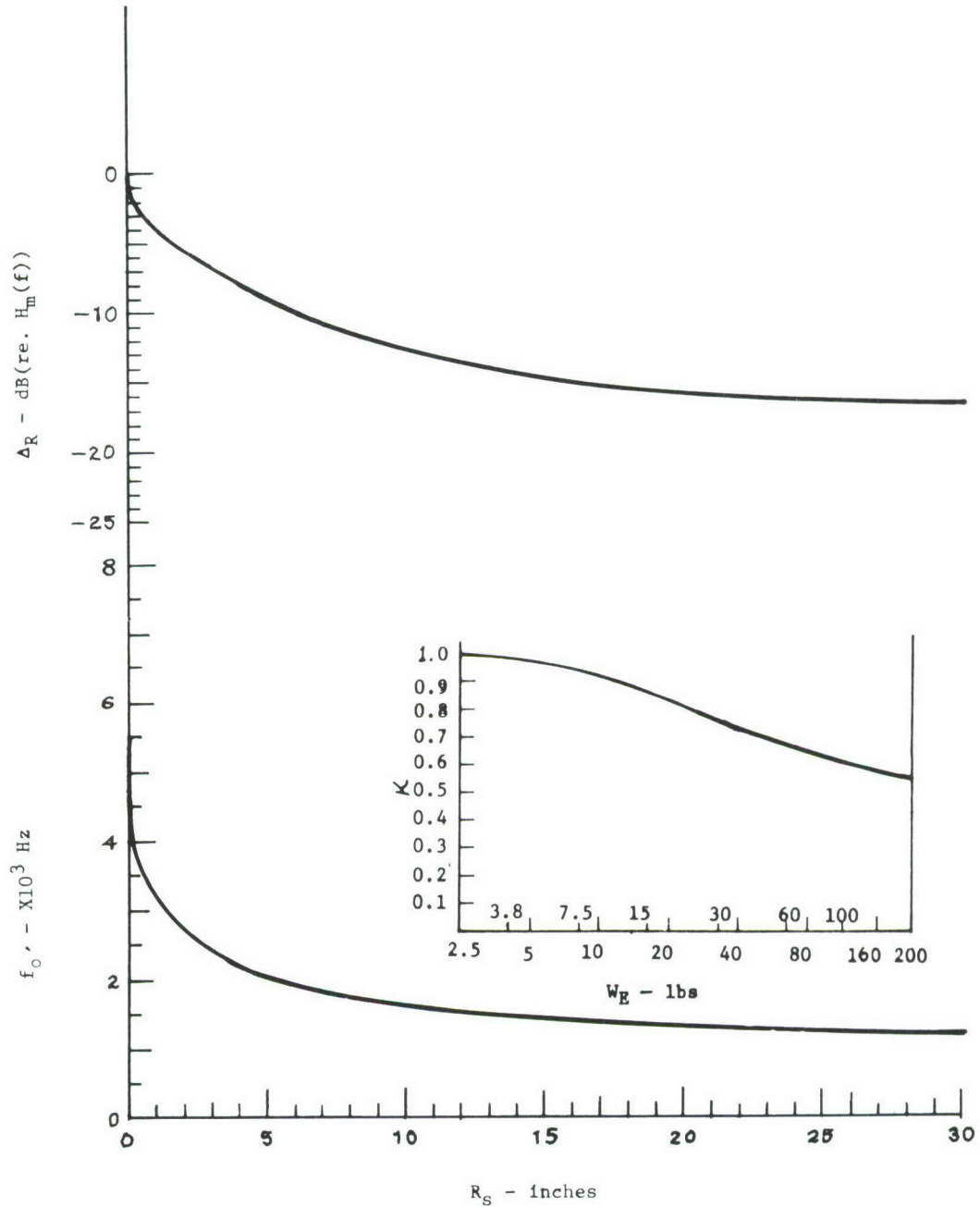


Figure C-3b. Frequency and Amplitude Attenuation of  $H_m(f)$  as a Function of  $R_s$

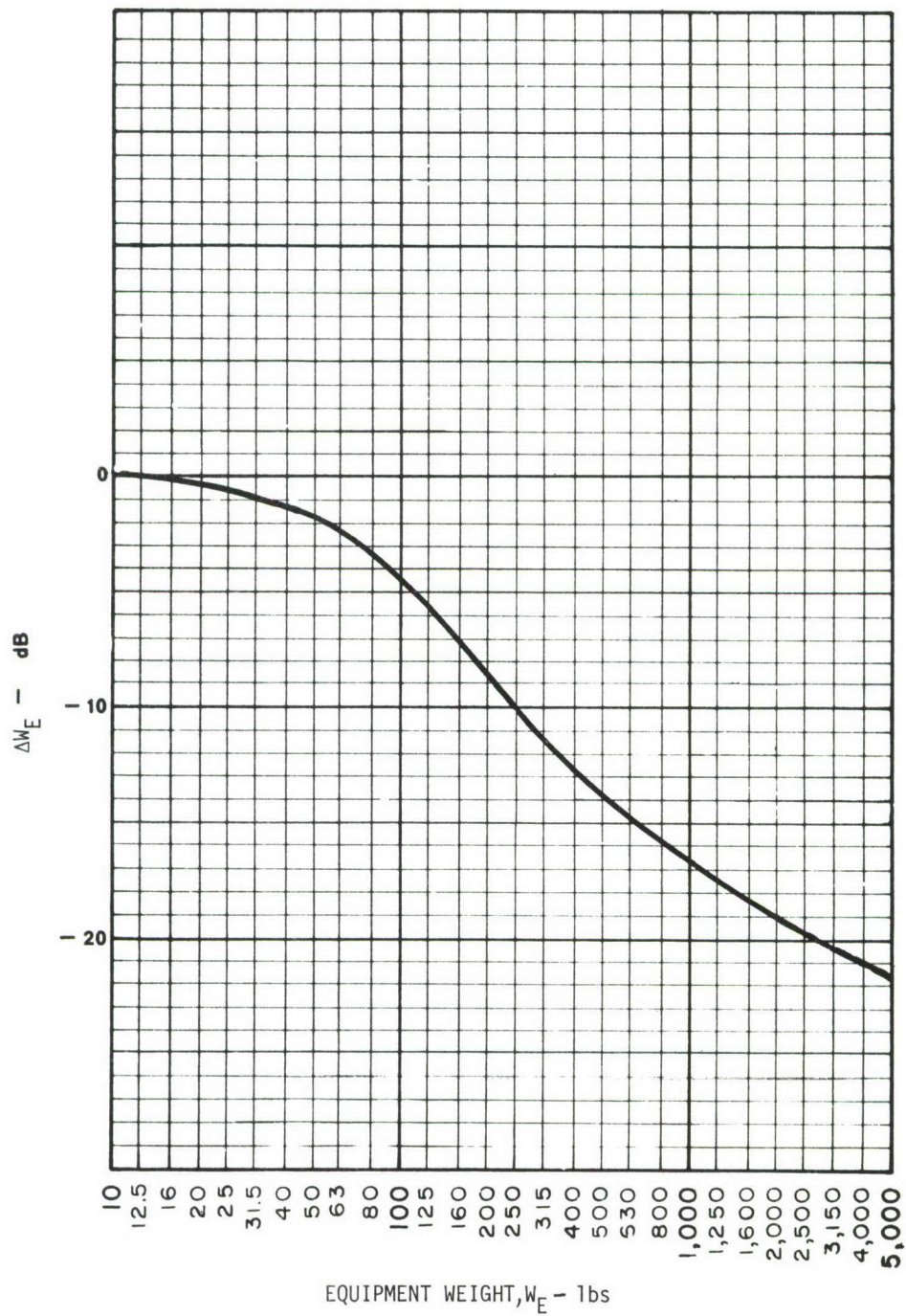


Figure C-3c. Attenuation of  $H_m(f)$  as a Function of Equipment Weight



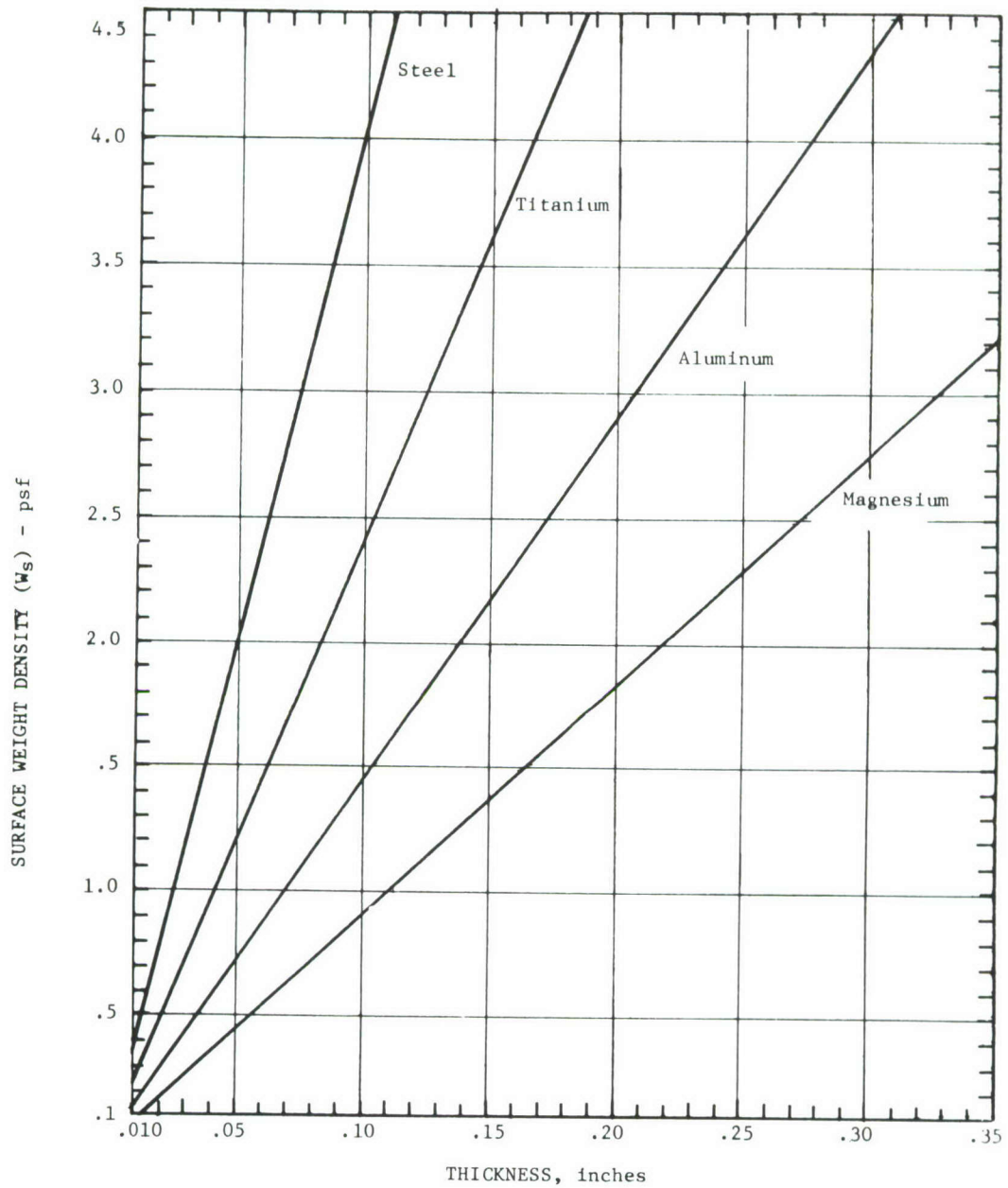


Figure C-3d. Surface Weight Density for Aircraft Materials and Their Thicknesses

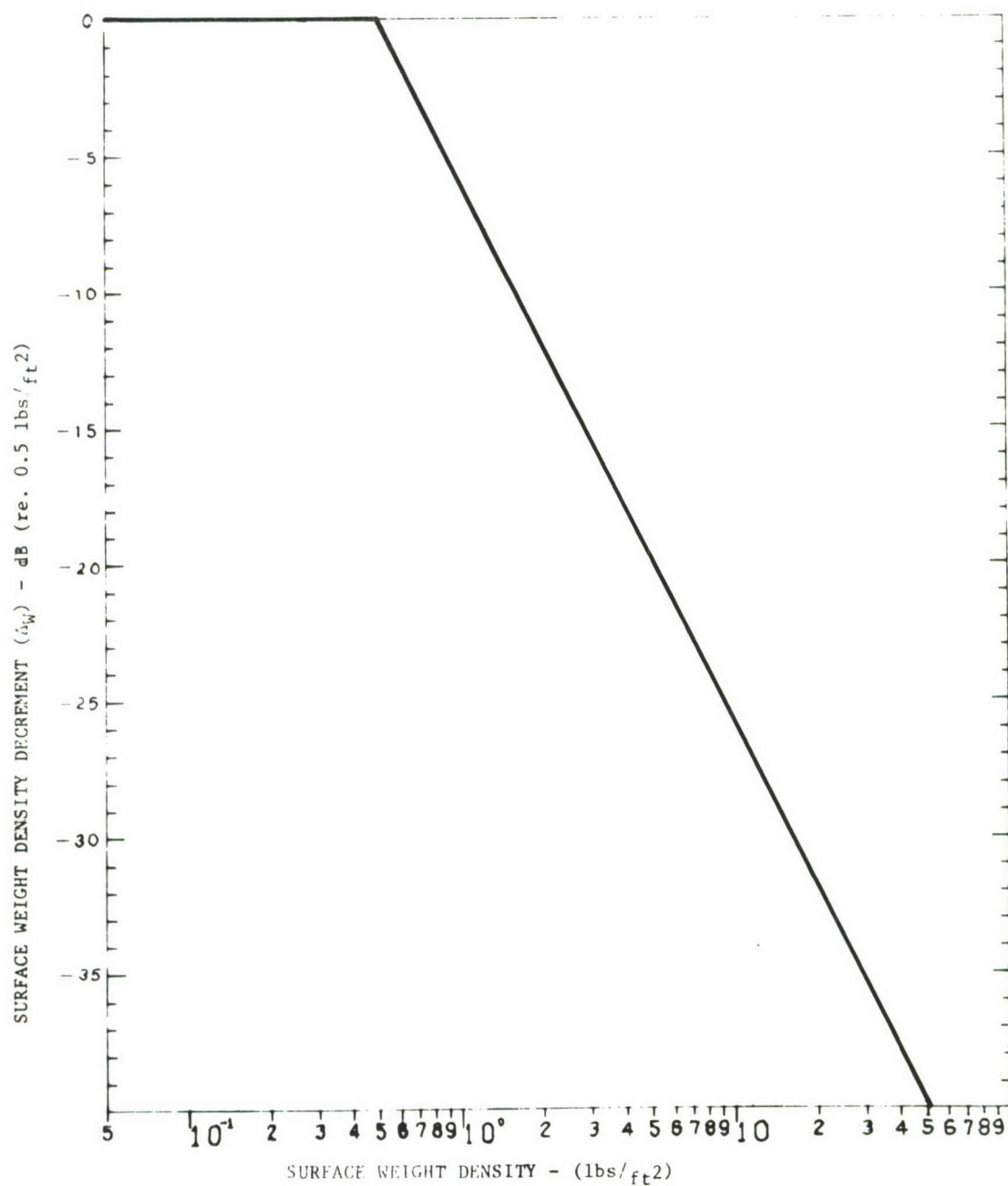


Figure C-3e. Attenuation of  $H_m(f)$  as a Function Surface Weight Density

## APPENDIX D

### SPECIAL FUNCTIONS

The purpose of the special functions is to provide an appropriate function which, after having operated on  $P(f)$ , results in a specific input to the transfer function elements that, in turn, predict the vibration input spectra of aircraft equipments during flight conditions that deviate from the smooth, straight and level norm. Such flight phases as buffet turn, pullups, takeoff, landing, rough air turbulence, proximity to open speed brakes (flaps), refueling doors, chin effects, including open weapons bay cavitations -- all of these conditions invoke special functions, a limited number of which are described in Figures D-2 through D-4.

#### 1.0 Available Functions

Four functions presently incorporated into this Appendix describe the following flight phases: buffet turn (BT), takeoff (T), landing (L), low frequency atmospheric turbulence (TB). Several of the special functions involve a series of distance parameters listed in Table D-1 and illustrated in Figure D-1.

#### 1.1 Buffet Turn

This excitation results from tight, high g turns that appear only infrequently in the fighter mission profile. The resultant levels, however, are sufficiently severe (see Figure D-2) to warrant inclusion. Note that excitations arising from pullups, speed brakes, flaps, landing gears, and open refueling doors belong

TABLE D-I

Downstream Distance ( $x$ )<sup>\*</sup> for Special  
Functions  $S_{BT}(f)$ ,  $S_T(f)$  and  $S_L(f)$

<u>Aircraft</u>	<u><math>x_{BT}</math></u>	<u><math>x_T</math></u>	<u><math>x_L</math></u>
F-4	32.3	35.3	35.3
F-111	38.1	47.7	47.7
F-16	27.1	29.5	29.5
F-5	27.7	28.3	28.3
A-7D	20.5	25.4	25.4
F-15	39.1	40.2	40.2

\*in feet

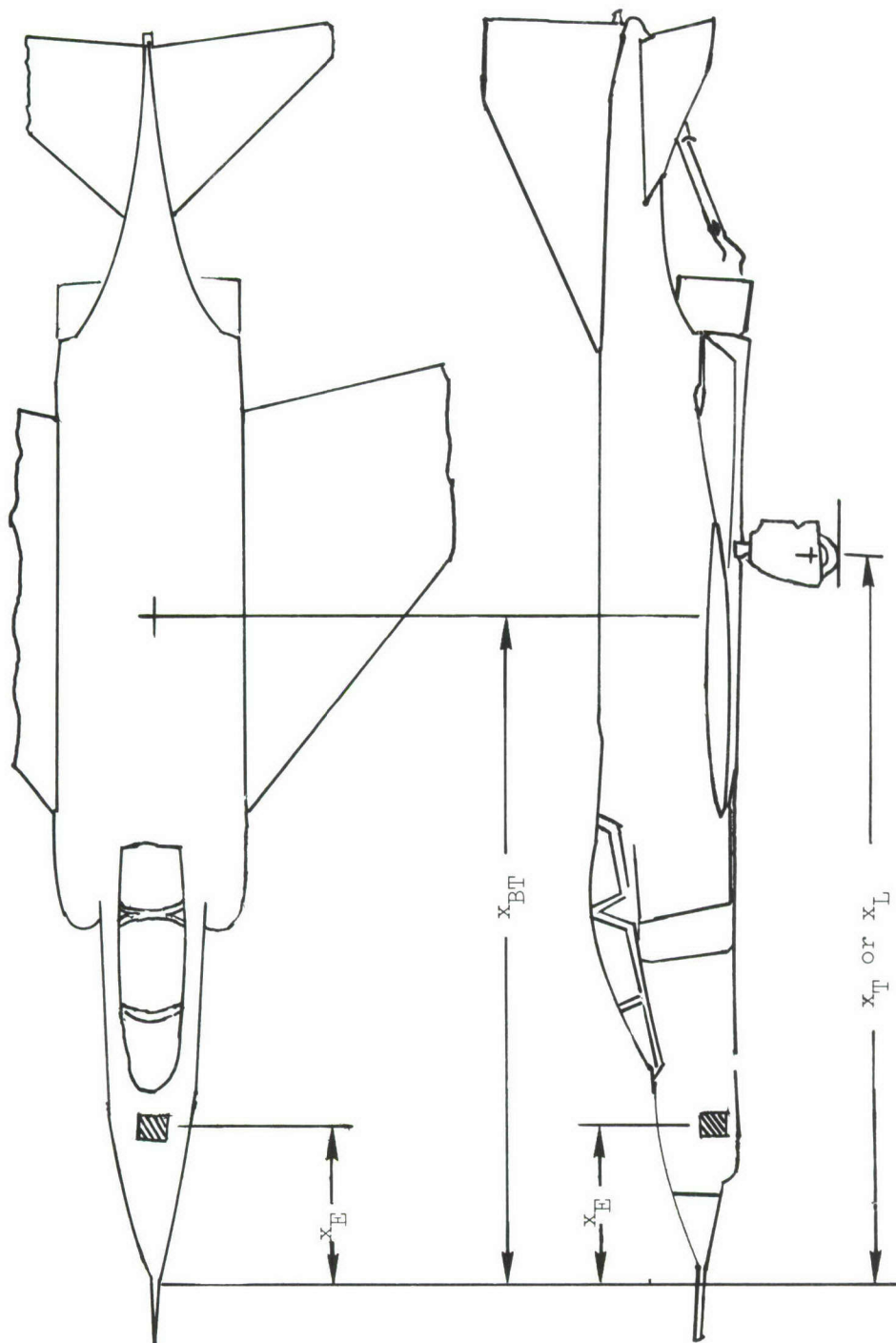


Figure D-1. Location on Aircraft of  $x_{BT}$ ,  $x_T$ ,  $x_L$



in this family of special functions. They have not, as yet, been synthesized for the current computer program. The pullup phase (PU), be it noted, is, in its main characteristics, sufficiently close to that of the BT phase to allow temporary substitution.

## 1.2 Takeoff

$S_T(f)$  is derived from F-4 data and is referenced to that aircraft at the straight and level flight conditions noted in Figure D-4. Although this approach may be suitable as an approximation for most predicted results, it is prudent to add  $10 \log_{10} T_{\max}/5 \times 10^4$  to the high frequency portion (see  $H(f)$ ) of the final predicted spectrum when the aircraft features engines with a maximum thrust,  $T_{\max}$ , appreciably greater than 50,000 lbs. Note that this last provision has not yet been entered into the computer program.

## 1.3 Landing

$S_L(f)$  emphasizes the excitation of the fuselage second bending mode (vertical); otherwise there is no great distinction to this flight phase.

## 1.4 Low Frequency Atmospheric Turbulence

This function is, in effect, added to the SANDL flight phase of the aircraft to provide emphasis in the low frequency regime. Simulation of rough air characteristics is the objective of this special function and may be used in conjunction with  $P(f)$  at any altitude and mach combination so long as the flight conditions are straight and level.

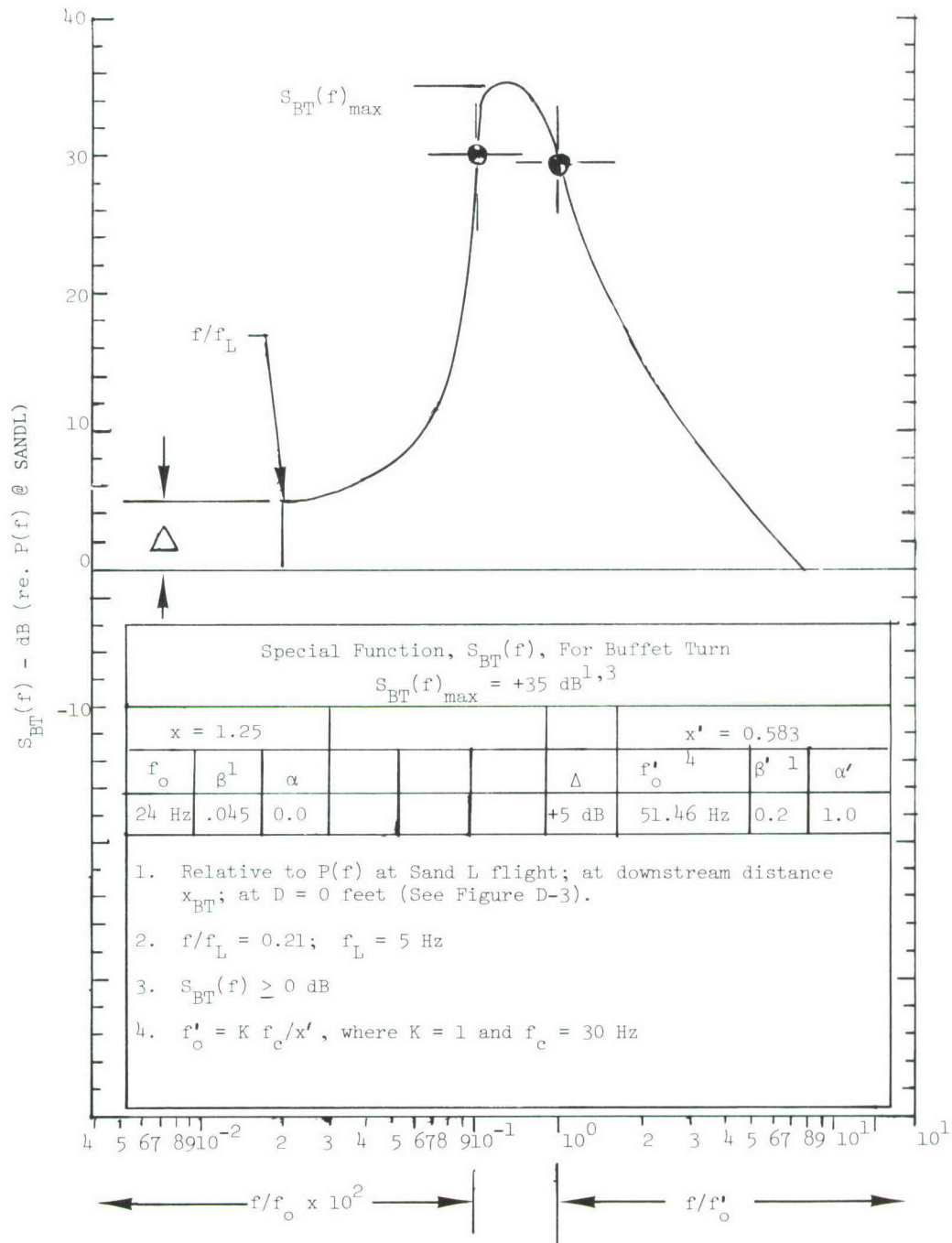


Figure D-2. Special Function,  $S_{BT}(f)$ , for Buffet Turn

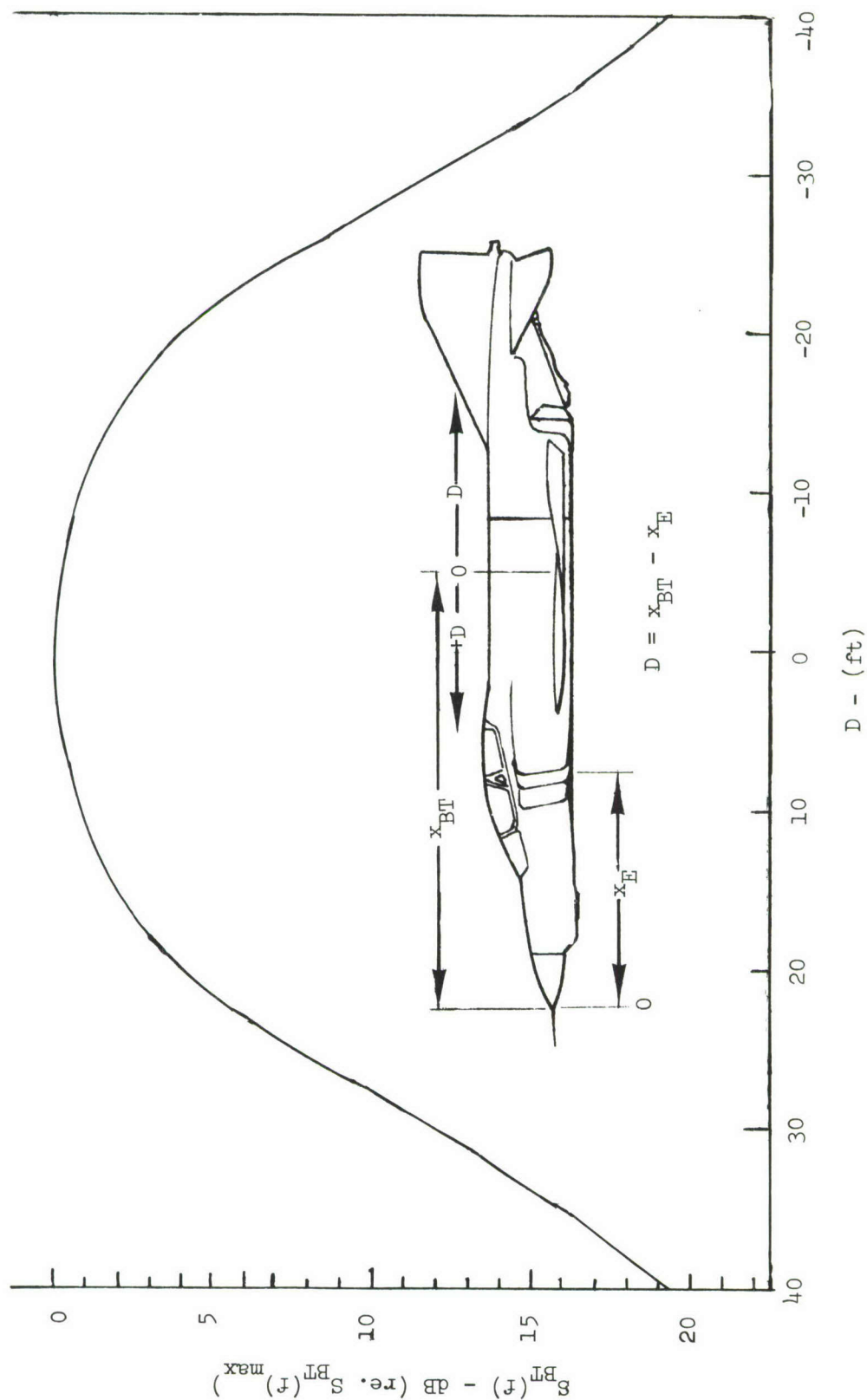


Figure D-3. Location on Aircraft of D Parameter

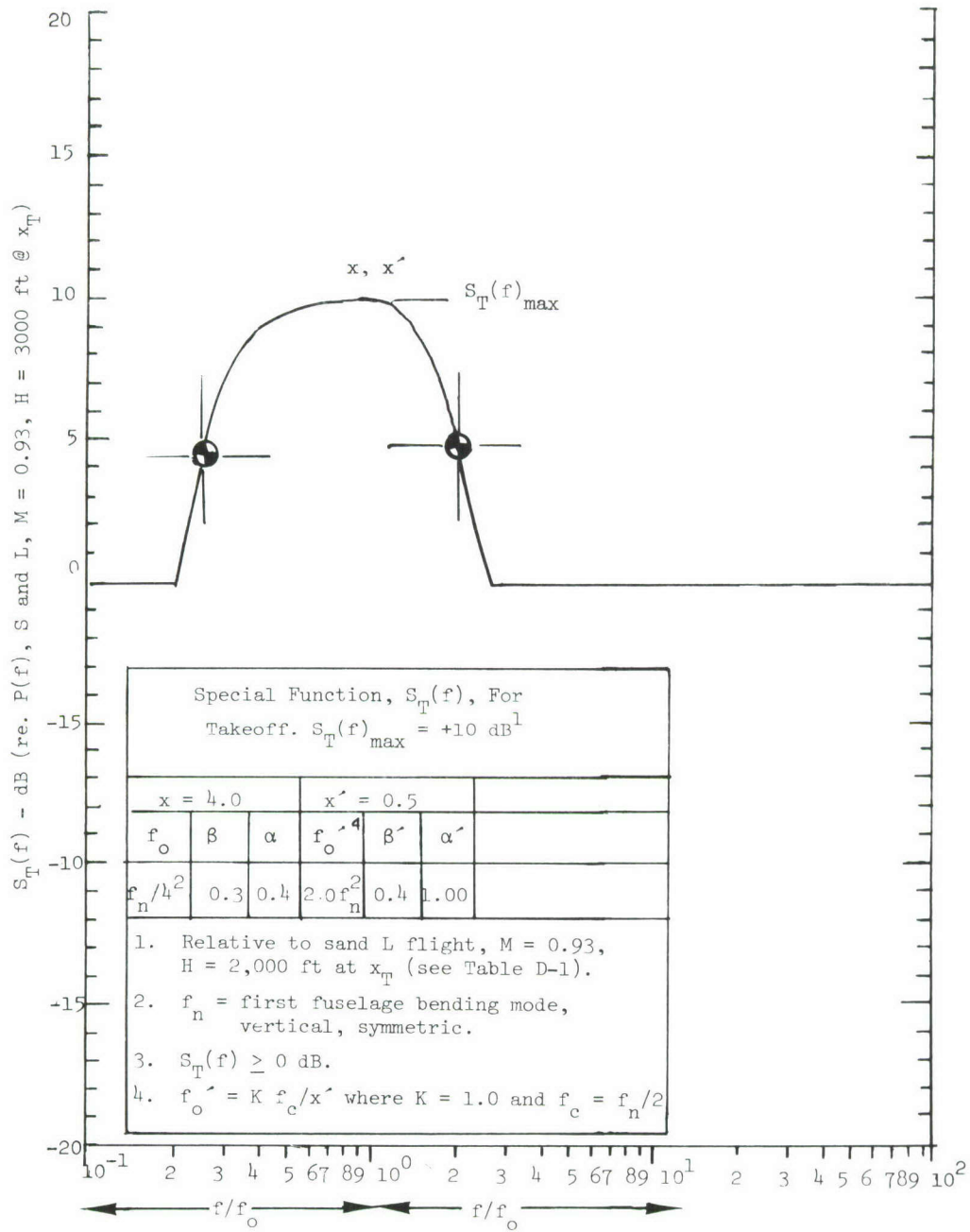
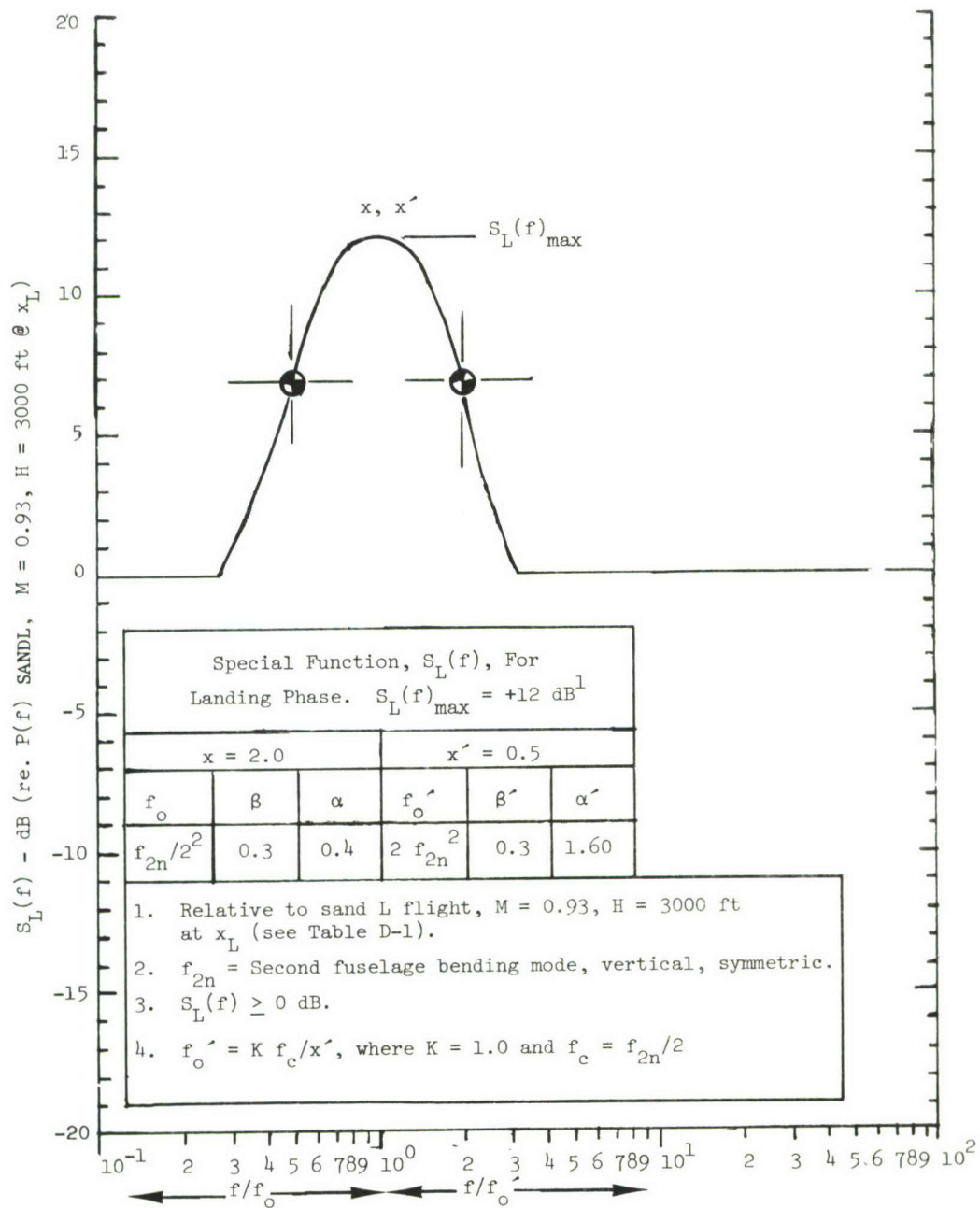


Figure D-4. Special Function,  $S_T(f)$ , for Takeoff

Figure D-5. Special Function,  $S_L(f)$ , for Landing

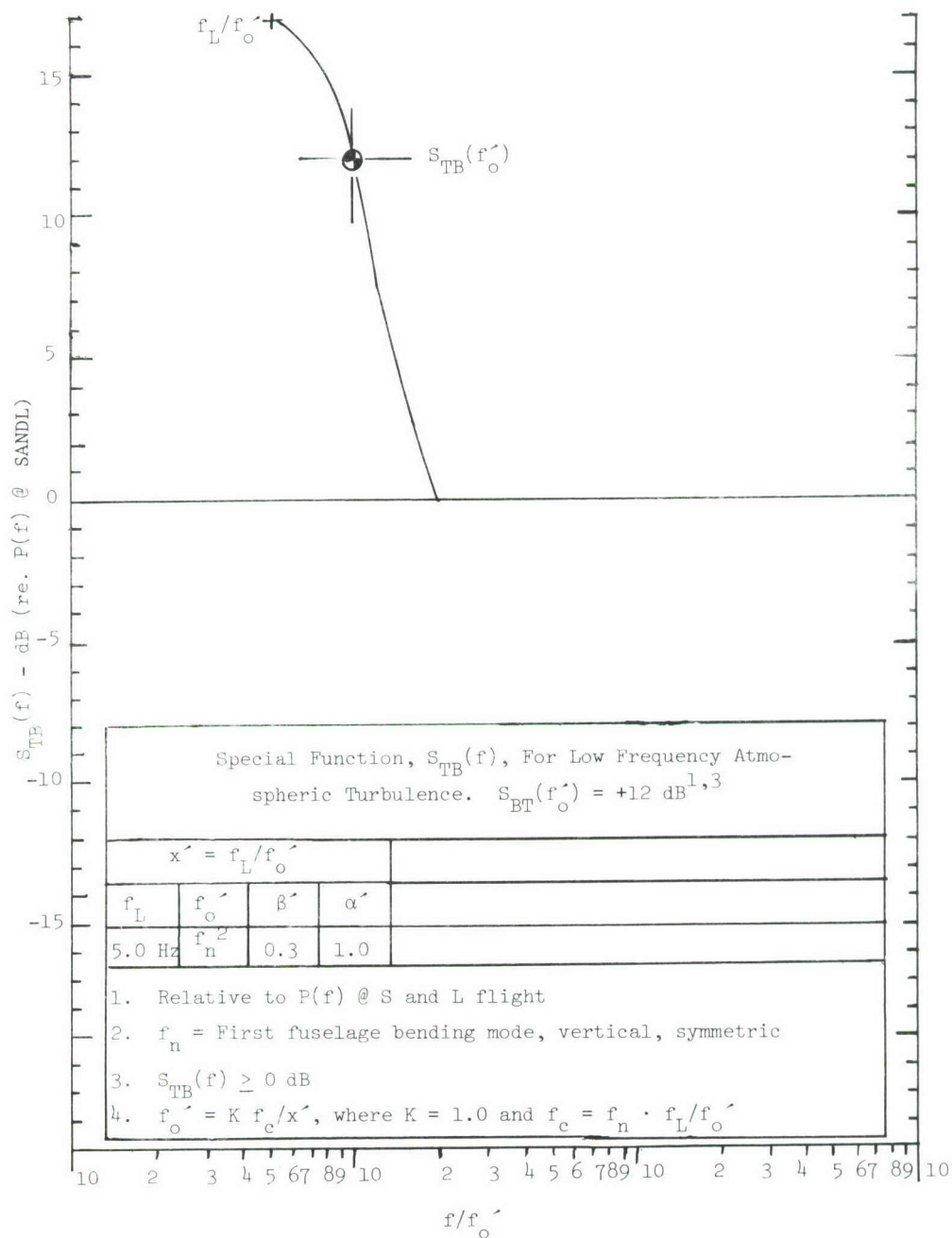


Figure D-6. Special Function,  $S_{TB}(f)$ , for Low Frequency Atmospheric Turbulence



APPENDIX E  
EQUIPMENT MOUNTING CATEGORIES

1.0 Category Selection

Table E-1 provides a number of equipment mounting configurations that, with the possible exceptions of categories III and IV(a), represent equipment mounting methods commonly encountered in fighter aircraft. By referring to the simplified drawings of the table, the user may choose which of the configurations most closely agrees with the user's particular equipment mounting situation. Having selected a category, the user has immediate reference to the adjacent remarks column which identifies and locates the transfer function corresponding to the selected category. All such transfer functions are, of course, stored in the program card file and are automatically selected when the user identifies the category during the input steps detailed in Section III.

1.1 I(b), A Special Case

Note that Category I(b) is simply the high frequency transfer function,  $H(f)$ , and represents the only case when  $H_m(f)$  is corrected for the equipment mass loading,  $W_E$  (see Appendix C). Mass loading corrections for the other categories are integrated into their respective transfer functions,  $Y(f)$ ; this can be seen by referring to the associated graphs of the transfer function curves (Figures E-1 through E-5).

## 1.2 Spatial Adjustment for $R(f)$

Predicted response magnitudes of the secondary structure are based upon structural transfer functions, whose maximum values,  $Y_m(f)$ , are taken to be at the first bending antinodal point of the shelves, racks, or instrument panels (Figures E-5 and E-6). Thus  $R(f)$  represents the maximum expected response of the structure and this is usually at the midspace point. For many fighter aircraft configurations, the equipment mounting points are located rather close to the end constraints of the secondary structure. From the equipment response viewpoint, this situation represents the case where  $R(f)$  tends to approach  $G(f)$  and thereby induces the following decision criteria (not yet entered into the computer program); a criteria which allows the user a choice of responses,  $R(f)$  or  $G(f)$ .

$$\begin{array}{ll} \text{If } \epsilon \leq L/4 & \text{(see Figure E-5)} \\ \text{let } R(f) = G(f) \end{array}$$

If the above condition is obtained, then the user may reject the computer output of  $R(f)$  and select  $G(f)$ .

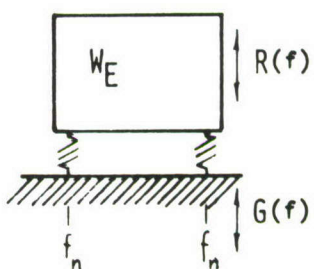
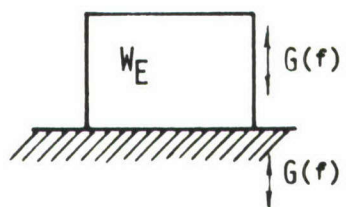
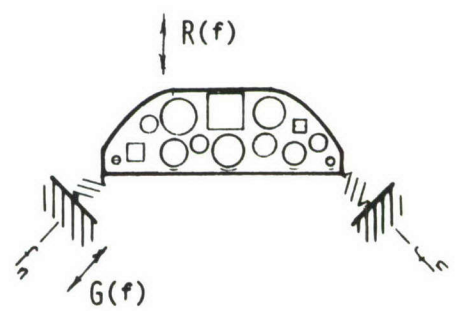
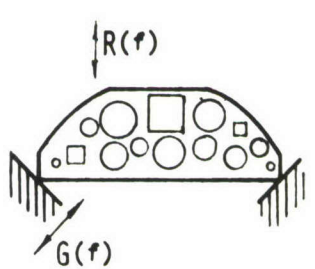
TABLE E-I Transfer Function Categories For Equipments Mounted In Fighter Aircraft		
CATEGORY		REMARKS
I(a)		See Fig. E-1(a)
I(b)		See Fig. E-1(b) and Fig. C-7
II(a)		See Fig. E-2(a) and Table E-II
II(b)		See Fig. E-2(b) and Table E-II

TABLE E-I (Cont.)

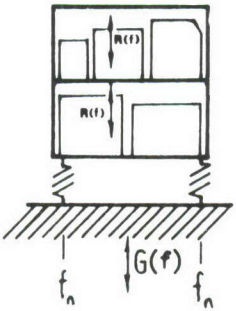
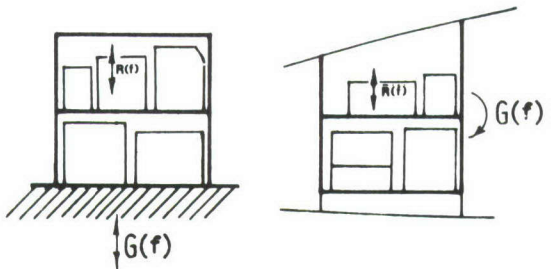
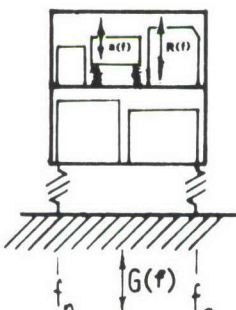
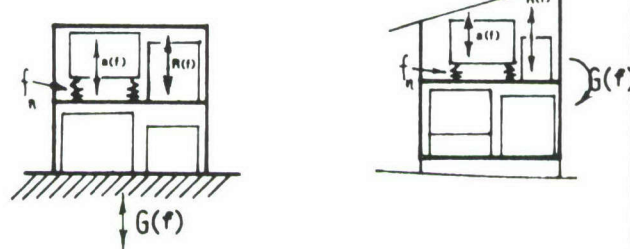
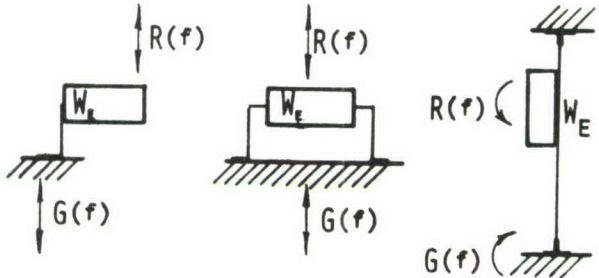
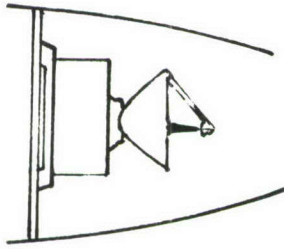
CATEGORY		REMARKS
III(a)		See Fig. E-3(a)
III(b)		See Fig. E-3(b)
IV(a)		dB wise, add Fig. E-1(a) to Fig. E- 3(a)
IV(b)		dB wise, add Fig. E-1(a) to Fig. E - 3(b)

TABLE E-I (Cont.)

CATEGORY		REMARKS
V		See Fig. E-5
VI		See Fig. E-7

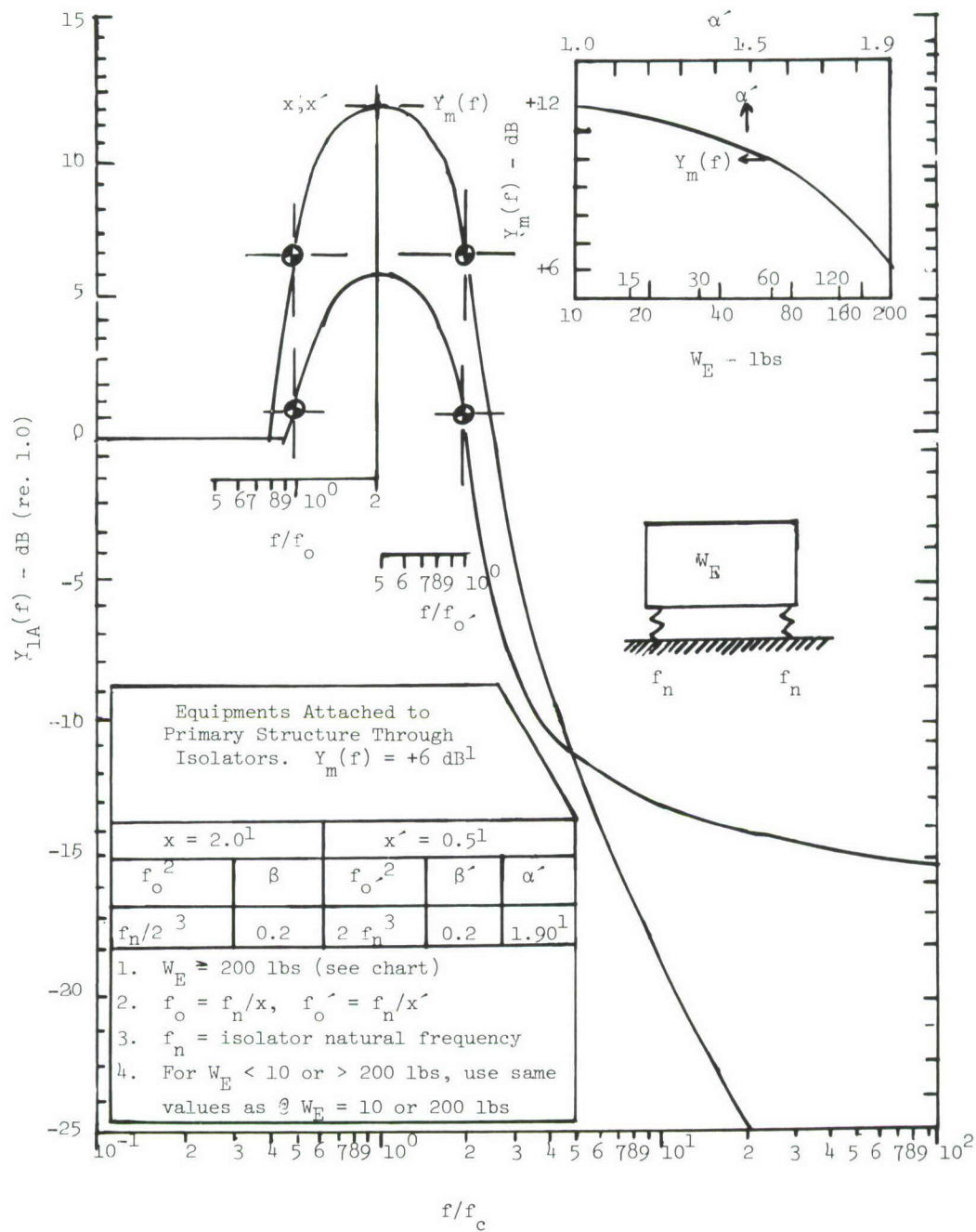


Figure E-1a. Transfer Function for Category I(a)



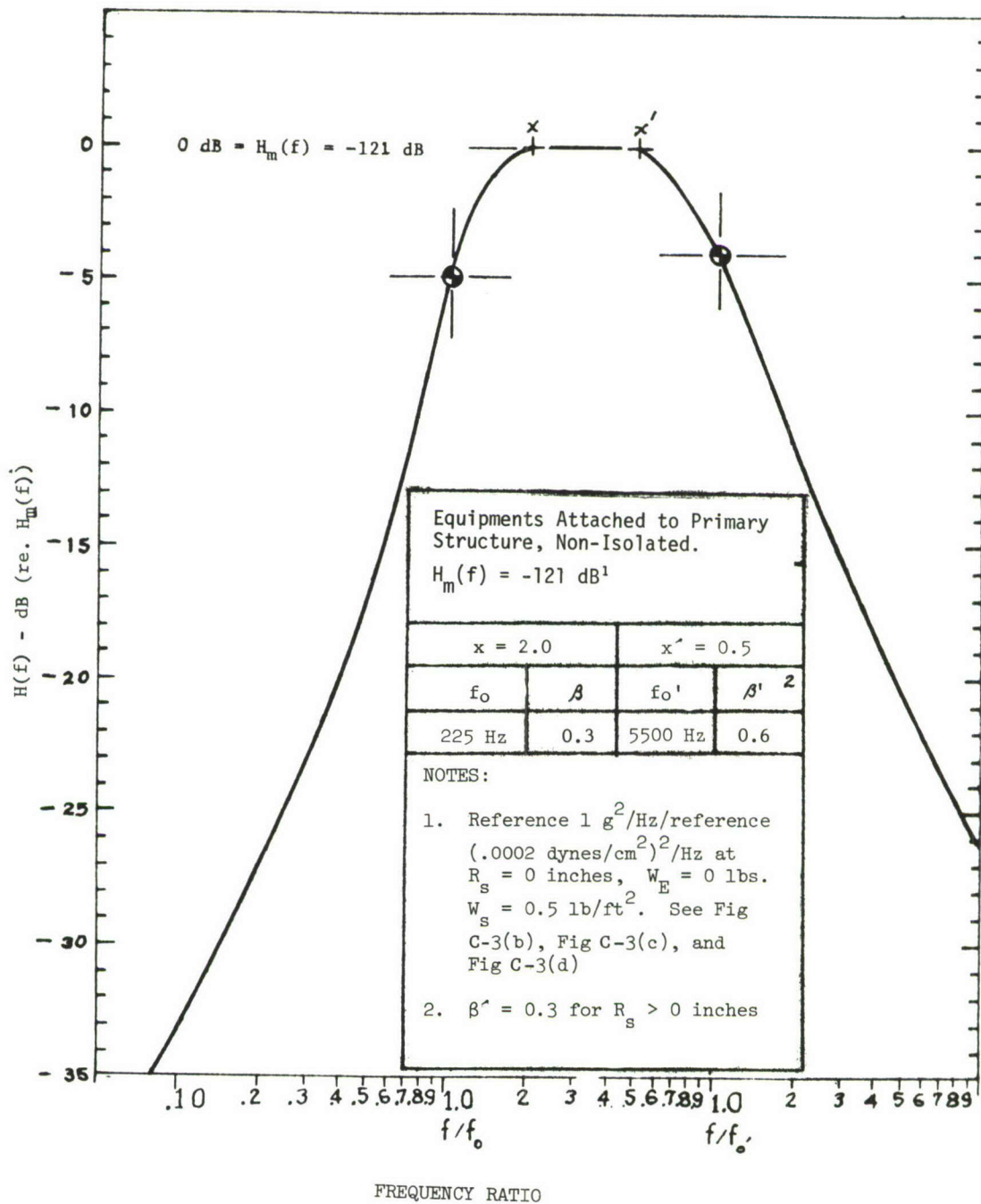


Figure E-1b. Transfer Function for Category I(b)

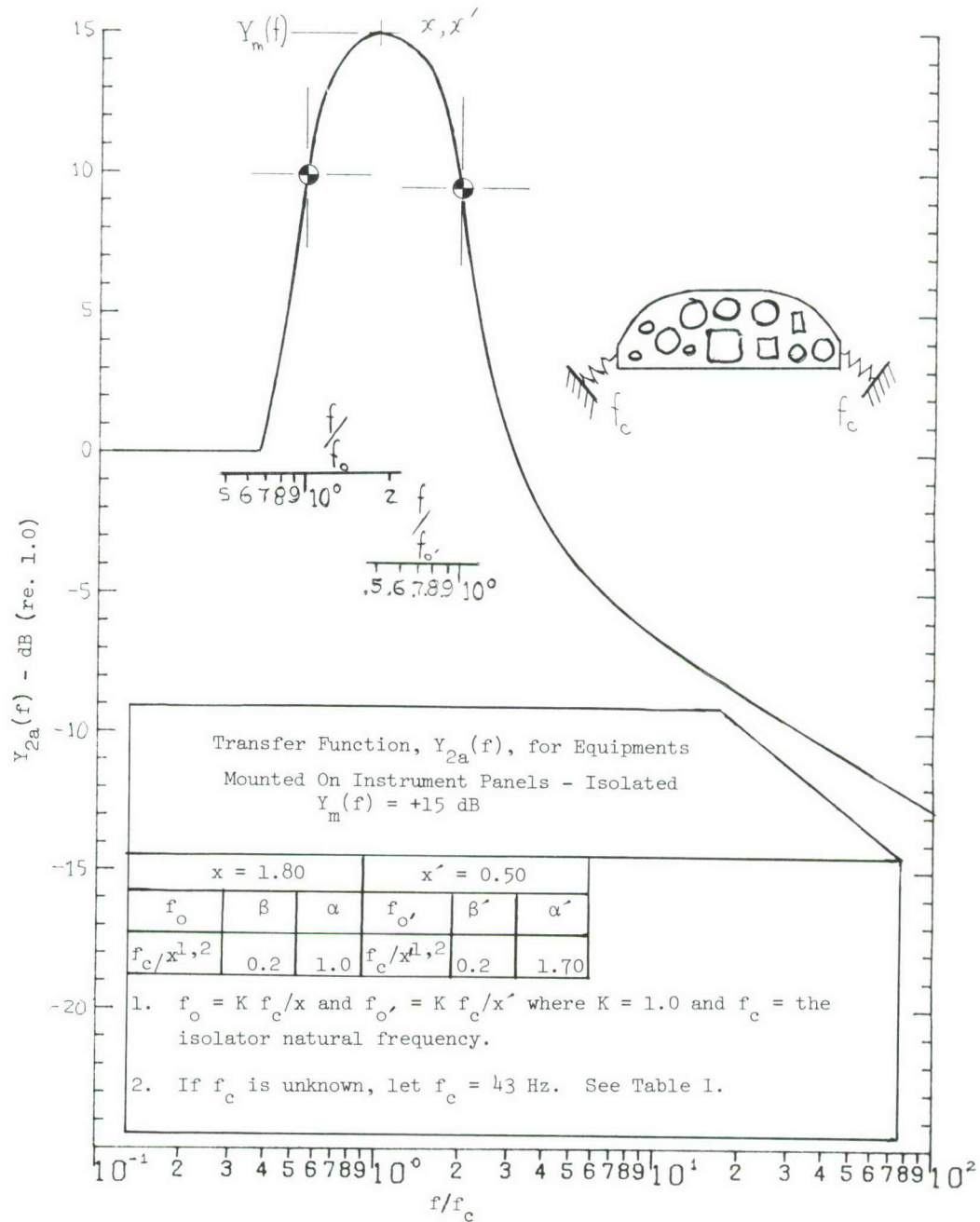


Figure E-2a. Transfer Function for Category II(a)

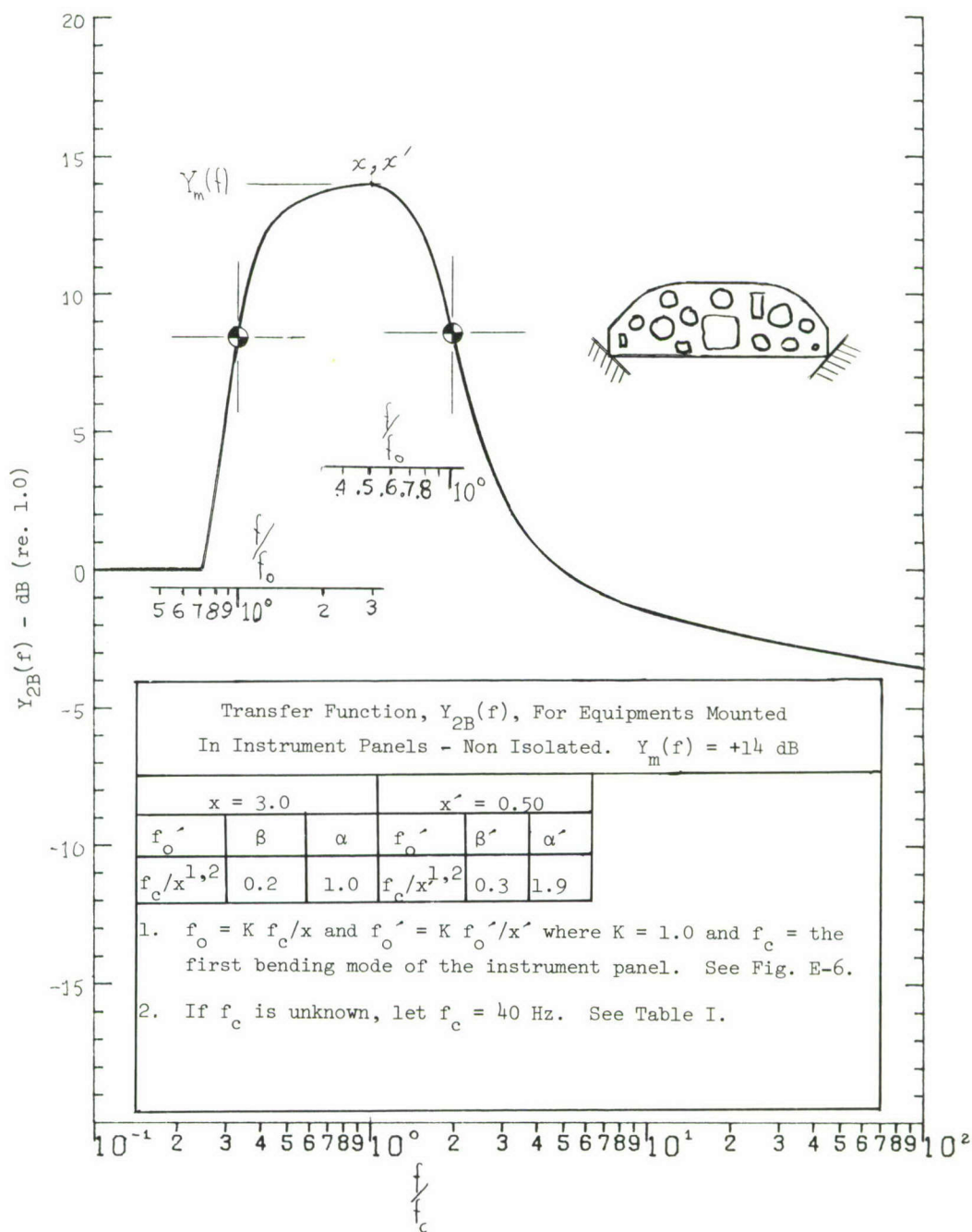


Figure E-2b. Transfer Function for Category II(b)

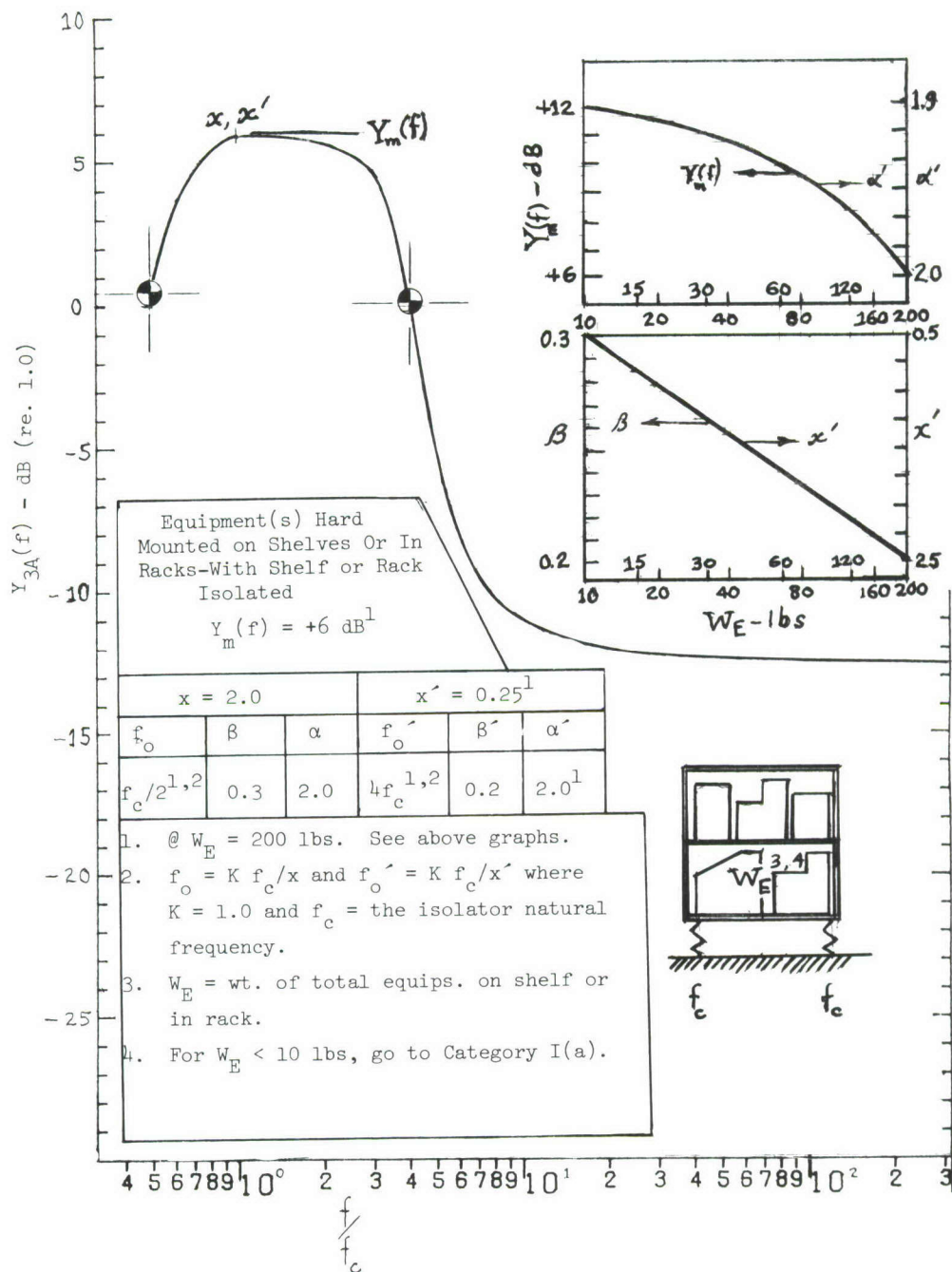


Figure E-3a. Transfer Function for Category III(a)

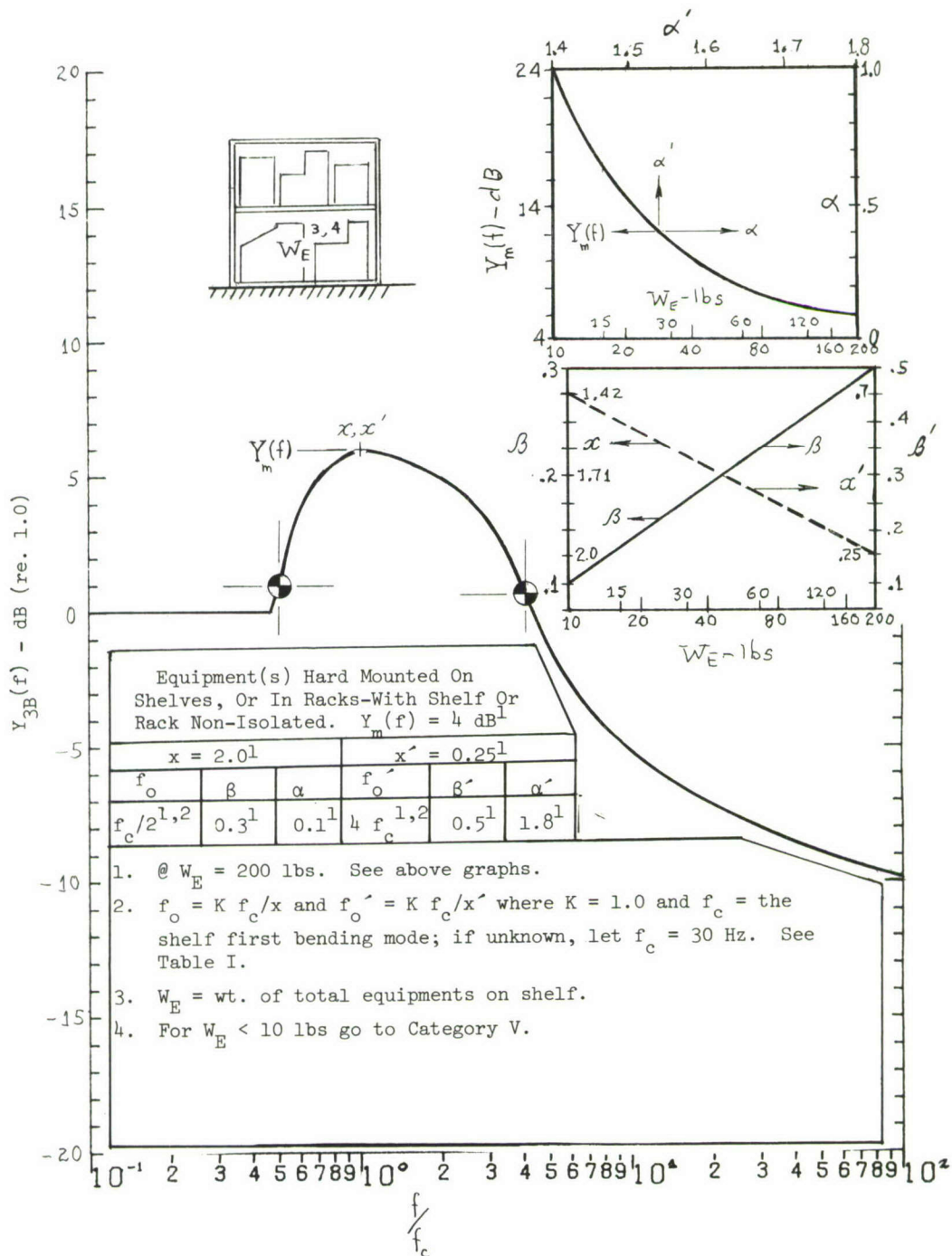


Figure E-3b. Transfer Function for Category III(b)

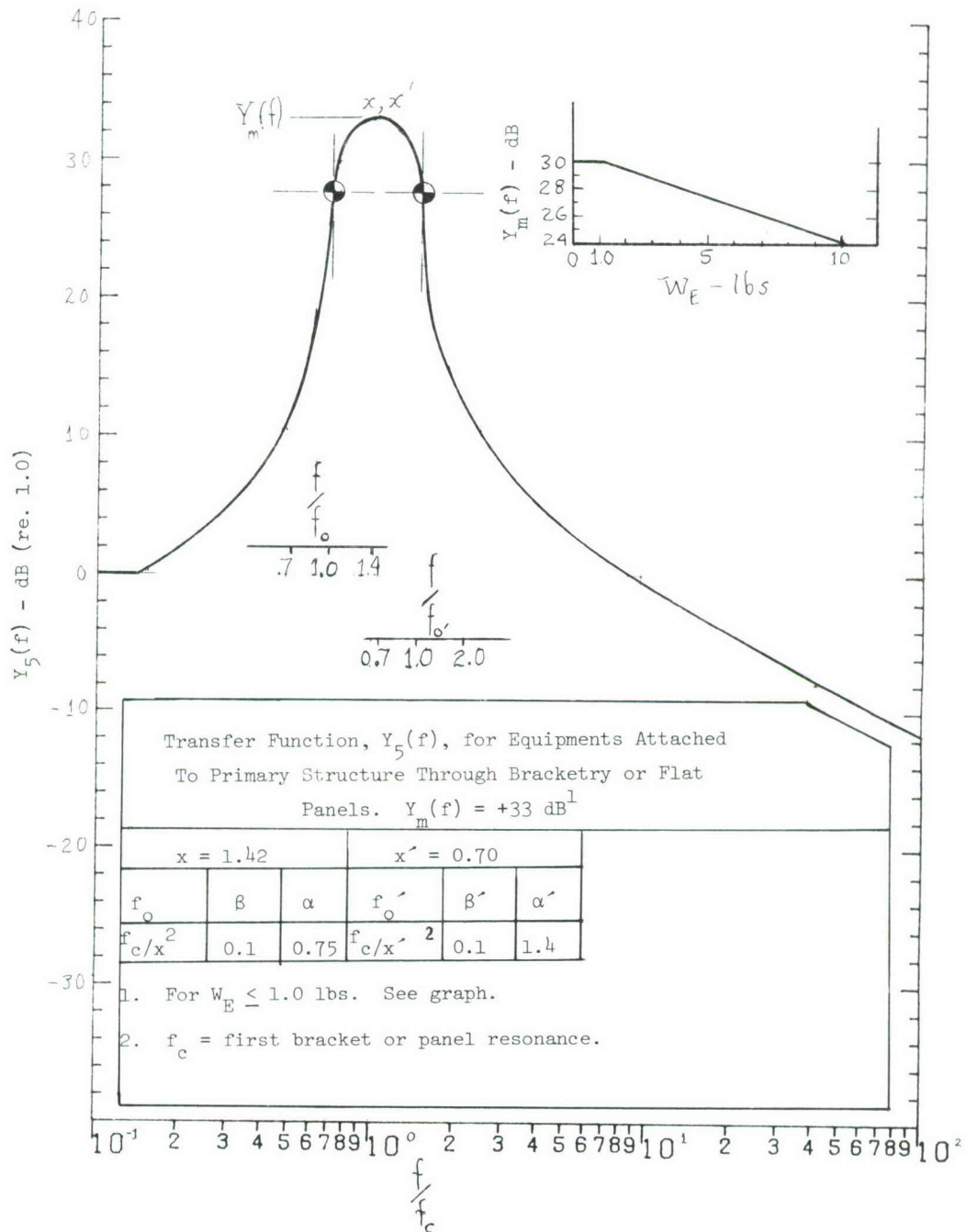
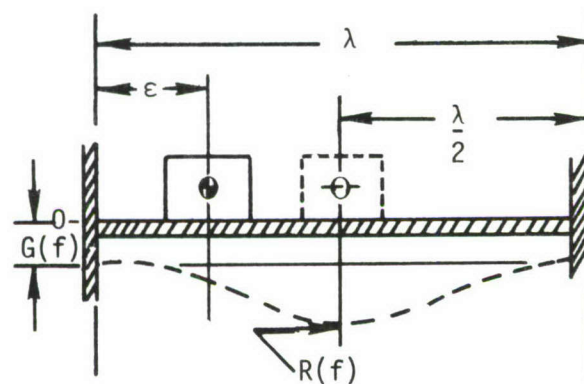


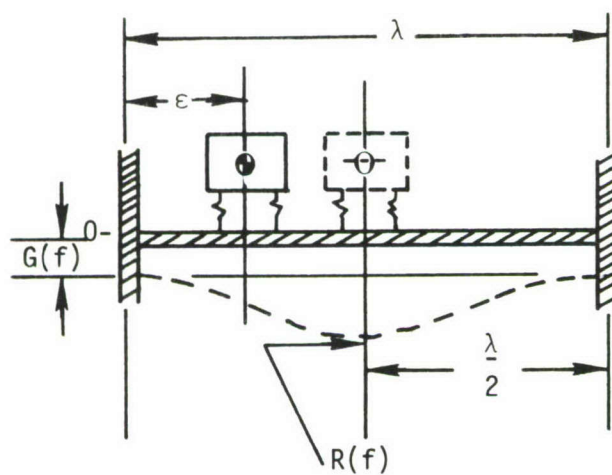
Figure E-4. Transfer Function for Category V





Category III(b)

$$0 \leq \epsilon \leq \frac{\lambda}{2}$$



Category IV(b)

Figure E-5. Midspan Location of  $R(f)$

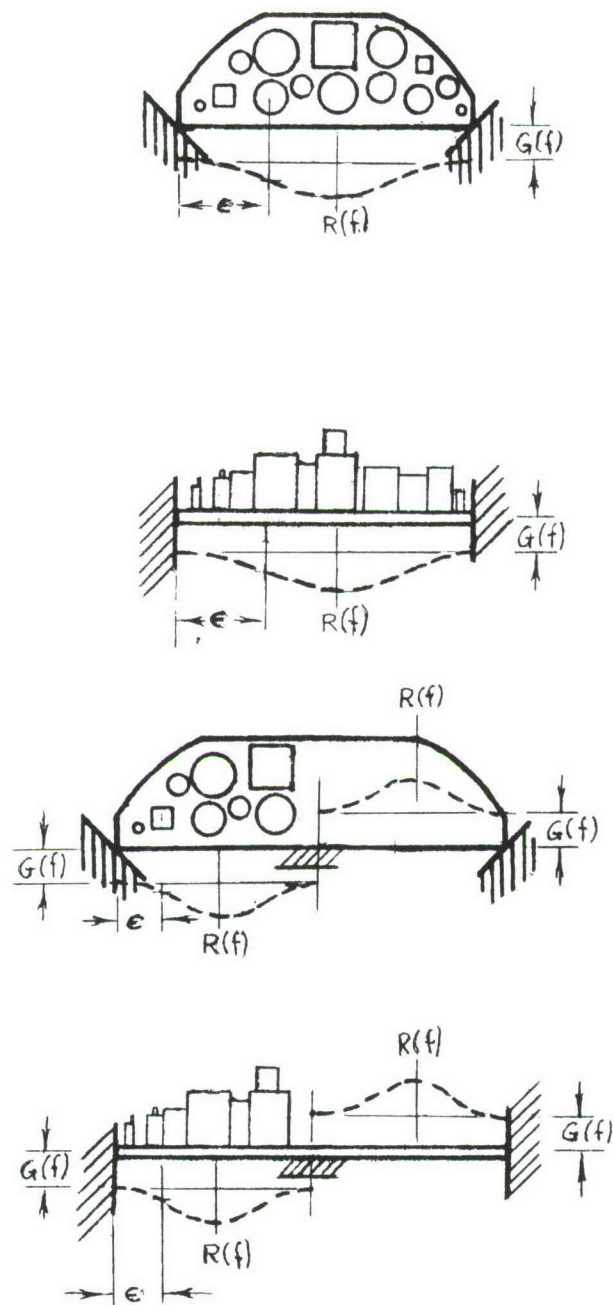


Figure E-6. Midspan Locations of  $R(f)$  for Instrument Panels

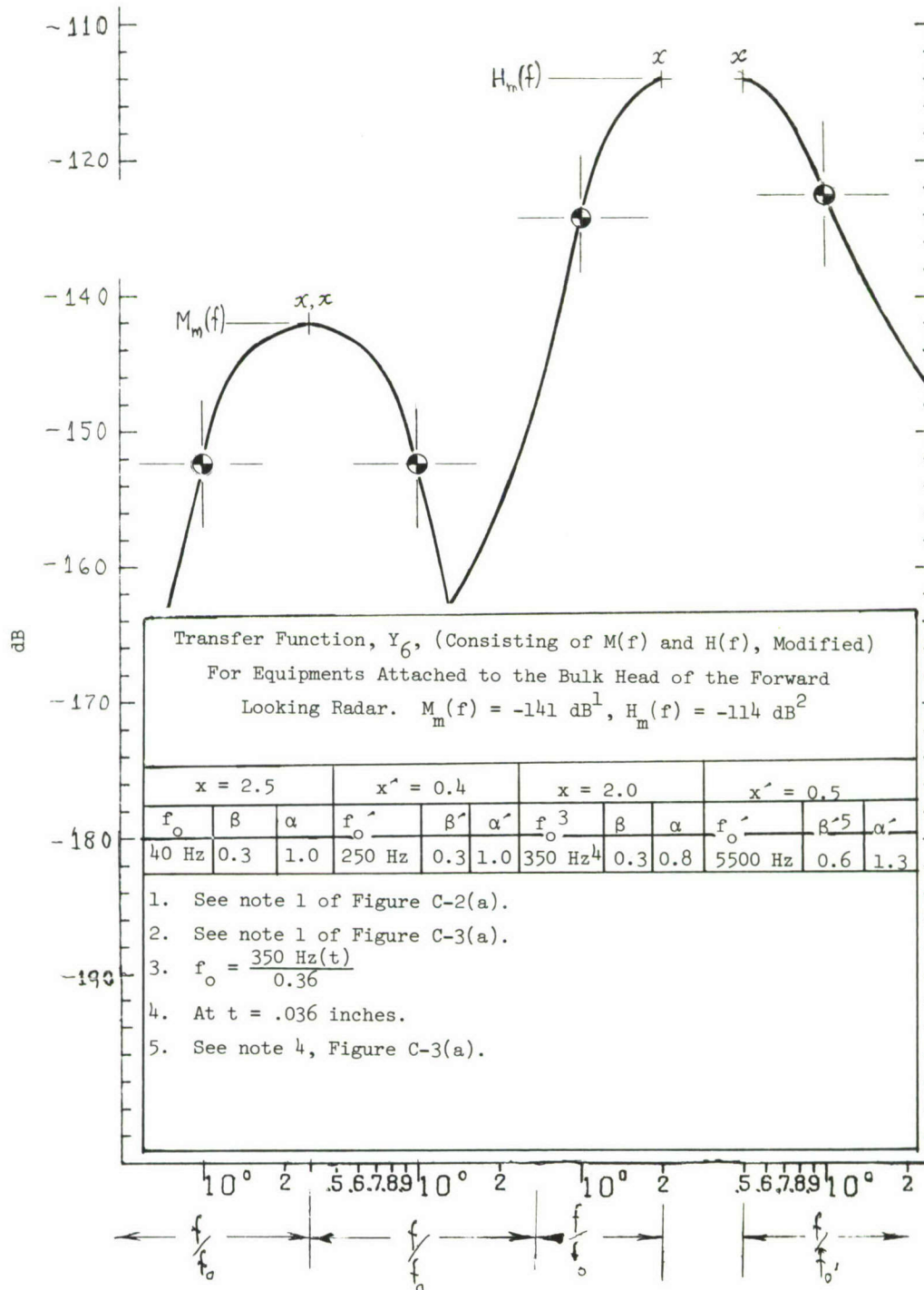


Figure E-7. Transfer Function for Category VI

## APPENDIX F

74/74 OPT=1

COMPUTER PROGRAM

FTN 4.5+414

08/16/77 13.11.28

1	C	PROGRAM VIPRF(INPUT,OUTPUT,TAPES=INPUT,PLFILE)	VIPRF	2
	C	AMFHI FORM FACTOR, HIGH-FREQ.ROLL-OFF, FOR H(F)	VIPRF	3
	C	AMFLO FORM FACTOR, LOW-FREQ.ROLL-OFF, FOR H(F)	VIPRF	4
	C	AMFMAX MAXIMUM VALUE OF H(F)	VIPRF	5
5	C	AHI FORM FACTOR, HIGH-FREQ.ROLL-OFF=FORM FACTOR OF Y(F) FOR	VIPRF	6
	C	SPECIFIED CATEGORY	VIPRF	7
	C	AK WORKING VAR, USED WHEN CALCULATING FZHEHI	VIPRF	8
	C	ALFHI FORM FACTOR, HIGH-FREQ.ROLL-OFF, FOR L(F)	VIPRF	9
	C	ALFLO FORM FACTOR, LOW-FREQ.ROLL-OFF, FOR L(F)	VIPRF	10
10	C	ALNAHI FORM FACTOR, HIGH-FREQ.ROLL-OFF, FOR S(F)-LANDING PHASE	VIPRF	11
	C	ALNALC FORM FACTOR, LOW-FREQ.ROLL-OFF, FOR S(F)-LANDING PHASE	VIPRF	12
	C	ALNDHI SLOPE FACTOR, HIGH-FREQ.ROLL-OFF, FOR S(F)-LANDING PHASE	VIPRF	13
	C	ALNDLC SLOPE FACTOR, LOW-FREQ.ROLL-OFF, FOR S(F)-LANDING PHASE	VIPRF	14
	C	ALNMAX MAXIMUM VALUE OF S(F)-LANDING PHASE	VIPRF	15
15	C	ALNXHI NORM. FREQ. RATIO, HIGH FREQ.ROLL-OFF, FOR S(F)-LANDING PHASE	VIPRF	16
	C	ALNXLC NORM. FREQ. RATIO, LOW FREQ.ROLL-OFF, FOR S(F)-LANDING PHASE	VIPRF	17
	C	ALC FORM FACTOR, LOW FREQ.ROLL-OFF=FORM FACTOR OF Y(F) FOR	VIPRF	18
	C	SPECIFIED CATEGORY	VIPRF	19
	C	ALPHA ARRAY USED FOR STORING FORM FACTORS OF TRANSFER FUNCTIONS	VIPRF	20
20	C	WHEN CALCULATING L(F)-M(F)-H(F)	VIPRF	21
	C	ALT ARRAY USED FOR STORING INPUT ALTITUDE VALUES	VIPRF	22
	C	ALTUT ARRAY USED FOR STORING ALTITUDE TABULAR VALUES	VIPRF	23
	C	AL2FHI FORM FACTOR, HIGH-FREQ.ROLL-OFF, FOR L (F)	VIPRF	24
	C	2	VIPRF	25
25	C	AL2FLO FORM FACTOR, LOW-FREQ.ROLL-OFF, FOR L (F)	VIPRF	26
	C	2	VIPRF	27
	C	AMAKNC MACH NO.	VIPRF	28
	C	AMFHI FORM FACTOR, HIGH-FREQ.ROLL-OFF, FOR M(F)	VIPRF	29
	C	AMFLO FORM FACTOR, LOW-FREQ.ROLL-OFF, FOR M(F)	VIPRF	30
30	C	AMFMAX MAXIMUM VALUE OF M(F)	VIPRF	31
	C	APFHI FORM FACTOR, HIGH-FREQ.ROLL-OFF, FOR P(F)	VIPRF	32
	C	AVFENS ARRAY USED FOR STORING AVERAGE DENSITY TABULAR VALUES	VIPRF	33
	C	AVP ARRAY USED FOR STORING AVERAGE PRESSURE TABULAR VALUES	VIPRF	34
	C	BP2FHI SLOPE FACTOR, HIGH-FREQ.ROLL-OFF, FOR L(F)-INITIAL VALUE	VIPRF	35
35	C	BP2FLO SLOPE FACTOR, LOW-FREQ.ROLL-OFF, FOR L(F)-INITIAL VALUE	VIPRF	36
	C	BF2PF ARRAY FOR TABULAR BETA VALUES USED WHEN CALCULATING FZPF	VIPRF	37
	C	PF2FHI SLOPE FACTOR, HIGH-FREQ.ROLL-OFF, FOR H(F)	VIPRF	38
	C	PF2FLO SLOPE FACTOR, LOW-FREQ.ROLL-OFF, FOR H(F)	VIPRF	39
	C	FHI SLOPE FACTOR, HIGH-FREQ.ROLL-OFF=SLOPE FACTOR OF Y(F) FOR	VIPRF	40
40	C	SPECIFIED CATEGORY	VIPRF	41
	C	PLFHI SLOPE FACTOR, HIGH-FREQ.ROLL-OFF, FOR L (F)	VIPRF	42
	C	PLFLO SLOPE FACTOR, LOW-FREQ.ROLL-OFF, FOR L (F)	VIPRF	43
	C	ELC SLOPE FACTOR, LOW-FREQ.ROLL-OFF=SLOPE FACTOR OF Y(F) FOR	VIPRF	44
	C	SPECIFIED CATEGORY	VIPRF	45
45	C	PL2FHI SLOPE FACTOR, HIGH-FREQ.ROLL-OFF, FOR L (F)	VIPRF	46
	C	2	VIPRF	47
	C	PL2FLO SLOPE FACTOR, LOW FREQ.ROLL-OFF, FOR L (F)	VIPRF	48
	C	2	VIPRF	49
	C	PMFHI SLOPE FACTOR, HIGH FREQ.ROLL-OFF, FOR M(F)	VIPRF	50
50	C	PMFLO SLOPE FACTOR, LOW FREQ.ROLL-OFF, FOR M(F)	VIPRF	51
	C	PPF SLOPE FACTOR, HIGH FREQ.ROLL-OFF, FOR P(F)	VIPRF	52
	C	BUFFAHI FORM FACTOR, HIGH FREQ.ROLL-OFF, FOR S(F)-BUFFET TURN PHASE	VIPRF	53
	C	BUFFALC FORM FACTOR, LOW FREQ.ROLL-OFF, FOR S(F)-BUFFET TURN PHASE	VIPRF	54
	C	BUFF2FHI SLOPE FACTOR, HIGH FREQ.ROLL-OFF, FOR S(F)-BUFFET TURN PHASE	VIPRF	55
55	C	BUFF2EL DELTA VALUE FOR S(F)-BUFFET TURN PHASE	VIPRF	56
	C	BUFF2FH LOCATOR FREQ., HIGH FREQ.ROLL-OFF, FOR S(F)-BUFFET TURN PHASE	VIPRF	57
	C	BUFF2FL LOCATOR FREQ., LOW FREQ.ROLL-OFF, FOR S(F)-BUFFET TURN PHASE	VIPRF	58



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	C	BUFXMAX	MAXIMUM VALUE OF S(F) FOR BUFFET-TURN FLIGHT PHASE	VIPRF	59
	C	BUFXHI	NORM.FREQ.RATIO,HIGH FREQ.ROLL-OFF,FOR BUFFET TURN PHASE	VIPRF	60
60	C	BUFXLC	NORM.FREQ.RATIO, LOW FREQ.ROLL-OFF,FOR BUFFET TURN PHASE	VIPRF	61
	C	C	SPEED OF SOUND,CURRENT VALUE	VIPRF	62
	C	CATGRY	EQUIP.COUNTING CATEGORY,CURRENT VALUE	VIPRF	63
	C	CONST	FRACTION OF FREQ.VALUE BY WHICH THE FREQ.IS INCREASED	VIPRF	64
	C	CORLEF	VALUE OF CORRECTION TO MAXIMUM VALUE OF L(F)	VIPRF	65
65	C	CORLEF	VALUE OF CORRECTION TO MAXIMUM VALUE OF L (F)	VIPRF	66
	C		2	VIPRF	67
	C	C1A	C1A=2H1A(CATEGORY 1A)	VIPRF	68
	C	C1AAHI	FORM FACTOR,HIGH FREQ.ROLL-OFF,FOR CATEGORY 1A	VIPRF	69
	C	C1AALC	FORM FACTOR, LOW FREQ.ROLL-OFF,FOR CATEGORY 1A	VIPRF	70
70	C	C1AAWF	ARRAY FOR STORING TABULAR FORM FACTOR VALUES(HIGH FREQ.	VIPRF	71
	C		ROLL-OFF FOR CATEGORY 1A)	VIPRF	72
	C	C1ABHI	SLOPE FACTOR,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 1A	VIPRF	73
	C	C1ABLC	SLOPE FACTOR, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 1A	VIPRF	74
	C	C1AFN	FIRST FUSELAGE BENDING MODE FREQ.,FOR Y(F)-CATEGORY 1A	VIPRF	75
75	C	C1AFZH	LOCATOR FREQ.,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 1A	VIPRF	76
	C	C1AFZL	LOCATOR FREQ., LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 1A	VIPRF	77
	C	C1AMAX	MAXIMUM VALUE OF Y(F)-CATEGORY 1A	VIPRF	78
	C	C1AMWF	ARRAY FOR STORING TABULAR DB VALUES USED WHEN CALCULATING	VIPRF	79
	C		CORRECTION TO C1AMAX FOR WE VALUE	VIPRF	80
80	C	C1AMXC	CORRECTED MAXIMUM VALUE OF Y(F)-CATEGORY 1A	VIPRF	81
	C	C1AXHI	NORM.FREQ.RATIO,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 1A	VIPRF	82
	C	C1AXLC	NORM.FREQ.RATIO, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 1A	VIPRF	83
	C	C1P	C1P=2H1P(CATEGORY 1A)	VIPRF	84
	C	C2A	C2A=2H2A(CATEGORY 2A)	VIPRF	85
85	C	C2AAHI	FORM FACTOR,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2A	VIPRF	86
	C	C2AALC	FORM FACTOR, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2A	VIPRF	87
	C	C2ABHI	SLOPE FACTOR,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2A	VIPRF	88
	C	C2ABLC	SLOPE FACTOR, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2A	VIPRF	89
	C	C2AFN	FIRST FUSELAGE BENDING MODE FREQ. FOR Y(F)-CATEGORY 2A	VIPRF	90
90	C	C2AMAX	MAXIMUM VALUE OF Y(F)-CATEGORY 2A	VIPRF	91
	C	C2AXHI	NORM.FREQ.RATIO,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2A	VIPRF	92
	C	C2AXLC	NORM.FREQ.RATIO, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2A	VIPRF	93
	C	C2P	C2P=2H2P(CATEGORY 2B)	VIPRF	94
95	C	C2PAHI	FORM FACTOR,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2B	VIPRF	95
	C	C2PALC	FORM FACTOR, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2B	VIPRF	96
	C	C2PBHI	SLOPE FACTOR,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2B	VIPRF	97
	C	C2PBLC	SLOPE FACTOR, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2B	VIPRF	98
	C	C2PFN	FIRST FUSELAGE BENDING MODE FREQ. FOR Y(F)-CATEGORY 2B	VIPRF	99
	C	C2PMAX	MAXIMUM VALUE OF Y(F)-CATEGORY 2B	VIPRF	100
100	C	C2PXHI	NORM.FREQ.RATIO,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2B	VIPRF	101
	C	C2PYLC	NORM.FREQ.RATIO, LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 2B	VIPRF	102
	C	C3A	C3A=2H3A(CATEGORY 3A)	VIPRF	103
	C	C3AALC	FORM FACTOR,LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 3A	VIPRF	104
105	C	C3AAP	ARRAY FOR STORING TABULAR ALPHA* VALUES,USED WHEN CALCULATI	VIPRF	105
	C		ALPHA* FOR Y(F)-CATEGORY 3A FROM WE(EQUIP.WEIGHT)	VIPRF	106
	C	C3AB	ARRAY FOR STORING TABULAR BETA VALUES,USED WHEN CALCULATING	VIPRF	107
	C		BETA FOR Y(F)-CATEGORY 3A FROM WE(EQUIP.WEIGHT)	VIPRF	108
	C	C3ABHI	SLOPE FACTOR,HIGH FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 3A	VIPRF	109
	C	C3AFN	FIRST FUSELAGE BENDING MODE FREQ.,FOR Y(F)-CATEGORY 3A	VIPRF	110
110	C	C3AXLC	NORM.FREQ.RATIO,LOW FREQ.ROLL-OFF,FOR Y(F)-CATEGORY 3A	VIPRF	111
	C	C3AXP	ARRAY FOR STORING TABULAR X* VALUES USED WHEN CALCULATING	VIPRF	112
	C		X* FOR Y(F)-CATEGORY 3A FROM WE(EQUIP.WEIGHT)	VIPRF	113
	C	C3AYMX	ARRAY FOR STORING TABULAR Y(F),MAXIMUM,VALUES,USED WHEN	VIPRF	114
	C		CALCULATING THE MAX.OF Y(F)-CATEGORY 3A FROM WE(EQUIP.WEIGH	VIPRF	115

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115	C	C3P	C3P=2H3B(CATEGORY 3B)	VIPRF	116
	C	C3PA	ARRAY FOR STORING TABULAR ALPHA VALUES, USED WHEN CALCULATING	VIPRF	117
	C		ALPHA FOR Y(F)-CATEGORY 3B FROM WE(EQUIP.WEIGHT)	VIPRF	118
	C	C3PAP	ARRAY FOR STORING TABULAR ALPHA' VALUES USED WHEN	VIPRF	119
	C		CALCULATING ALPHA' FOR Y(F)-CATEGORY 3B FROM WE(EQUIP.WEIGHT)	VIPRF	120
120	C	C3PB	ARRAY FOR STORING TABULAR BETA VALUES USED WHEN CALCULATING	VIPRF	121
	C		BETA FOR Y(F)-CATEGORY 3B FROM WE(EQUIP.WEIGHT)	VIPRF	122
	C	C3PBP	ARRAY FOR STORING TABULAR BETA' VALUES USED WHEN CALCULATING	VIPRF	123
	C		BETA' FOR Y(F)-CATEGORY 3B FROM WE(EQUIP.WEIGHT)	VIPRF	124
	C	C3PFN	FIRST FUSELAGE BENDING MODE FREQ. FOR Y(F)-CATEGORY 3B	VIPRF	125
125	C	C3PX	ARRAY FOR STORING TABULAR X VALUES USED WHEN CALCULATING	VIPRF	126
	C		X FOR Y(F)-CATEGORY 3B FROM WE(EQUIP.WEIGHT)	VIPRF	127
	C	C3PXP	ARRAY FOR STORING TABULAR X' VALUES USED WHEN CALCULATING	VIPRF	128
	C		X' FOR Y(F)-CATEGORY 3B FROM WE(EQUIP.WEIGHT)	VIPRF	129
	C	C3PYMX	ARRAY FOR STORING TABULAR Y(F), MAX., VALUES USED WHEN	VIPRF	130
130	C	C3WE	ARRAY FOR STORING VALUES OF "WE" USED WHEN INTERPOLATING	VIPRF	131
	C		FOR PARAMETERS OF Y(F) FOR CATEGORIES 3A AND 3P	VIPRF	132
	C		CALCULATING Y(F), MAX., (CATEGORY 3B) FROM WE(EQUIP.WEIGHT)	VIPRF	133
	C	C4A	C4A=2H4A(CATEGORY 4A)	VIPRF	134
	C	C4B	C4B=2H4B(CATEGORY 4B)	VIPRF	135
135	C	C5	C5=1H5 (CATEGORY 5)	VIPRF	136
	C	C5AHI	FORM FACTOR, HIGH FREQ. ROLL-OFF, FOR Y(F)-CATEGORY 5	VIPRF	137
	C	C5ALO	FORM FACTOR, LOW FREQ. ROLL-OFF, FOR Y(F)-CATEGORY 5	VIPRF	138
	C	C5PHI	SLOPE FACTOR, HIGH FREQ. ROLL-OFF, FOR Y(F)-CATEGORY 5	VIPRF	139
	C	C5PLO	SLOPE FACTOR, LOW FREQ. ROLL-OFF, FOR Y(F)-CATEGORY 5	VIPRF	140
140	C	C5FN	FIRST FUSELAGE BENDING MODE FREQ. FOR Y(F)-CATEGORY 5	VIPRF	141
	C	C5MAX	MAXIMUM VALUE OF Y(F)-CATEGORY 5	VIPRF	142
	C	C5XHI	NORM. FREQ. RATIO, HIGH FREQ. ROLL-OFF, FOR Y(F)-CATEGORY 5	VIPRF	143
	C	C5XLO	NORM. FREQ. RATIO, LOW FREQ. ROLL-OFF, FOR Y(F)-CATEGORY 5	VIPRF	144
	C	C6	C6=1H6 (CATEGORY 6)	VIPRF	145
145	C	D	DIFFERENCE BET. BUFFT-TURN AND E DISTANCES	VIPRF	146
	C	DB	ARRAY FOR STORING DECIBEL VALUES OF L(F), M(F) AND H(F)	VIPRF	147
	C		USED WHEN CALCULATING L(F)-M(F)-H(F) FUNCTION	VIPRF	148
	C	DBFL	ARRAY FOR STORING DECIBEL VALUES WHEN MAKING CALCULATIONS	VIPRF	149
	C		TO DETERMINE THE COORDINATES OF POINTS OF FUNCTIONS P(F), G(F)	VIPRF	150
150	C		Y(F), R(F) AND A(F)	VIPRF	151
	C	DBMFRS	ARRAY FOR STORING TABULAR DECIBEL VALUES USED FOR	VIPRF	152
	C		CORRECTING "XMFMAX" FOR THE VALUE OF "RS"	VIPRF	153
	C	DBMIN	MIN. Y AXIS(DECIBEL) VALUE, AN ARGUMENT OF "XLOG" PLOT SUBROUTINE	VIPRF	154
	C	DBMOD1	ARRAY FOR STORING 1ST BENDING MODE (DB) VALS. FOR CURRENT	VIPRF	155
155	C		TYPE AIRCRAFT	VIPRF	156
	C	DBMOD2	ARRAY FOR STORING 2ND BENDING MODE (DB) VALS. FOR CURRENT	VIPRF	157
	C		TYPE AIRCRAFT	VIPRF	158
	C	DBRS	ARRAY FOR STORING DECIBEL VALUES USED WHEN CALCULATING	VIPRF	159
	C		CORRECTION TO H(F) FOR R	VIPRF	160
160	C		M S	VIPRF	161
	C	DBSPL	ARRAY FOR STORING DECIBEL VALUES WHEN MAKING CALCULATIONS	VIPRF	162
	C		TO DETERMINE THE COORDINATES OF POINTS OF FUNCTIONS P(F), S(F)	VIPRF	163
	C	DB1A10	ARRAY FOR STORING 1ST BENDING MODE (DB) VALUES FOR A10	VIPRF	164
	C	DB1A70	ARRAY FOR STORING 1ST BENDING MODE VALUES FOR A-70	VIPRF	165
165	C	DB1F15	ARRAY FOR STORING 1ST BENDING MODE VALUES FOR F-15	VIPRF	166
	C	DB1F16	ARRAY FOR STORING 1ST BENDING MODE VALUES FOR F-16	VIPRF	167
	C	DB1F4	ARRAY FOR STORING 1ST BENDING MODE VALUES FOR F-4	VIPRF	168
	C	DB1111	ARRAY FOR STORING 1ST BENDING MODE VALUES FOR F-111	VIPRF	169
	C	DB2A10	ARRAY FOR STORING 2ND BENDING MODE (DB) VALUES FOR A10	VIPRF	170
170	C	DB2A70	ARRAY FOR STORING 2ND BENDING MODE VALUES FOR A-70	VIPRF	171
	C	DB2F15	ARRAY FOR STORING 2ND BENDING MODE VALUES FOR F-15	VIPRF	172



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	0	DB2F16	ARRAY FOR STORING 2ND BENDING MODE VALUES FOR F-16	VIPRF	173
	0	DB2F4	ARRAY FOR STORING 2ND BENDING MODE VALUES FOR F-4	VIPRF	174
	0	DB2111	ARRAY FOR STORING 2ND BENDING MODE (DB) VALUES FOR F-111	VIPRF	175
175	0	DDFVAL	ARRAY FOR STORING DECIBEL VALUES USED FOR CORRECTING	VIPRF	176
	0		S (F) * TO DETERMINE S (F), GIVEN D=X -X	VIPRF	177
	0		BT M BT M BT F	VIPRF	178
	0	DECEPL	ARRAY FOR STORING DECIBEL VALUES WHEN MAKING CALCULATIONS	VIPRF	179
	0		TO DETERMINE THE COORDINATES OF POINTS OF FUNCTIONS	VIPRF	180
180	0		L(F)-M(F)-H(F),G(F),R(F),A(F)	VIPRF	181
	0	DELDEE	INTERVAL BETWEEN THE UNIFORMLY SPACED "D" VALUES FOR EACH C	VIPRF	182
	0		WHICH A DB VALUE IS STORED IN ARRAY "DDFVAL"	VIPRF	183
	0	DELR5	CORRECTION TO M(F) AND H(F) FOR R (DISTANCE FROM SKIN)	VIPRF	184
	0		S	VIPRF	185
185	0	DELTA7	BOUNDARY LAYER THICKNESS AT THE GIVEN ALTITUDE	VIPRF	186
	0	DELTA7	BOUNDARY LAYER THICKNESS AT ZERO ALTITUDE	VIPRF	187
	0	DELLWE	CORRECTION TO H(F) FOR W (EQUIPMENT WEIGHT)	VIPRF	188
	0		F	VIPRF	189
	0	DELSW	CORRECTION TO M(F) AND H(F) FOR W (SKIN SURFACE DENSITY)	VIPRF	190
190	0		S	VIPRF	191
	0	DE	DIAMETER OF FUSELAGE AT LOCATION OF EQUIPMENT	VIPRF	192
	0	DNCRM	NORMALIZED, AVERAGE DENSITY AT A GIVEN ALTITUDE	VIPRF	193
	0	DWE100	DISTANCE BETWEEN UNIFORMLY SPACED WE VALUES(100 LBS. MAX.),	VIPRF	194
	0		FOR EACH OF WHICH A DB VALUE IS STORED IN ARRAY WE100	VIPRF	195
195	0	DWE1K	DISTANCE BETWEEN UNIFORMLY SPACED WE VALUES(1000 LBS. MAX.)	VIPRF	196
	0		FOR EACH OF WHICH A DB VALUE IS STORED IN ARRAY WE1000	VIPRF	197
	0	DWE5K	DISTANCE BETWEEN UNIFORMLY SPACED WE VALUES(5000 LBS. MAX.)	VIPRF	198
	0		FOR EACH OF WHICH A DB VALUE IS STORED IN ARRAY WE5000	VIPRF	199
	0	EXMFFS	INTERVAL, DELTA RS, BETWEEN TABULAR, DECIBEL VALUES USED	VIPRF	200
200	0		WHEN CALCULATING CORRECTION TO M(F) FOR "RS".	VIPRF	201
	0	EXMOD1	INTERVAL, DELTA XE, BETWEEN TABULAR 1ST BENDING MODE (DE) VAL	VIPRF	202
	0		STORED IN ARRAY DBMOD1 FOR CURRENT TYPE AIRCRAFT	VIPRF	203
	0	EXMOD2	INTERVAL, DELTA XE, BETWEEN TABULAR 2ND BENDING MODE (DE) VAL	VIPRF	204
	0		STORED IN ARRAY DBMOD2 FOR CURRENT TYPE AIRCRAFT	VIPRF	205
205	0	DX1A10	INTERVAL, DELTA XE, BETWEEN TABULAR 1ST BENDING MODE VALS., A-	VIPRF	206
	0	DX1A70	INTERVAL, DELTA XE, BETWEEN TABULAR 1ST BENDING MODE VALS., A-	VIPRF	207
	0	DX1F15	INTERVAL, DELTA XE, BETWEEN TABULAR 1ST BENDING MODE VALS., F-	VIPRF	208
	0	DX1F16	INTERVAL, DELTA XE, BETWEEN TABULAR 1ST BENDING MODE VALS., F-	VIPRF	209
	0	DX1F4	INTERVAL, DELTA XE, BETWEEN TABULAR 1ST BENDING MODE VALS., F-	VIPRF	210
210	0	DX1111	INTERVAL, DELTA XE, BETWEEN TABULAR 1ST BENDING MODE VALS., F-	VIPRF	211
	0	DX2A10	INTERVAL, DELTA XE, BETWEEN TABULAR 2ND BENDING MODE VALS., A-	VIPRF	212
	0	DX2A70	INTERVAL, DELTA XE, BETWEEN TABULAR 2ND BENDING MODE VALS., A-	VIPRF	213
	0	DX2F15	INTERVAL, DELTA XE, BETWEEN TABULAR 2ND BENDING MODE VALS., F-	VIPRF	214
	0	DX2F16	INTERVAL, DELTA XE, BETWEEN TABULAR 2ND BENDING MODE VALS., F-	VIPRF	215
215	0	DX2F4	INTERVAL, DELTA XE, BETWEEN TABULAR 2ND BENDING MODE VALS., F-	VIPRF	216
	0	DX2111	INTERVAL, DELTA XE, BETWEEN TABULAR 2ND BENDING MODE VALS., F-	VIPRF	217
	0	DYVAL	ORDINAL DISTANCE BETWEEN LINES OF LEGENDS ON PLOTS	VIPRF	218
	0	EQ	CENTER FREQ. OF Y(F) TRANSFER FUNCTION	VIPRF	219
	0	EQCAT1	INPUT VALUE FOR EQ FOR CATEGORIES OTHER THAN 1B, 4A AND 4B	VIPRF	220
220	0	EQCAT2	INPUT VALUE FOR EQ FOR CATEGORIES 4A AND 4B	VIPRF	221
	0	EQMOVE	INPUT VALUE FOR MULTIPLICATION CONSTANT K	VIPRF	222
	0	EQS	CENTER FREQ. OF S(F)	VIPRF	223
	0		BT	VIPRF	224
	0	FLX	ARRAY FOR STORING VALUES OF FLEX-FUNCTIONS USED WHEN	VIPRF	225
225	0		CALCULATING L(F)-M(F)-H(F)	VIPRF	226
	0	FLXDF	VALUE OF FLEX-FUNCTION(HI-FREQ. ROLL-OFF) FOR P(F)	VIPRF	227
	0	FLX1	VALUE OF FLEX-FUNCTION WHEN F/F =X	VIPRF	228
	0		0	VIPRF	229

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		VALUE OF TRANSFER OR SPECIAL FUNCTIONS WHEN F=F OR F=F'	VIPRF	230
230	C	FL2FHI LOCATOR FREQ., HIGH-FREQ. ROLL-OFF, FOR L (F)	VIPRF	231
	C	FL2FLO LOCATOR FREQ., LOW-FREQ. ROLL-OFF, FOR L (F)	VIPRF	232
	C	FL2FHI LOCATOR FREQ., HIGH-FREQ. ROLL-OFF, FOR M (F)	VIPRF	233
	C	FL2FLO LOCATOR FREQ., LOW-FREQ. ROLL-OFF, FOR M (F)	VIPRF	234
235	C	FMAX MAXIMUM FREQ. VALUE USED WHEN CALC. VALUES OF TRANSFER FUNCTI	VIPRF	235
	C	FMAXGF MAXIMUM FREQ. FOR PLOT OF G(F)	VIPRF	236
	C	FMAXHF MAXIMUM FREQ. FOR PLOT OF H(F)	VIPRF	237
	C	FMAXPF MAXIMUM FREQ. FOR PLOT OF P(F)	VIPRF	238
	C	FMFHI LOCATOR FREQ., HIGH-FREQ. ROLL-OFF, FOR M (F)	VIPRF	239
240	C	FMFLO LOCATOR FREQ., LOW-FREQ. ROLL-OFF, FOR M (F)	VIPRF	240
	C	FMINGF MINIMUM FREQ. FOR PLOT OF G(F)	VIPRF	241
	C	FMINHF MINIMUM FREQ. FOR PLOT OF H(F)	VIPRF	242
	C	FMINPF MINIMUM FREQ. FOR PLOT OF P(F)	VIPRF	243
	C	FN 1ST FUSELAGE BENDING MODE FREQ., VERTICAL-SYMMETRIC	VIPRF	244
245	C	FPPHFF ARRAY FOR STORING VALUES OF FREQ. USED WHEN CALCULATING F' F	VIPRF	245
	C	FREQ0 ARRAY FOR STORING FREQ. VALUES SELECTED WHEN CALCULATING	VIPRF	246
	C	L(F)-M(F)-H(F) AND USED AS ABSCISSAS OF POINTS ON PLOTS	VIPRF	247
	C	FREQ FREQ. VALUE	VIPRF	248
250	C	FSPFL ARRAY FOR STORING FREQ. VALUES SELECTED FOR ABSCISSAS OF PCIN	VIPRF	249
	C	ON PLOTS OF P(F) AND H(F)	VIPRF	250
	C	FZ ARRAY FOR STORING VALUES OF F AND F' USED WHEN CALC. L(F)-M	VIPRF	251
	C	0 0	VIPRF	252
	C	FZHFHI LOCATOR FREQ., HIGH-FREQ. ROLL-OFF, FOR H(F)	VIPRF	253
255	C	FZHFLO LOCATOR FREQ., LOW FREQ. ROLL-OFF, FOR H(F)	VIPRF	254
	C	FZHI LOCATOR FREQ., HIGH FREQ. ROLL-OFF, FOR SPECIFIED Y(F) CATEGOR	VIPRF	255
	C	FZLHFI LOCATOR FREQ., HIGH FREQ. ROLL-OFF, FOR L (F)	VIPRF	256
	C	FZLFLO LOCATOR FREQ., LOW FREQ. ROLL-OFF, FOR L (F)	VIPRF	257
	C	FZLO LOCATOR FREQ., LOW FREQ. ROLL-OFF, FOR SPECIFIED Y(F) CATEGOR	VIPRF	258
260	C	FZMFHI LOCATOR FREQ., HIGH FREQ. ROLL-OFF, FOR M (F)	VIPRF	259
	C	FZMFLO LOCATOR FREQ., LOW FREQ. ROLL-OFF, FOR M (F)	VIPRF	260
	C	FZPF LOCATOR FREQ., HIGH FREQ. ROLL-OFF, FOR P (F)	VIPRF	261
	C	FZN SECOND FUSELAGE BENDING MODE FREQ., VERTICAL-SYMMETRIC	VIPRF	262
	C	H ARRAY FOR STORING VALUES OF ALTITUDE	VIPRF	263
265	C	H1LO ARRAY FOR STORING VALUES=0 OR =1, DENOTING LOW-PASS, HIGH-PAS	VIPRF	264
	C	H1H HEIGHT OF CHARACTERS ON PLOT LABELS, TITLES ETC.	VIPRF	265
	C	H1H1 HEIGHT OF CHARACTERS ON PLOT LABELS, TITLES ETC.	VIPRF	266
	C	HMAX MAXIMUM VALUE OF ALTITUDE	VIPRF	267
	C	I WORKING INTEGER VARIABLE	VIPRF	268
270	C	IALUM =1H4 FOR ALUMINUM	VIPRF	269
	C	IA10 =7H 4-10 FOR COMPARE WITH IPLANE(1)	VIPRF	270
	C	IA70 =7H 4-70 FOR COMPARE WITH IPLANE(1)	VIPRF	271
	C	IBLANK =1H BLANK	VIPRF	272
	C	IBUFFET =2HET BUFFET TURN	VIPRF	273
275	C	ICK VARIABLE EQUAL TO 1 OR 0 USED FOR DETERMINING CURRENT	VIPRF	274
	C	FLIGHT PHASE	VIPRF	275
	C	IERROR ARGUMENT OF SUBROUTINE "READDCS" WHICH DETERMINES	VIPRF	276
	C	BRANCHING DIRECTION AFTER RETURN FROM CALL TO "READDCS"	VIPRF	277
	C	IFIRST SUBSCRIPT OF FIRST ELEMENT IN AN ARRAY WHICH IS PLOTTED	VIPRF	278
280	C	IFLITE SET EQUAL TO VARIABLE ISANDL OR VARIABLE JFLITE	VIPRF	279
	C	IFN =1H4 OR 2H2N FOR SUBSCRIPT IN PRINT OF F OR F	VIPRF	280
	C	N 2N	VIPRF	281
	C	IFNISH =6HFINISH USED FOR COMPARE WITH CONTENTS OF COL.1-6	VIPRF	282
	C	OF INPUT DATA CARDS	VIPRF	283
285	C	IF111 =8H F-111 FOR COMPARE WITH IPLANE(1)	VIPRF	284
	C		VIPRF	285
	C		VIPRF	286

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	C	IF15	=7H F-15 FOR COMPARE WITH IPLANE(1)	VIPRF	287
	C	IF16	=7H F-16 FOR COMPARE WITH IPLANE(1)	VIPRF	288
	C	IF4	=6H F-4 FOR COMPARE WITH IPLANE(1)	VIPRF	289
	C	IPLOD	ARRAY FOR STORING CONTENTS OF APPARENT "DESCRIPTION"	VIPRF	290
290	C		INPUT, DATA CARD AFTER RETURN FROM SUBROUTINE "READCCS"	VIPRF	291
	C	II	WORKING INTEGER VARIABLE	VIPRF	292
	C	ILAND	=7HLANDING FOR LANDING FLIGHT PHASE	VIPRF	293
	C	ILINE1	ARRAY FOR STORING PLOT TITLE LINE CHARACTERS	VIPRF	294
	C	ILINE2	ARRAY FOR STORING PLOT TITLE LINE CHARACTERS	VIPRF	295
295	C	IMAG	=1HM FOR MAGNESIUM	VIPRF	296
	C	INCPLOT	VALUE (BLANKS OR NOT BLANKS) DETERMINES WHETHER THE PLOTS OF	VIPRF	297
	C		TRANSFER AND RESPONSE FUNCTIONS ARE PRODUCED	VIPRF	298
	C	IPHASE	SET EQUAL TO CHAR, COMB. DENOTING FLIGHT PHASE, REQUIRED FOR F	VIPRF	299
	C	IPLANE	ARRAY FOR STORING INPUT VALUES FOR INPUT DATA IDENTIFICATIO	VIPRF	300
300	C	IPLOT	INTEGER VARIABLE FOR COUNT OF PLOTS	VIPRF	301
	C	ISANDL	=7HSANDL, DENOTING S AND L FLIGHT PHASE	VIPRF	302
	C	ISTEEL	=1HS, DENOTING STEEL PLATE MATERIAL	VIPRF	303
	C	ITAKEOFF	=7HTAKEOFF, DENOTING TAKEOFF FLIGHT PHASE	VIPRF	304
	C	ITITAN	=1HT, DENOTING TITANIUM PLATE MATERIAL	VIPRF	305
305	C	ITITLE	ARRAY FOR STORING PLOT TITLE LINE CHARACTERS	VIPRF	306
	C	ITURB	=2HTB, FOR LOW FREQ. ATMOS. TURBULENCE	VIPRF	307
	C	IX	INTEGER VARIABLE FOR SUBSCRIPT IN PRINT OF X, X, X OR X	VIPRF	308
	C		PT T L E	VIPRF	309
	C	J	INTEGER WORKING VARIABLE	VIPRF	310
310	C	JFLITE	INPUT VALUE FOR FLIGHT PHASE	VIPRF	311
	C	K	INTEGER WORKING VARIABLE	VIPRF	312
	C	L	INTEGER WORKING VARIABLE	VIPRF	313
	C	LXNAME	ARRAY FOR STORING CHARACTERS FOR NAME OF X-AXIS ON PLOT	VIPRF	314
	C	LYNAME	ARRAY FOR STORING CHARACTERS FOR NAME OF Y-AXIS ON PLOT	VIPRF	315
315	C	M	INTEGER WORK VARIABLE	VIPRF	316
	C	MATERL	INPUT VALUE FOR PLATE MATERIAL	VIPRF	317
	C	NDEFZPF	NUMBER OF P* VALUES IN ARRAY "DEFZPF"	VIPRF	318
	C	NCF	NUMBER OF TABULAR VALUES FOR CATEGORY 3, Y(F) PARAMETERS	VIPRF	319
	C	NDDP	NUMBER OF DECIMAL VALUES STORED IN ARRAY "DDPVAL"	VIPRF	320
320	C	NDEPS	NUMBER OF DECIMAL VALUES IN ARRAY "DEPSERS"	VIPRF	321
	C	NMCD01	NUMBER OF DECIMAL VALUES IN ARRAY "CDM001"	VIPRF	322
	C	NMCD02	NUMBER OF DECIMAL VALUES IN ARRAY "CDM002"	VIPRF	323
	C	NPTS	NUMBER OF POINTS CALCULATED FOR FUNCTION L(F)-M(F)-H(F)	VIPRF	324
325	C	NRSVAL	NUMBER OF TABULAR VALUES OF R USED WHEN CALC. F* FOR H(F)	VIPRF	325
	C		S 0	VIPRF	326
	C		CORRECTION TO M(F) AND H(F) FOR R	VIPRF	327
	C		S	VIPRF	328
	C	NWF100	NUMBER OF DB VALUES IN ARRAY WF100	VIPRF	329
	C	NWF1K	NUMBER OF DB VALUES IN ARRAY WF1000	VIPRF	330
330	C	NWF5K	NUMBER OF DB VALUES IN ARRAY WF5000	VIPRF	331
	C	N1A10	NUMBER OF DECIMAL VALUES IN ARRAY "DB1A10"	VIPRF	332
	C	N1A70	NUMBER OF DECIMAL VALUES IN ARRAY "DB1A70"	VIPRF	333
	C	N1F15	NUMBER OF DECIMAL VALUES IN ARRAY "DB1F15"	VIPRF	334
	C	N1F16	NUMBER OF DECIMAL VALUES IN ARRAY "DB1F16"	VIPRF	335
335	C	N1F4	NUMBER OF DECIMAL VALUES IN ARRAY "DB1F4"	VIPRF	336
	C	N1F111	NUMBER OF DECIMAL VALUES IN ARRAY "DB1111"	VIPRF	337
	C	N2A10	NUMBER OF DECIMAL VALUES IN ARRAY "DB2A10"	VIPRF	338
	C	N2A70	NUMBER OF DECIMAL VALUES IN ARRAY "DB2A70"	VIPRF	339
	C	N2F15	NUMBER OF DECIMAL VALUES IN ARRAY "DB2F15"	VIPRF	340
340	C	N2F16	NUMBER OF DECIMAL VALUES IN ARRAY "DB2F16"	VIPRF	341
	C	N2F4	NUMBER OF DECIMAL VALUES IN ARRAY "DB2F4"	VIPRF	342
	C	N2F111	NUMBER OF DECIMAL VALUES IN ARRAY "DB2111"	VIPRF	343



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	C	PFAK	MAXIMUM OF Y(F) FOR SPECIFIED CATEGORY	VIPRF	344
	C		<sup>2</sup>	VIPRF	345
345	C	PFM	MAXIMUM OF P(F),PSF./HZ.	VIPRF	346
	C	PFMDR	MAXIMUM OF P(F),DB.	VIPRF	347
	C	PI	CONSTANT=3.14159265	VIPRF	348
	C	FNCRM	RATIO:AV.PRESSURE AT ALTITUDE/AV.PRESSURE AT SEA LEVEL ALTI	VIPRF	349
	C	QSQ	SQUARE OF Q,DYNAMIC PRESSURE	VIPRF	350
350	C	R	AVERAGE DENSITY	VIPRF	351
	C	REX	RE,REYNOLDS NUMBER AT DISTANCE X	VIPRF	352
	C		Y	VIPRF	353
	C	RNCRM	RATIO:AV.DENSITY AT ALTITUDE/AV.DENSITY AT SEA LEVEL ALTITU	VIPRF	354
	C	RS	INPUT VALUE FOR DISTANCE FROM SKIN,R	VIPRF	355
355	C		S	VIPRF	356
	C	PSMAX	MAX.VALUE OF P COVERED BY ARRAY OF TABULAR,DECIBEL VALUES,	VIPRF	357
	C		S	VIPRF	358
	C	RSVALS	ARRAY FOR STOPPING TABULAR DECIBEL VALUES USED WHEN CALCULAT	VIPRF	359
	C		F' FOR H(F) AND CORRECTION TO M(F) AND H(F) FOR R	VIPRF	360
360	C		0	VIPRF	361
	C		S	VIPRF	362
	C	SAHI	SET EQUAL TO FORM FACTOR,HF ROLL-OFF FOR S(F) OF SPEC.FLIGHT	VIPRF	362
	C	SALO	SET EQUAL TO FORM FACTOR,LF ROLL-OFF FOR S(F) OF SPEC.FLIGHT	VIPRF	363
	C	SBIHI	SET EQUAL TO SLOPE FACTOR,HF ROLL-OFF FOR S(F) OF SPEC.FLIGHT	VIPRF	364
	C	SPLO	SET EQUAL TO SLOPE FACTOR,LF ROLL-OFF FOR S(F) OF SPEC.FLIGHT	VIPRF	365
365	C	SPFTD	RATIO:S(F)/S(F)' FOR CALC. S(F) CORRES.TO A D>0,USING IN	VIPRF	366
	C		BT M BT M BT M	VIPRF	367
	C		VALUE FOR PHMAX	VIPRF	368
	C	SDelta	VALUE OF S(F) AT FMINGF	VIPRF	369
	C		BT	VIPRF	370
370	C	SFZHI	SET EQUAL TO LOCATOR FREQ.,HIGH FREQ.ROLL-OFF,FOR S(F)	VIPRF	371
	C		OF SPEC.FLIGHT PHASE	VIPRF	372
	C	SFZLO	SET EQUAL TO LOCATOR FREQ., LOW FREQ.ROLL-OFF,FOR S(F)	VIPRF	373
	C		OF SPEC.FLIGHT PHASE	VIPRF	374
	C	SIGN	ARRAY FOR STORING VALUE 0 OR VALUE 1, DENOTING LOW-FREQ. AND	VIPRF	375
375	C		HIGH-FREQ.ROLL-OFF,RESP.,WHEN CALC. L(F)-M(F)-H(F)	VIPRF	376
	C	SOUND	ARRAY FOR STOPPING TABULAR VALUES FOR VELOCITY OF SOUND	VIPRF	377
	C	SPEAK	SET EQUAL TO MAXIMUM VALUE OF S(F) FOR SPEC.FLIGHT PHASE	VIPRF	378
	C	SXHI	SET EQUAL TO NORM.FREQ.RATIO,HIGH FREQ.ROLL-OFF FOR S(F)	VIPRF	379
	C		OF SPEC.FLIGHT PHASE	VIPRF	380
380	C	SXLO	SET EQUAL TO NORM.FREQ.RATIO, LOW FREQ.ROLL-OFF FOR S(F)	VIPRF	381
	C		OF SPEC.FLIGHT PHASE	VIPRF	382
	C	T	INPUT VALUE FOR AIRCRAFT PLATE THICKNESS	VIPRF	383
	C	TAKAHI	FORM FACTOR,HIGH FREQ.ROLL-OFF,FOR S(F) OF TAKE-OFF FLIGHT	VIPRF	384
	C	TAKALO	FORM FACTOR, LOW FREQ.ROLL-OFF,FOR S(F) OF TAKE-OFF FLIGHT	VIPRF	385
385	C	TAKAHI	SLOPE FACTOR,HIGH-FREQ.ROLL-OFF,FOR S(F) OF TAKE-OFF FLIGHT	VIPRF	386
	C	TAKALO	SLOPE FACTOR, LOW-FREQ.ROLL-OFF,FOR S(F) OF TAKE-OFF FLIGHT	VIPRF	387
	C	TAKMAX	MAXIMUM VALUE OF SPECIAL FUNCTION S(F) FOR TAKE-OFF FLIGHT	VIPRF	388
	C	TAKXHI	NORM.FREQ.RATIO,HIGH FREQ.ROLL-OFF,FOR S(F),TAKE-OFF FLIGHT	VIPRF	389
	C	TAKXLO	NORM.FREQ.RATIO, LOW FREQ.ROLL-OFF,FOR S(F),TAKE-OFF FLIGHT	VIPRF	390
390	C	TBAHI	FORM FACTOR,HIGH FREQ.ROLL-OFF,FOR S(F) OF LOW FREQ.	VIPRF	391
	C		ATMOS.TURBULENCE PHASE	VIPRF	392
	C	TBSHI	SLOPE FACTOR,HIGH FREQ.ROLL-OFF,FOR S(F) FOR LOW FREQ.	VIPRF	393
	C		ATMOS. TURBULENCE	VIPRF	394
	C	TBFC	CENTER FREQ.OF HIGH FREQ.ROLL-OFF SECTION OF S(F) FOR	VIPRF	395
395	C		LOW FREQ.ATMOS.TURBULENCE PHASE	VIPRF	396
	C	TBREF	VALUE(REFERENCE) OF S(F) AT FREQ=F' USED WHEN CALC. MAXIMUM	VIPRF	397
	C		0	VIPRF	398
	C		VALUE OF S(F) AT FREQ.=TBFC	VIPRF	399
	C	TITLEN	LENGTH OF TICK MARK ON RIGHT HAND Y AXIS OF PLOT	VIPRF	400

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410	C	TWOP	ARRAY FOR STORING VALUES OF PETA AND PETA' FOR L(F),M(F) AND	VIPRF	401
	C		H(F),USED WHEN CALCULATING L(F)-M(F)-H(F) TRANSFER FUNCTION	VIPRF	402
	C	TWOPPE	TWICE PETA' FOR P(F)	VIPRF	403
	C	U	FREE-STREAM VELOCITY	VIPRF	404
	C	V	AVERAGE KINEMATIC VISCOSITY	VIPRF	405
415	C	VALK	ARRAY FOR STORING VALUES OF K USED WHEN CALCULATING F' FOR	VIPRF	406
	C		C	VIPRF	407
	C	VISCO	ARRAY FOR STORING TABULAR VALUES OF AVERAGE KINEMATIC VISCO	VIPRF	408
	C	VNCRM	RATIO:AV,KINEMATIC VISCOSITY AT ALTITUDE/AV,KINEMATIC VISCO	VIPRF	409
	C		AT SEALLEVEL ALTITUDE	VIPRF	410
415	C	WE	INFLT VALUE FOR EQUIPMENT WEIGHT	VIPRF	411
	C	WEK	ARRAY FOR STORING TABULAR VALUES OF EQUIPMENT WEIGHT USED W	VIPRF	412
	C		CALCULATING F' FOR H(F)	VIPRF	413
	C		C	VIPRF	414
	C	WEMAX	MAXIMUM VALUE OF EQUIPMENT WEIGHT,WE, FOR TABULAR DECIBEL	VIPRF	415
415	C		VALUES STORED IN ARRAY "WE5000"	VIPRF	416
	C	WE100	ARRAY FOR STORING DECIBEL VALUES CORRESPONDING TO EQUIP.WEI	VIPRF	417
	C		UP TO 100LBS.,USED WHEN CALC.CORRECTION TO MAXIMUM OF H(F)	VIPRF	418
	C	WE1000	ARRAY FOR STORING DECIBEL VALUES CORRESPONDING TO EQUIP.WEI	VIPRF	419
	C		UP TO 1000LBS.,USED WHEN CALC.CORRECTION TO MAXIMUM OF H(F)	VIPRF	420
420	C	WE5000	ARRAY FOR STORING DECIBEL VALUES CORRESPONDING TO EQUIP.WEI	VIPRF	421
	C		UP TO 5000LBS.,USED WHEN CALC.CORRECTION TO MAXIMUM OF H(F)	VIPRF	422
	C	WS	DENSITY OF AIRCRAFT PLATE MATERIAL	VIPRF	423
	C	X	DISTANCE X, X <sub>1</sub> OR X <sub>2</sub>	VIPRF	424
	C		I PT TL	VIPRF	425
425	C	XAXIS	LENGTH OF X AXIS OF PLOTS	VIPRF	426
	C	XBI	PT DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE AERODYNAM	VIPRF	427
	C		PROFILE TO THE WING CHORD CENTER	VIPRF	428
	C	XCYCLE	LENGTH OF LOGARITHMIC CYCLE FOR XAXIS OF PLOT	VIPRF	429
	C	XE	E DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE AERODYNAM	VIPRF	430
430	C		PROFILE TO THE WING CHORD CENTER	VIPRF	431
	C	XFEPMX	ARRAY FOR STORING THE MAXIMUM VALUES OF L(F),L <sup>2</sup> (F),M(F) AND	VIPRF	432
	C		TRANSFER FUNCTIONS USED WHEN CALCULATING L(F)-M(F)-H(F)	VIPRF	433
	C	XHFCOE	MAXIMUM VALUE OF H(F) CORRECTED FOR W <sub>1</sub> ,W <sub>2</sub> AND R <sub>1</sub>	VIPRF	434
435	C		E S S	VIPRF	435
	C	XHFHI	NORM.FREQ.RATIO,HIGH-FREQ.ROLL-OFF,H(F) OF CURRENT FLIGHT P	VIPRF	436
	C	XHFLC	NORM.FREQ.RATIO, LOW-FREQ.ROLL-OFF,H(F) OF CURRENT FLIGHT P	VIPRF	437
	C	XHFMAX	MAXIMUM VALUE OF H(F) BEFORE CORRECTION	VIPRF	438
	C	YHI	SET EQUAL TO NORM.FREQ.RATIO,HIGH-FREQ.POLL-OFF, FOR SPEC.Y(F)	VIPRF	439
440	C	XLFCOE	MAXIMUM VALUE OF L(F) CORRECTED FOR X <sub>1</sub>	VIPRF	440
	C		E	VIPRF	441
	C	XLFHI	NORM.FREQ.RATIO,HIGH-FREQ.ROLL-OFF, FOR L(F)	VIPRF	442
	C	XLFLC	NORM.FREQ.RATIO, LOW-FREQ.ROLL-OFF, FOR L(F)	VIPRF	443
	C	XLFMAX	MAXIMUM VALUE OF L(F) BEFORE CORRECTION	VIPRF	444
445	C	YLC	SET EQUAL TO NORM.FREQ.RATIO,LOW-FREQ.ROLL-OFF, FOR SPEC.Y(F)	VIPRF	445
	C	XL2FCOE	MAXIMUM VALUE OF L <sup>2</sup> (F) AFTER CORRECTION FOR X <sub>1</sub>	VIPRF	446
	C		E	VIPRF	447
	C	XL2FHI	NORM.FREQ.RATIO,HIGH-FREQ.ROLL-OFF, FOR L <sup>2</sup> (F)	VIPRF	448
	C		E	VIPRF	449
450	C	XL2FLC	NORM.FREQ.RATIO, LOW-FREQ.POLL-OFF, FOR L <sup>2</sup> (F)	VIPRF	450
	C		E	VIPRF	451
	C	XL2FMX	MAXIMUM VALUE OF L <sup>2</sup> (F)	VIPRF	452
	C		E	VIPRF	453
	C	XMAKNC	MACH NO. OF CURRENT AIRCRAFT PROFILE ANALYSIS	VIPRF	454
455	C	XHFCOE	MAXIMUM VALUE OF H(F),CORRECTED FOR "WS"AND"RS"	VIPRF	455
	C	XHFHI	NORM.FREQ.RATIO,HIGH FREQ.ROLL-OFF, FOR H(F)	VIPRF	456
	C			VIPRF	457

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	C	YMFLO	NCRV,FREQ,RATIO, LOW FREQ.ROLL-OFF, FOR 1(F)	VIPRF	458
	C	YMFMAX	MAXIMUM VALUE OF 4(F)	VIPRF	459
	C	YPF	NCRV,FREQ,RATIO,HIGH-FREQ.ROLL-OFF, FOR 2(F)	VIPRF	460
460	C	XTL	"T" OR "L" DISTANCE FROM THE LEADING EDGE OF THE FUSELAGE	VIPRF	461
	C		AERO-DYNAMIC PROFILE TO THE LANDING GEAR	VIPRF	462
	C	XVAL	X COORDINATE OF LOWER LEFT-CORNER OF INFO.LINE PLOT ON	VIPRF	463
	C		PLOT BY DISSPLA SUB-ROUTINE "RLMESS"	VIPRF	464
	C	XX	WORKING, REAL VARIABLE	VIPRF	465
465	C	XXFHT	NCRV,FREQ,RATIO,HIGH FREQ.ROLL-OFF, FOR 4(F)--CONSTANT VALUE	VIPRF	466
	C	XXFLO	NCRV,FREQ,RATIO, LOW FREQ.ROLL-OFF, FOR 4(F)--CONSTANT VALUE	VIPRF	467
	C	XXFHT	NCRV,FREQ,RATIO,HIGH FREQ.ROLL-OFF, FOR 4(F)--CONSTANT VALUE	VIPRF	468
	C	XXFLO	NCRV,FREQ,RATIO, LOW FREQ.ROLL-OFF, FOR 4(F)--CONSTANT VALUE	VIPRF	469
	C	X1	WORKING VARIABLE	VIPRF	470
470	C	X2	WORKING VARIABLE	VIPRF	471
	C	X3	WORKING VARIABLE	VIPRF	472
	C	X4	WORKING VARIABLE	VIPRF	473
	C	YAXIS	LENGTH OF Y AXIS ON PLOTS	VIPRF	474
	C	YSTEP	STEP SIZE, Y DATA UNITS/INCH FOR PLOT Y AXIS	VIPRF	475
475	C	YVAL	Y COORDINATE OF LOWER LEFT-CORNER OF INFO.LINE PLOT ON	VIPRF	476
	C		PLOT BY DISSPLA SUB-ROUTINE "RLMESS"	VIPRF	477
				VIPRF	478
				VIPRF	479
				VIPRF	480
480			DIMENSION FREQ(100),DECRFL(150),DRFL(150),DRSPL(150),FSPL(150)	VIPRF	481
			DIMENSION ALT(6),AMAXNO(6),ALPHA(4),DOBVAL(41),IHOLO(5)	VIPRF	482
			DIMENSION DB1F4(41),DB2F4(41),DB1F15(41),DB2F15(41)	VIPRF	483
			DIMENSION DB1F16(55),DB2F16(41),DB1111(41),DB2111(41)	VIPRF	484
			DIMENSION DB1A70(41),DB2A70(41),DB1A10(41),DB2A10(41)	VIPRF	485
485			DIMENSION WSK(14),VALK(14),C1AAWE(11),C1AMWE(11)	VIPRF	486
			DIMENSION SF7PF(29),FORIHF(43),DBRS(43),RSVALS(43),WF100(7)	VIPRF	487
			DIMENSION WF100(7),WF500(9),DBMFPS(29)	VIPRF	488
			DIMENSION CB(4),XFFRMX(4),THOR(4),FLX(4),FZ(4),HILC(4),SIGN(4)	VIPRF	489
			DIMENSION ALTUD(61),AVP(61),AVDENS(61),SOUND(61),VISCOS(61)	VIPRF	490
490			DIMENSION C3WF(10),C3AYMX(10),C3AAP(10),C3AXP(10),C3BE(10),	VIPRF	491
			103PX(10),C3PPP(10),C3RXP(10),C3RYMX(10),C3RAP(10),C3PA(10),	VIPRF	492
			203AP(10)	VIPRF	493
				VIPRF	494
				VIPRF	495
495			COMMON/PFLCIT/F,XMAKNO,X,RS,WE,WS,IFLITL,CATGRY,ILINE1(7),	VIPRF	496
			1ITITL1(7),IPLANE(3),LYNAME(4),LYNAME(4),XCYCLE,YSTEP,YAXIS,	VIPRF	497
			2XAXIS,HITF,HITF1,TICLEN,X1,X2,X3,X4,XX,IPHASE,INOPLT,IPLANK	VIPRF	498
				VIPRF	499
			COMMON/XARCS/FN,XLFMAX,F2N,XL2FMX,PUFMAX,XFT,XTL,FCMOVE,	VIPRF	500
500			1NMCCF1,CXMOD1,CBMOD1(100),NMCCF2,CXMOD2,CBMOD2(100),	VIPRF	501
			2ILINE2(A),ISANCL,IRUFET,ITAKOF,ILAND,ITURP,IFNISH	VIPRF	502
				VIPRF	503
				VIPRF	504
			DATA NSF7PF/29/,9F7PF/1.745,1.150,0.900,0.745,0.651,0.592,0.551,	VIPRF	505
505			10.530,0.500,0.492,0.480,0.470,0.457,0.454,0.446,0.440,0.435,	VIPRF	506
			20.424,0.421,0.4164,0.4118,0.4072,0.4026,0.3980,0.3934,0.3888,	VIPRF	507
			30.3842,0.3796,0.375/	VIPRF	508
				VIPRF	509
			DATA RSVALS/0.,0.25,0.50,0.75,1.0,1.25,1.50,1.75,2.0,2.25,2.50,	VIPRF	510
510			12.75,3.0,3.5,4.0,4.5,5.0,5.5,6.0,7.0,8.0,9.0,10.0,11.0,12.0,13.0,	VIPRF	511
			214.0,15.0,16.0,17.0,18.0,19.0,20.0,21.0,22.0,23.0,24.0,25.0,26.0,	VIPRF	512
			327.0,28.0,29.0,30.0/	VIPRF	513
				VIPRF	514



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515	DATA DPRS/1.,-2.00,-2.60,-3.30,-3.90,-4.40,-4.80,-5.20,-5.50, 1-5.90,-6.15,-6.40,-6.80,-7.30,-8.00,-8.50,-9.0,-9.5,-10.0,-10.8, 2-11.5,-12.0,-12.75,-13.20,-13.70,-14.00,-14.40,-14.60,-14.90, 3-15.20,-15.35,-15.70,-15.85,-15.95,-16.0,-16.10,-16.20,-16.30, 4-16.40,-16.50,-16.60,-16.65,-16.70/	VIPRF	515			
		VIPRF	516			
		VIPRF	517			
		VIPRF	518			
		VIPRF	519			
		VIPRF	520			
520	DATA FPRIF/5500.,3800.,3550.,3350.,3200.,3100.,2950.,2800., 12730.,2650.,2550.,2470.,2400.,2320.,2200.,2100.,2000.,1950., 21900.,1800.,1754.,1690.,1600.,1580.,1550.,1510.,1480.,1450., 31420.,1380.,1360.,1340.,1320.,1305.,1285.,1268.,1256.,1250., 41244.,1238.,1232.,1225.,1220./	VIPRF	521			
		VIPRF	522			
		VIPRF	523			
		VIPRF	524			
		VIPRF	525			
525		VIPRF	526			
		VIPRF	527			
	DATA WCK/2.5,3.8,5.0,7.5,10.0,15.0,20.0,30.0,40.0,60.0,80.0,100.0, 1160.0,200.0/	VIPRF	528			
		VIPRF	529			
	DATA VALK/1.0,0.99,0.98,0.95,0.92,0.87,0.84,0.76,0.73,0.675, 10.650,0.600,0.575,0.550/	VIPRF	530			
530		VIPRF	531			
		VIPRF	532			
	DATA NMFRS/29/,DXMFRS/0.10/	VIPRF	533			
	DATA FEMFRS/-17.0,-16.5,-15.0,-13.7,-12.4,-11.2,-10.2,-9.2,-8.1, 1-7.3,-6.6,-5.8,-5.0,-4.5,-3.9,-3.2,-2.8,-2.2,-2.0,-1.7,-1.2, 2-1.1,-0.9,-0.70,-0.40,-0.30,-0.20,-0.10,0./	VIPRF	534			
535		VIPRF	535			
		VIPRF	536			
		VIPRF	537			
		VIPRF	538			
	DATA NC1A/11/,DNC1A/20.0/,XINC1A/10.0/	VIPRF	539			
	DATA C1AAWE/1.0,1.34,1.43,1.57,1.62,1.70,1.75,1.77,1.82,1.86,1.92/	VIPRF	540			
540		VIPRF	541			
	DATA C1AAWE/0.,-1.0,-1.8,-2.7,-3.7,-4.0,-4.5,-5.2,-5.5,-6.5/	VIPRF	542			
	DATA NWE100/77,DWE100/15.0/	VIPRF	543			
	DATA WE100/0.,-0.5,-1.25,-2.0,-2.5,-3.75,-4.5/	VIPRF	544			
	DATA NWE1K/77,DWE1K/150.0/	VIPRF	545			
545		VIPRF	546			
	DATA WE100/-4.5,-10.0,-12.6,-14.4,-15.2,-16.1,-16.6/	VIPRF	547			
	DATA NWE5K/57,DWE5K/500.0/	VIPRF	548			
	DATA WE500/-16.6,-17.65,-18.9,-19.7,-20.15,-20.6,-21.0,-21.25, 1-21.50/	VIPRF	549			
		VIPRF	550			
550	DATA N00R/41/,D0L00R/1.0/	VIPRF	551			
	DATA C0GVAL/0.,-0.02,-0.05,-0.10,-0.20,-0.22,-0.30, 1-0.44,-0.50,-0.60,-0.80,-1.00,-1.20,-1.40,-1.60,-1.90,-2.20, 2-2.50,-3.00,-3.50,-4.00,-4.50,-5.10,-5.80,-6.60,-7.50,-8.30, 3-9.20,-10.10,-11.50,-11.80,-12.70,-13.50,-14.30,-15.00, 4-15.70,-16.50,-17.20,-17.90,-18.50,-19.10/	VIPRF	552			
555		VIPRF	553			
		VIPRF	554			
		VIPRF	555			
		VIPRF	556			
	DATA C34F/10.0,15.0,20.0,30.0,40.0,60.0,90.0,120.0,160.0,200.0/	VIPRF	557			
	DATA C3AYX/12.0,11.6,11.5,11.0,10.7,10.0,9.6,9.3,7.5,6.0/	VIPRF	558			
	DATA C3AP/0.300,0.285,0.278,0.264,0.257,0.240,0.235,0.220, 10.212,0.200/	VIPRF	559			
560		VIPRF	560			
	DATA C3AXF/0.500,0.460,0.445,0.406,0.385,0.350,0.332,0.295, 10.280,0.250/	VIPRF	561			
		VIPRF	562			
	DATA C3AAF/1.900,1.907,1.909,1.918,1.920,1.936,1.940,1.960, 11.970,2.000/	VIPRF	563			
		VIPRF	564			
	DATA C3BYX/24.0,16.7,14.6,11.2,10.2,8.0,7.4,6.3,6.1,6.0/	VIPRF	565			
565		VIPRF	566			
	DATA C3BE/0.100,0.130,0.140,0.175,0.190,0.225,0.235,0.265, 10.283,0.300/	VIPRF	567			
		VIPRF	568			
	DATA C3BBF/0.100,0.167,0.190,0.260,0.280,0.350,0.375,0.435, 10.463,0.500/	VIPRF	569			
		VIPRF	570			
570		VIPRF	571			
	DATA C3BX/1.42,1.52,1.55,1.65,1.69,1.78,1.81,1.89,1.95,2.00/	VIPRF	570			
	DATA C3BXF/0.700,0.625,0.599,0.524,0.494,0.419,0.400,0.333,	VIPRF	571			

PROGRAM	VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
		10.288,0.250/			VIPRF	572
		DATA C3BA/1.00,0.64,0.54,0.36,0.30,0.20,0.175,0.120,0.110,0.10/			VIPRF	573
		DATA C3BAF/1.40,1.46,1.50,1.56,1.58,1.64,1.68,1.73,1.75,1.80/			VIPRF	574
					VIPRF	575
575		DATA ALTITUDE/ 0.,500.,1000.,1500.,2000.,2500.,3000.,3500.,4000.,			VIPRF	576
		* 4500., 5000., 5500., 6000., 6500., 7000., 7500., 8000., 8500.,			VIPRF	577
		* 9000., 9500., 10000., 11000., 12000., 13000., 14000., 15000., 16000.,			VIPRF	578
		* 17000., 18000., 19000., 20000., 21000., 22000., 23000., 24000., 25000.,			VIPRF	579
		* 26000., 27000., 28000., 29000., 30000., 31000., 32000., 33000., 34000.,			VIPRF	580
580		* 35000., 36000., 37000., 38000., 39000., 40000., 41000., 42000., 43000.,			VIPRF	581
		* 44000., 45000., 46000., 47000., 48000., 49000., 50000./			VIPRF	582
					VIPRF	583
		DATA AVP/2116.2,2078.3,2040.9,2004.0,1967.7,1931.9,1896.6,1861.9,			VIPRF	584
		* 1827.7,1794.0,1760.8,1728.1,1695.9,1664.2,1632.9,1602.2,1571.9,			VIPRF	585
585		* 1542.1,1512.7,1483.8,1455.3,1399.7,1345.9,1293.7,1243.2,1194.3,			VIPRF	586
		* 1146.9,1101.1,1056.8,1013.9, 972.5, 932.4, 893.7, 856.3, 820.2,			VIPRF	587
		* 785.3,751.6,719.1,687.8,657.6,628.4,600.3,573.3,547.2,522.1,498.0,			VIPRF	588
		* 474.7,452.4,431.2,411.0,391.7,373.3,355.8,339.1,323.2,308.0,293.6,			VIPRF	589
		* 279.8,266.7,254.1,242.2/			VIPRF	590
590					VIPRF	591
		DATA AMPLITUDE/.2513E-02,.2467E-02,.2422E-02,.2377E-02,.2334E-02,			VIPRF	592
		* .2291E-02,.2249E-02,.2210E-02,.2173E-02,.2137E-02,.2102E-02,			VIPRF	593
		* .2067E-02,.2033E-02,.1999E-02,.1965E-02,.1932E-02,.1900E-02,			VIPRF	594
		* .1868E-02,.1836E-02,.1805E-02,.1774E-02,.1748E-02,.1663E-02,			VIPRF	595
595		* .1611E-02,.1579E-02,.1548E-02,.1518E-02,.1411E-02,.1364E-02,			VIPRF	596
		* .1318E-02,.1277E-02,.1230E-02,.1188E-02,.1147E-02,.1107E-02,			VIPRF	597
		* .1068E-02,.1030E-02,.9933E-03,.9577E-03,.9228E-03,.8890E-03,			VIPRF	598
		* .8576E-03,.8199E-03,.7853E-03,.7529E-03,.7215E-03,.6912E-03,			VIPRF	599
		* .6621E-03,.6341E-03,.6074E-03,.5818E-03,.5573E-03,.5338E-03,			VIPRF	600
600		* .5113E-03,.4898E-03,.4692E-03,.4495E-03,.4306E-03,.4125E-03,			VIPRF	601
		* .3952E-03,.3796E-03/			VIPRF	602
					VIPRF	603
		DATA SOUND/1090.6,1090.4,1090.3,1090.1,1090.,1089.8,1089.7,1089.0,			VIPRF	604
		* 1087.8,1086.7,1085.5,1084.3,1083.1,1081.9,1080.7,1079.5,1078.4,			VIPRF	605
605		* 1077.1,1075.9,1074.7,1073.4,1069.6,1065.9,1062.1,1058.4,1054.5,			VIPRF	606
		* 1050.7,1046.9,1043.1,1039.2,1035.4,1031.5,1027.5,1023.6,1019.7,			VIPRF	607
		* 1015.8,1011.8,1007.8,1003.8, 999.7, 995.7, 991.1, 990.7, 988.2,			VIPRF	608
		* 985.7,983.3,980.8,978.3,975.8,973.3,970.9,968.5,966.0,963.6,961.1,			VIPRF	609
		* 958.8,956.3,954.0,951.6,949.2,946.9/			VIPRF	610
610					VIPRF	611
		DATA VISCOS/.1467E-03,.1492E-03,.1517E-03,.1543E-03,.1570E-03,			VIPRF	612
		* .1597E-03,.1625E-03,.1651E-03,.1675E-03,.1699E-03,.1724E-03,			VIPRF	613
		* .1749E-03,.1775E-03,.1802E-03,.1828E-03,.1856E-03,.1883E-03,			VIPRF	614
		* .1911E-03,.1940E-03,.1969E-03,.1998E-03,.2051E-03,.2106E-03,			VIPRF	615
615		* .2163E-03,.2222E-03,.2283E-03,.2346E-03,.2411E-03,.2478E-03,			VIPRF	616
		* .2551E-03,.2621E-03,.2696E-03,.2774E-03,.2854E-03,.2938E-03,			VIPRF	617
		* .3025E-03,.3115E-03,.3208E-03,.3306E-03,.3407E-03,.3512E-03,			VIPRF	618
		* .3639E-03,.3775E-03,.3917E-03,.4066E-03,.4223E-03,.4387E-03,			VIPRF	619
		* .4559E-03,.4738E-03,.4925E-03,.5118E-03,.5320E-03,.5530E-03,			VIPRF	620
620		* .5749E-03,.5976E-03,.6213E-03,.6460E-03,.6717E-03,.6984E-03,			VIPRF	621
		* .7263E-03,.7554E-03/			VIPRF	622
					VIPRF	623
		DATA ISTEFL,ITITAN,IALUM,IMAG/1HS,1HT,1HA,1HM/			VIPRF	624
					VIPRF	625
625		DATA C1A/2H1A/,C2A/2H2A/,C2B/2H2B/,C3A/2H3A/,C3B/2H3B/,C5/1H5/			VIPRF	626
		DATA C1B/2H1B/,C4A/2H4A/,C4B/2H4B/,C6/1H6/,I9LANK/1H /			VIPRF	627
					VIPRF	628

PROGRAM VIPRF 74/74 OPT=1 ETN 4.5+414 08/16/77 13.11.28

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DATA IF4/6H F-4/,IF15/7H F-15/,IF16/7H F-16/
DATA IF111/8H F-111/,IA70/7H A-70/,IA10/7H A-10/
DATA ISANDL,IPHET,ILAND,ITAKOF/5HSANDL,2HPT,7HLANDING,7HTAKLOFF/
DATA IFUPP/2HTR/
DATA FI/3.14159265/,IFATSH/6HFINISH/
DATA N1F4/41/,DX1F4/1.57/
DATA D1F4/ 0.0, -0.80, -1.60, -2.80, -4.10, -5.40, -7.30, -9.80,
1-12.00,-15.00,-20.00,-25.00,-24.40,-22.10,-20.20,-19.10,-18.40,
2-18.00,-17.00,-17.00,-19.20,-18.90,-20.40,-22.90,-25.30,-26.00,
3-25.20,-22.60,-19.60,-17.70,-15.60,-14.00,-12.70,-11.30,-10.10,
4 -9.10, -8.30, -7.50, -6.80, -6.00, -5.30/
DATA N2F4/41/,DX2F4/1.57/
DATA D2F4/ 0.0, -0.90, -2.00, -4.00, -6.50, -9.70,-15.00,-26.00,
1-22.00,-16.70,-13.70,-11.00,-11.00,-11.30,-11.30,-12.60,-14.20,
2-16.00,-18.80,-22.40,-20.00,-25.90,-22.00,-19.10,-17.90,-17.30,
3-17.40,-17.90,-19.80,-25.90,-25.60,-19.00,-14.80,-11.00, -8.75,
4 -7.00, -5.75, -4.60, -3.80, -3.00, -2.40/
DATA N1F15/41/,DX1F15/1.375/
DATA D1F15/ 0.0, -0.90, -1.75, -2.80, -3.90, -5.00, -6.00, -7.80,
1 -0.25,-11.10,-13.75,-16.90,-21.20,-25.40,-26.00,-25.60,-23.60,
2-20.10,-18.30,-16.90,-16.25,-16.10,-16.15,-16.80,-17.60,-18.70,
3-20.00,-21.75,-25.00,-25.80,-25.70,-21.40,-19.00,-16.80,-15.40,
4-14.30,-13.00,-12.20,-11.10,-10.30, -9.50/
DATA N2F15/41/,DX2F15/1.375/
DATA D2F15/ 0.0, -1.10, -2.40, -4.25, -6.30, -8.80,-12.40,-18.00,
1-26.00,-17.00,-13.00,-11.35,-10.90,-10.75,-10.93,-11.10,-11.90,
2-14.00,-16.50,-23.00,-24.00,-20.30,-19.10,-18.50,-18.40,-18.80,
3-19.90,-25.30,-26.00,-21.40,-21.40,-19.80,-18.20,-17.20,-16.20,
4-15.70,-15.00,-14.60,-13.90,-13.40,-13.00/
DATA N1F16/55/,DX1F16/0.85/
DATA D1F16/ 0.0, -0.40, -1.00, -1.40, -2.20, -2.60, -3.40, -4.20,
1 -5.00, -6.00, -7.40, -8.60,-10.60,-12.30,-14.80,-18.80,-22.60,
2-25.20,-25.90,-23.10,-21.60,-20.90,-20.15,-19.80,-19.30,-19.00,
3-18.90,-18.80,-18.60,-18.50,-18.60,-18.75,-19.00,-19.60,-20.20,
4-21.40,-22.80,-24.40,-25.50,-26.00,-26.20,-26.00,-25.80,-25.30,
5-21.90,-21.20,-19.30,-17.80, -0.00,-15.10,-14.10,-13.20,-12.30,
6-11.60,-11.00/
DATA N2F16/41/,DX2F16/1.1475/
DATA D2F16/ 0.0, -1.20, -2.50, -4.30, -6.00, -8.20,-10.90,-15.00,
1-22.10,-26.00,-20.75,-17.60,-17.15,-17.40,-21.60,-25.10,-25.90,
2-26.00,-25.90,-25.00,-23.70,-21.90,-21.60,-22.75,-24.50,-25.80,
3-26.00,-25.80,-24.10,-21.80,-21.60,-21.80,-25.10,-26.00,-21.00,
4-16.25,-12.75, -9.70, -7.30, -5.40, -3.80/
DATA N1F111/41/,DX1F111/1.7621/
DATA D1F111/ 1.0, -0.20, -0.75, -1.70, -2.60, -3.75, -4.90, -6.00,
1 -7.80, -9.60,-11.25,-13.60,-16.25,-20.00,-25.90,-26.00,-24.00,
2-20.50,-18.30,-16.80,-15.60,-14.90,-14.40,-14.05,-14.70,-15.20,

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PROGRAM VIPRF      74/74      OPT=1      FTN 4.5+4.14      08/16/77 13.11.28

685      3-16.00,-17.60,-19.90,-22.00,-25.85,-26.20,-26.10,-25.20,-20.70,      VIPRF      686
        4-17.75,-17.80,-14.00,-12.70,-11.50,-10.50/      VIPRF      687
        DATA N2F111/41/,DX2111/1.7621/      VIPRF      688
        DATA D52111/41*0./      VIPRF      689
        VIPRF      690
690      DATA N1A70/41/,DX1A70/1.104/      VIPRF      691
        DATA D51A70/ 0.0, -1.80, -1.60, -2.20, -3.00, -3.90, -4.90, -5.80,      VIPRF      692
        1 -7.00, -8.60,-10.60,-12.90,-16.60,-25.20,-25.80,-20.20,-16.40,      VIPRF      693
        2-14.10,-17.00,-12.40,-12.10,-11.80,-11.60,-11.65,-11.90,-12.50,      VIPRF      694
        3-17.75,-17.80,-19.90,-25.20,-26.00,-25.80,-27.00,-15.80,-13.40,      VIPRF      695
        4-11.00, -9.50, -8.75, -7.70, -6.90, -6.00/      VIPRF      696
        VIPRF      697
        DATA N2A70/41/,DX2A70/1.104/      VIPRF      698
        DATA D52A70/ 0.0, -1.60, -3.70, -6.40, -9.50,-13.00,-21.70,-21.70,      VIPRF      699
        1-16.00,-11.15,-10.00, -9.50, -9.72,-10.20,-11.20,-12.50,-14.60,      VIPRF      700
        2-17.70,-22.00,-25.90,-25.70,-22.00,-18.10,-16.10,-14.30,-13.75,      VIPRF      701
        3-17.40,-13.60,-13.98,-14.25,-15.60,-19.70,-26.10,-20.00,-13.00,      VIPRF      702
        4-10.30, -7.80, -5.00, -3.30, -1.80, -1.66/      VIPRF      703
        VIPRF      704
        DATA N1A10/41/,DX1A10/1.315/      VIPRF      705
        DATA D51A10/ 0.0, -1.00, -2.38, -4.01, -5.68, -7.54,-10.12,-13.40,      VIPRF      706
        1-19.00,-25.50,-25.50,-19.17,-15.29,-13.15,-11.70,-10.63, -9.68,      VIPRF      707
        2 -9.00, -8.71, -8.40, -8.27, -8.04, -8.11, -8.74, -9.66, -9.32,      VIPRF      708
        3-10.43,-11.57,-14.00,-18.27,-25.80,-20.90,-17.68, -9.24, -6.02,      VIPRF      709
        4 -3.68, -1.87, -1.32, .95, 2.26, 3.15/      VIPRF      710
        DATA N2A10/41/,DX2A10/1.315/      VIPRF      711
        DATA D52A10/41*0./      VIPRF      712
        VIPRF      713
        VIPRF      714
        VIPRF      715
        NRSVAL=43      VIPRF      716
        FMINPF=100.0 FMAXPF=10000.0      VIPRF      717
        FMINHF=10. FMAXHF=10000.      VIPRF      718
        FMINCF=5.0 FMAXCF=10000.      VIPRF      719
        HMAX=50000.0 FRSMAX=30.0 FHEMAX=5000.0      VIPRF      720
        YPF=0.10 PILOT=0      VIPRF      721
        DRLFLC=0.3 DRLEFHI=0.5 $XXLFLO=2.0 $XXLFHI=0.5      VIPRF      722
        FMELO=40.0 FMEFHI=250.0 RMEFLO=0.3 RMEFHI=0.3      VIPRF      723
        XMELO=2.5 XMEFHI=0.4      VIPRF      724
        RHELO=0.3 RHEFHI=0.3 $XXHFLC=2.0 $XXHFHI=0.5      VIPRF      725
        AHFLO=0.8 AHFHI=1.30 $APFHI=1.0 $ALFLO=1.0 $ALFHI=1.0      VIPRF      726
        AMELO=1.0 AMEFHI=1.0      VIPRF      727
        PL2FLC=0.2 PL2FHI=0.2 $XL2FLO=1.80 $XL2FHI=0.555      VIPRF      728
        AL2FLC=1.0 AL2FHI=2.0      VIPRF      729
        AMEMAX=-144.0 $AHFMAX=-121.0      VIPRF      730
        C1AXLC=2.0 C1AXHI=0.5 C1ABLO=0.2 C1ABHI=0.2 C1AALO=1.0      VIPRF      731
        C1AAHI=1.0 C1AFN=25.0 C1AMAX=12.0      VIPRF      732
        C2AXLC=1.5 C2AXHI=0.5 C2ABLO=0.2 C2ABHI=0.2 C2AALO=1.0      VIPRF      733
        C2AAHI=1.7 C2AFN=43.0 C2AMAX=13.0      VIPRF      734
        C2BXL=2.0 C2BXHI=0.5 C2BBL=0.200 C2BEHI=0.300 C2BALC=1.0      VIPRF      735
        C2BAHI=1.5 C2BFN=40.0 C2BMAX=14.0      VIPRF      736
        C5BLO=0.1 C5BFHI=0.1 C5BXLO=1.42 C5BXHI=1.1/1.42 C5BALC=0.50      VIPRF      737
        C5BAHI=1.4 C5BFN=200.0 C5BMAX=37.0      VIPRF      738
        CUFYLC=1.23 CUFYHI=0.93 $BUFFHI=0.200 $BUFFZL=24.0 $BUFFZH=60.0      VIPRF      739
        DUFALC=0. $BUFAHI=1.0 $BUFDEL=5.0      VIPRF      740
        TAKDLC=0.3 TAKBHI=0.4 TAKXLO=4.0 TAKXHI=0.50 TAKALC=0.4      VIPRF      741
        TAKAHI=1.0 TAKMAX=10.0      VIPRF      742

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PROGRAM	VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
		ALNPLC=0.3 \$ALNBHI=0.3 \$ALNXLO=2.0 \$ALNXHI=0.5 \$ALNALC=0.4			VIPRF	743
		ALNAHT=1.0 \$ALNMAX=12.0			VIPRF	744
		TRPHI=0.3 \$TRAHI=1.0 \$TBFO=5.0 \$TBREF=12.0			VIPRF	745
745		MO3=10			VIPRF	746
		\$C3APHI=0.2 \$C3AXLO=2.0 \$C3AALO=2.0 \$C3AFN=25.0 \$C3RFN=35.0			VIPRF	747
					VIPRF	748
					VIPRF	749
		CALL COMPRS \$CALL YAXANG(0.) \$CALL YINTAX			VIPRF	750
750		CALL BASALF("L/GSTO") \$CALL MIXALF("STANDARD") \$CALL MARKER(1)			VIPRF	751
		HITE=0.140 \$HITE1=5.*HITE/7.			VIPRF	752
		XCYCLEF=2.0 \$YAXIS=8.0 \$TICLFN=0.026			VIPRF	753
					VIPRF	754
					VIPRF	755
755	C	*****			VIPRF	756
	C	* * *			VIPRF	757
	C	* READ INPUT DATA *			VIPRF	758
	C	* * *			VIPRF	759
	C	*****			VIPRF	760
760					VIPRF	761
		1 READ(F,15) (IPLANE(I),I=1,3),JFLITE,INOPLT			VIPRF	762
		IF(FCF(F).NE.0) GO TO 89J			VIPRF	763
		15 FORMAT(8A10)			VIPRF	764
					VIPRF	765
765		31 I=10H*****0 \$PRINT 2F,I,J,I,I,I,I,I			VIPRF	766
		25 FORMAT(1H1,19X,*INPUT DATA CARDS*//63X,*COLUMN NUMBER*//			VIPRF	767
		13BX,*1*,9X,*2*,3X,*3*,9X,*4*,9X,*5*,9X,*6*,9X,*7*,9X,*8*//			VIPRF	768
		22CX,1CH1*****0,7A10//)			VIPRF	769
		PRINT 37, (IPLANE(I),I=1,3),JFLITE,INOPLT			VIPRF	770
770		37 FORMAT(1H0,28X,*DESCRIPTION CARD*/29X,8A10)			VIPRF	771
					VIPRF	772
		READ 15,ILINE2			VIPRF	773
		PRINT 36,ILINE2			VIPRF	774
		36 FORMAT(1H0,28X,*ALTITUDE-MACH NO. CARD*/29X,8A10)			VIPRF	775
775		RECDEF(8C,37,ILINE2) (ALT(I),AMAKNO(I),I=1,6)			VIPRF	776
		37 FORMAT(6(F9.2,F5.2))			VIPRF	777
					VIPRF	778
		READ 15,ILINE2			VIPRF	779
		PRINT 38,ILINE2			VIPRF	780
780		38 FORMAT(1H0,28X,*AIRCRAFT PARAMETERS CARD*/29X,8A10)			VIPRF	781
		RECDEF(8C,38,ILINE2) XE,PS,WE,DF,T,FCCAT1,FCCAT2,MATERL,CATGRY			VIPRF	782
		39 FORMAT(7F11.3,A1,A2)			VIPRF	783
					VIPRF	784
					VIPRF	785
785		I=IPLANE(1)			VIPRF	786
		IF(I.EQ.1F4) GO TO 20			VIPRF	787
		IF(I.EQ.1F15) GO TO 26			VIPRF	788
		IF(I.EQ.1F16) GO TO 40			VIPRF	789
		IF(I.EQ.1F111) GO TO 47			VIPRF	790
790		IF(I.EQ.1A70) GO TO 45			VIPRF	791
		IF(I.EQ.1A10) GO TO 48			VIPRF	792
					VIPRF	793
		CALL READCDS(0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,I,IFRROR)			VIPRF	794
		GO TO 47			VIPRF	795
795					VIPRF	796
		20 CALL READCDS(14.3,-122.0,18.94,-129.0,35.0,32.3,35.3,1.0,			VIPRF	797
		1M1F4,1X1F4,1B1F4,1N2F4,1X2F4,1D32F4,1,1F4,1ERROR)			VIPRF	798
		GO TO 47			VIPRF	799



PROGRAM	VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
	25	CALL READDCDS(8.5,-127.0,27.8,-131.0,35.0,39.1,40.2,1.0,			VIPRF	800
		2N1F15,CX1F15,DB1F15,N2F15,DX2F15,DB2F15,1,IF15,IEPROR)			VIPRF	801
		GO TO 47			VIPRF	802
	40	CALL READDCDS(12.9,-131.0,32.5,-133.0,35.0,27.1,29.5,1.0,			VIPRF	803
		2N1F16,CX1F16,DB1F16,N2F16,DX2F16,DB2F16,1,IF16,IEPROR)			VIPRF	804
		GO TO 47			VIPRF	805
	47	CALL READDCDS(8.5,-134.0,0.00,0.0,35.0,38.1,47.1,1.0,			VIPRF	806
		1N1F111,DX1111,DB1111,N2F111,DX2111,DB2111,1,IF111,IEPROR)			VIPRF	807
		GO TO 47			VIPRF	808
	46	CALL READDCDS(15.2,-129.0,23.0,-140.0,35.0,20.5,25.4,1.0,			VIPRF	809
		2N1A7D,CX1A7D,DB1A7D,N2A7D,DX2A7D,DB2A7D,1,IA7D,IEPROR)			VIPRF	810
		GO TO 47			VIPRF	811
	48	CALL READDCDS(9.04,-131.0,0.0,0.0,35.0,0.00,4.0,1.0,			VIPRF	812
		1N1A10,CX1A10,DB1A10,N2A10,DX2A10,DB2A10,1,IA10,IEPROR)			VIPRF	813
					VIPRF	814
					VIPRF	815
	47	IF(IEPROR.EQ.0) GO TO 27			VIPRF	816
		IF(IEPROR.EQ.1) GO TO 1			VIPRF	817
		IF(IEPROR.EQ.2) GO TO 4			VIPRF	818
		IF(IEPROR.EQ.3.OR.IEPROR.EQ.4) GO TO 41			VIPRF	819
					VIPRF	820
	41	IPLANE(1)=ILINE2(1) *IPLANE(2)=ILINE2(2)			VIPRF	821
		IPLANE(3)=ILINE2(3) *JFLITE=ILINE2(4)			VIPRF	822
		INOPLT=ILTAE2(5)			VIPRF	823
		GO TO 31			VIPRF	824
					VIPRF	825
	41	GO 42 I=1,5			VIPRF	826
	42	IHOLD(I)=ILINE2(I)			VIPRF	827
					VIPRF	828
					VIPRF	829
					VIPRF	830
					VIPRF	831
					VIPRF	832
					VIPRF	833
					VIPRF	834
					VIPRF	835
	27	M=0			VIPRF	836
		IF(JFLITE.EQ.ISANDL.OR.JFLITE.EQ.IRUFET.OR.JFLITE.EQ.ITAKOF			VIPRF	837
		1.OR.JFLITE.EQ.ILAND.OR.JFLITE.EQ.ITURD) GO TO 9			VIPRF	838
		M=1 *PRINT 29,JFLITE,ISANDL,IRUFET,ITAKOF,ILAND,ITURD			VIPRF	839
	22	FORMAT(1H-, A10,* WAS READ FOR THE FLIGHT CONDITION,NOT*,A10,*OR*,			VIPRF	840
		1A10,*CR*,A10,*OR*,A10,*OR*,A10/* FOR "STRAIGHT-AND-LEVEL","BLUFFET-			VIPRF	841
		2TURN","TAKE-OFF","LANDING" AND "LOW-FREQ. ATMOSPHERIC TURELLENCE",			VIPRF	842
		3RESPERTIVELY,*)			VIPRF	843
					VIPRF	844
	9	IF(XE.GT.0.) GO TO 10			VIPRF	845
		M=1 *II=10HDOWN-STREA *I=10H4 AFRO.DST *PRINT 5,II,J,XF			VIPRF	846
		II=3H>0. *PRINT 8,II,IPLANK			VIPRF	847
					VIPRF	848
	10	IF(RS.GE.0.) GO TO 14			VIPRF	849
		M=1 *II=10H DISTANCE *J=9HFROM SKIN *PRINT 5,II,J,RS			VIPRF	850
		II=10H>0. CR =0. *PRINT 8,II,IPLANK			VIPRF	851
					VIPRF	852
	14	IF(WE.GE.0.) GO TO 11			VIPRF	853
		M=1 *II=10H EQUIPMEN *J=8HT WEIGHT *PRINT 5,II,J,WE			VIPRF	854
		II=10H>0. CR =0. *PRINT 8,II,IPLANK			VIPRF	855
					VIPRF	856
	11	IF(DF.GT.0.) GO TO 18				

PROGRAM VIPRF	74/74	OPT=1	FTN 4,5+414	08/16/77	13.11.28
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	M=1 \$II=10H FUSELAGE \$J=8HDIAMETER \$PRINT 5,II,J,DF	VIPRF	857
	II=3H>0. \$PRINT 8,II,IBLANK	VIPRF	858
	GO TO 19	VIPRF	859
860	13 Y1=DF/2. \$IF(PS,LF,X1) GO TO 19	VIPRF	860
	M=1 \$PRINT 16,PS,Y1	VIPRF	861
	14 FORMAT(1H-,*THE SPECIFIED DISTANCE FROM THE SKIN *,F7.2,* EXCEEDS	VIPRF	862
	1ONE-HALF THE FUSELAGE DIAMETER *,F7.2)	VIPRF	863
	II=10H FUSELAGE D \$J=6HIA/2. \$PRINT 8,II,J	VIPRF	864
865		VIPRF	865
	12 IF(T,CT,C.) GO TO 23	VIPRF	866
	M=1 \$II=10H SKIN TH \$J=7HICKNESS \$PRINT 5,II,J,T	VIPRF	867
	II=3H>0. \$PRINT 8,II,IBLANK	VIPRF	868
		VIPRF	869
870	27 IF(CATGRY,90,C19) GO TO 76	VIPRF	870
	IF(FCCAT1,95,C.) GO TO 74	VIPRF	871
	M=1 \$II=10H CATEGORY C \$J=10HENTER FRO. \$PRINT 5,II,J,FCCAT1	VIPRF	872
	II=10H>0. OR =0. \$PRINT 8,II,IBLANK	VIPRF	873
		VIPRF	874
		VIPRF	875
875	74 IF(FCCAT2,95,C.) GO TO 76	VIPRF	876
	M=1 \$II=10H CATEGORY 3 \$J=10HA OR 3P FC \$PRINT 5,II,J,FCCAT2	VIPRF	877
	II=10H>0. OR =0. \$PRINT 8,II,IBLANK	VIPRF	878
		VIPRF	879
880	75 IF(MATERL,90,ISTEEL,9P,MATERL,90,ITITAN,9P,MATERL,90,IALUM	VIPRF	880
	1,9P,MATERL,90,IMAG) GO TO 50	VIPRF	881
	M=1 \$PRINT 24,MATERL	VIPRF	882
	24 FORMAT(1H-,*THE LETTER SPECIFIED FOR THE AIRCRAFT MATERIAL WAS *,	VIPRF	883
	1A1/* IT MUST BE S,T,A OR M FOR STEEL,TITANIUM,ALUMINUM AND MAGNESI	VIPRF	884
	2UM,RESPECTIVELY.*)	VIPRF	885
885		VIPRF	886
	50 IF(CATGRY,90,C1A,9P,CATGRY,90,C1B,9P,CATGRY,90,C2A,9P,CATGRY,90,	VIPRF	887
	1C2P,9P,CATGRY,90,C3A,9P,CATGRY,90,C3P,9P,CATGRY,90,C4A,9P,	VIPRF	888
	2CATGRY,90,C4B,9P,CATGRY,90,C5,9P,CATGRY,90,C6) GO TO 54	VIPRF	889
	M=1 \$PRINT 52,CATGRY,C1A,C1B,C2A,C2B,C3A,C3B,C4A,C4B,C5,C6	VIPRF	890
890	52 FORMAT(1H-,A3,* WAS SPECIFIED FOR THE EQUIPMENT-MOUNTING CATEGORY.	VIPRF	891
	1/* THE PROGRAM EXPECTS SPECIFICATIONS FOR CATEGORIES ONLY AS FOLL	VIPRF	892
	2OWS:\$1J(1Y,A3)/* THE PROGRAM PROCEEDS TO THE NEXT PROBLEM FOR ANAL	VIPRF	893
	YSIS.*/	VIPRF	894
	54 IF(FN,CT,C.) GO TO 60	VIPRF	895
895	M=1 \$II=10H1ST MODE F \$J=8HREQUENCY \$PRINT 5,II,J,FN	VIPRF	896
	II=3H>0. \$PRINT 8,II,IBLANK	VIPRF	897
		VIPRF	898
	60 IF(XLFMAX,LT,C.) GO TO 56	VIPRF	899
	M=1 \$II=10H MAX.VALUE \$J=8H OF L(F) \$PRINT 5,II,J,XLFMAX	VIPRF	900
900	II=3H>0. \$PRINT 8,II,IBLANK	VIPRF	901
		VIPRF	902
	56 IF(F2N,95,C.) GO TO 64	VIPRF	903
	M=1 \$II=10H2ND MODE F \$J=8HREQUENCY \$PRINT 5,II,J,F2N	VIPRF	904
	II=10H>0. OR =0. \$PRINT 8,II,IBLANK	VIPRF	905
905		VIPRF	906
	64 IF(XL2FMX,LF,C.) GO TO 58	VIPRF	907
	M=1 \$II=10H MAX.VALUE \$J=8H OF L2(F) \$PRINT 5,II,J,XL2FMX	VIPRF	908
	II=10H>0. OR =0. \$PRINT 8,II,IBLANK	VIPRF	909
		VIPRF	910
910	58 IF(BUFMAX,95,C.) GO TO 62	VIPRF	911
	M=1 \$II=10HMAX,OF BUF \$J=10H.TURN S(F) \$PRINT 5,II,J,BUFMAX	VIPRF	912
	II=10H>0. OR =0. \$PRINT 8,II,IBLANK	VIPRF	913

PROGRAM	VIERF	74/74	OPT=1	FTN 4,5+414	08/16/77	13.11.28
					VIPRF	914
					VIPRF	915
915	57	IF(XST.GE.0.) GO TO 66			VIPRF	916
		M=1	II=10HUFFET-TUR	IJ=10HM DISTANCE	SPRINT 5,II,J,XPT	
		II=10H>0. OR =0.	SPRINT 8,II,IPLANK		VIPRF	917
					VIPRF	918
					VIPRF	919
920	69	IF(XTL.GE.0.) GO TO 69			VIPRF	920
		M=1	II=10HTAKEOFF-LA	II=10HNDING DIST	SPRINT 5,II,J,XTL	
		II=10H>0. OR =0.	SPRINT 8,II,IPLANK		VIPRF	921
					VIPRF	922
					VIPRF	923
					VIPRF	924
925	68	IF(FCMOVE.GE.0.) GO TO 70			VIPRF	925
		M=1	II=10HMULT.CONST	II=FMHANT K	SPRINT 5,II,J,FCMOVE	
		II=3H>0.	SPRINT 8,II,IPLANK		VIPRF	926
					VIPRF	927
					VIPRF	928
					VIPRF	929
					VIPRF	930
930	70	IF(NMOCF1.GT.0.) GO TO 21			VIPRF	931
		M=1	II=10HNO.FR VAL.	II=10H1ST B.MODE	II=X1=NMODEF1	SPRINT 5,II,J,X1
		II=3H>0.	SPRINT 8,II,IPLANK		VIPRF	932
					VIPRF	933
					VIPRF	934
					VIPRF	935
935	71	IF(F2N.FG.0.) GO TO 35			VIPRF	936
		IF(NMOCF2.GT.0.) GO TO 72			VIPRF	937
		M=1	II=10HNO.FR VAL.	II=10H2ND B.MODE	II=X1=NMODE2	SPRINT 5,II,J,X1
		II=3H>0.	SPRINT 8,II,IPLANK		VIPRF	938
					VIPRF	939
					VIPRF	940
940	72	IF(DXMCD2.GT.0.) GO TO 35			VIPRF	941
		M=1	II=10HVE DIST.3E	II=10H1.DB VALS.	SPRINT 5,II,J,DXMCD2	
		II=3H>0.	SPRINT 8,II,IPLANK		VIPRF	942
					VIPRF	943
					VIPRF	944
945	35	DO 1000 I=1,6			VIPRF	945
		IF(AMAKNO(I).EQ.0.) GO TO 1000			VIPRF	946
					VIPRF	947
					VIPRF	948
					VIPRF	949
					VIPRF	950
950		H=ALT(I)	IF(H.GE.0..AND.H.LE.HMAX)	GO TO 28		
		M=1	II=10H	ALT II	II=4HTUDE	SPRINT 5,II,J,H
		II=9H	> OR = II=9H	< OR =	II=X1=0.	SPRINT 6,II,J,HMAX
		6	FORMAT(* THE PROGRAM ASSUMES THAT IT WILL BE	*A10,G12.5,* AND *		
		1A10,F11.2)				
		GO TO 7				
					VIPRF	955
955	28	XMAKNO=AMAKNO(I)			VIPRF	956
		IF(JELITE.NE.ITAKOF.AND.JELITE.NE.ILAND)	GO TO 7		VIPRF	957
		IF(XMAKNO.EQ.0.93.AND.H.EQ.2000.0)	GO TO 79		VIPRF	958
		PRINT 2,H,XMAKNO			VIPRF	959
		7	FORMAT(/////////1H1/*THE FOLLOWING VALUES,READ FOR ALTITUDE(H) AND		VIPRF	960
960		1	MACH NUMBER(M),WERE INCORRECTLY SPECIFIED ON THE ALTITUDE-MACH NO		VIPRF	961
		2.	CARD:*/35X,*H=*,F10.1/35X,*M=*,F10.3/** THEY WERE SET EQUAL TO TH		VIPRF	962
		35	CORRECT VALUES,H=2000.0 AND M=0.93, WHICH ALWAYS MUST BE SPECIFI		VIPRF	963
		450/** WHEN THE FLIGHT PHASE IS TAKE-OFF AND LANDING.*)			VIPRF	964
		XMAKNO=0.93	II=2000.0	GO TO 76		
					VIPRF	965
					VIPRF	966
966	7	IF(XMAKNO.GT.0.) GO TO 78			VIPRF	967
		M=1	II=10H	MACH II=4H NO.	SPRINT 5,II,J,XMAKNO	
		6	FORMAT(1H=,*THE VALUE SPECIFIED FOR *	2A10,* IS *	G12.5)	
		II=3H>0.	SPRINT 8,II,IPLANK		VIPRF	969
					VIPRF	970

PROGRAM	VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
970	* FORMAT(* THE PROGRAM ASSUMES THAT IT WILL BE *,2A10)				VIPRF	971
					VIPRF	972
					VIPRF	973
	7* IF(M.EC.1) GO TO 1000				VIPRF	974
975	IF(FCMOVE.EC.0.) FCMOVE=1.0				VIPRF	975
	ICK=0 \$IFLITE=ISANDL				VIPRF	976
					VIPRF	977
					VIPRF	978
980	3 DO 17 II=1,7				VIPRF	979
	ILINE1(II)=1H \$ILINE2(II)=1H				VIPRF	980
	17 ITITL1(II)=1H				VIPRF	981
					VIPRF	982
	ILINE1(1)=10H TO EQUIPM \$ILINE1(2)=10HENT LOCATI \$ILINE1(3)=2HON				VIPRF	983
985	X=XE \$IX=1HE \$IPHASE=5H (F)\$ \$IF(IFLITE.EC.ISANDL) GO TO 34				VIPRF	984
	IF(IFLITE.NE.IPUFET) GO TO 12				VIPRF	985
	ILINE1(1)=10H TO THE CH \$ILINE1(2)=1CHORD CENTER				VIPRF	986
	ILINE1(3)=10H OF THE WI \$ILINE1(4)=2HNG				VIPRF	987
	Y=XPT \$IX=2HBT \$IPHASE=6H (PT)\$ \$GO TO 34				VIPRF	988
990	12 IF(IFLITE.NE.ITAXOF) GO TO 13				VIPRF	989
	ILINE1(1)=10H TO THE LA \$ILINE1(2)=10HNDING GEAR				VIPRF	990
	X=XTL \$IX=1HT \$IPHASE=5H (T)\$ \$IFN=1HN \$GO TO 34				VIPRF	991
					VIPRF	992
	13 IF(IFLITE.NE.ILAND) GO TO 22				VIPRF	993
995	X=XTL \$IX=1HL \$IPHASE=5H (L)\$ \$IFN=2H2N \$GO TO 34				VIPRF	994
					VIPRF	995
	22 X=XF \$IX=2HTF \$IPHASE=6H (TR)\$ \$IFN=1HN				VIPRF	996
					VIPRF	997
	74 II=H/500.*+1 \$X1=EC0.				VIPRF	998
1000	IF(H.LE.10000.) GO TO 44				VIPRF	999
	II=H/1000.*+11 \$X1=1000.				VIPRF	1000
	44 V=VISCOS(II) \$C=SCUND(II) \$R=AVDENS(II)				VIPRF	1001
	Y2=AMCO(H,X1) \$IF(X2.EC.0.) GO TO 45				VIPRF	1002
	II=II+1 \$X3=X2/Y1				VIPRF	1003
1005	R=R+(AVDENS(II)-R)*X3				VIPRF	1004
	C=C+(SCUND(II)-C)*X3				VIPRF	1005
	V=V+(VISCOS(II)-V)*X3				VIPRF	1006
					VIPRF	1007
	45 RNORM=R/AVDENS(1) \$VNORM=V/VISCOS(1) \$U=XMAKN0*C \$NSQ=P*U*U/2.				VIPRF	1008
1010	CSQ=CSC*CSQ \$REY=U*XF/VISCOS(1)				VIPRF	1009
	DELTA7=6.6E7/PEX \$DELTA7=1.0E-2*XE*(1.0+DELTA7*DELTA7)**0.10				VIPRF	1010
	DELTA8=DELTA7*(RNORM**0.7)				VIPRF	1011
					VIPRF	1012
	FZPF=C.700*L/DELTA8				VIPRF	1013
1015					VIPRF	1014
	PPF=1.745 \$IF(FZPF.LE.300.0) GO TO 90				VIPRF	1015
	GPS=C.375 \$IF(FZPF.GE.19900.0) GO TO 90				VIPRF	1016
	CALL TERPLIN(FZPF,700.0,300.0,X1,0,PPF,BFZFF,NBFZPF)				VIPRF	1017
1020					VIPRF	1018
	90 X1=.007/(1.0+C.14*XMAKN0*XMAKN0) \$PFM=X1*X1*CSQ*DELTA8/U				VIPRF	1019
	PFMDR=C.41771E-5 \$PFMDR=10.0*ALOG10(PFM/(PFMDR*PFMDR))				VIPRF	1020
					VIPRF	1021
					VIPRF	1022
					VIPRF	1023
					VIPRF	1024
1025	IF(MATERL.NE.ALUM) GO TO 92				VIPRF	1025
	WS=14.5*T \$J=10H ALUMINIUM				VIPRF	1026
					VIPRF	1027



PROGRAM	VIPRF	74/74	CPT=1	FTN 4.5+414	08/16/77	13.11.28
		GO TO 100			VIPRF	1028
		97 IF(MATERL.NE.ITITAN) GO TO 94			VIPRF	1029
		WS=24.0*T :J=10H TITANIUM			VIPRF	1030
1030		GO TO 100			VIPRF	1031
		98 IF(MATERL.NE.ISTEEL) GO TO 96			VIPRF	1032
		WS=41.0*T :J=10H STEEL			VIPRF	1033
		GO TO 100			VIPRF	1034
1035		99 WS=9.17*T :J=10H MAGNESIUM			VIPRF	1035
					VIPRF	1036
					VIPRF	1037
		100 PRINT 246			VIPRF	1038
		PRINT 353,IPLANE,IFLITE			VIPRF	1039
		PRINT 205,H,XMAKNO,X,IX,(ILINE1(II),II=1,5)			VIPRF	1040
1040		II=1H :IF(CATGRY.EQ.C1A) II=14*			VIPRF	1041
		PRINT 210,RS,WE,T,J,WS,CATGRY,DF			VIPRF	1042
		PRINT 220			VIPRF	1043
		PRINT 225,R,AVDENS(1),PNORM,V,VISCOS(1),VNCRM,C			VIPRF	1044
		PRINT 230			VIPRF	1045
1045		PRINT 235,U,OSQ,PEY,DELTAZ,DELTAB			VIPRF	1046
		205 FORMAT(1H-,10X,*H=F12.1,6X,*ALTITUDE(FT.)*//			VIPRF	1047
		*20X,*V=F12.2,6X,*MACH NO.*//			VIPRF	1048
		219X,*Y=F12.2,6X,A2,*DISTANCE FROM THE LEADING EDGE OF THE *//			VIPRF	1049
		320X,A2,18X,*FUSELAGE AERODYNAMIC PROFILE(FT.)*,5A10)			VIPRF	1050
1050		210 FORMAT(10X,*F=F12.2,6X,*DISTANCE FROM SKIN(IN.)*//20X,*S*//			VIPRF	1051
		110X,*W=F12.2,6X,*EQUIPMENT WEIGHT(LBS.)*//20X,*E*//			VIPRF	1052
		220X,*T=F12.4,6X,*THICKNESS OF SKIN MATERIAL(IN.)*//			VIPRF	1053
		313X,*MATERIAL=*3X,A10,5X,*TYPE SKIN MATERIAL*//			VIPRF	1054
1055		472X,*2*/10X,*W=F12.7,6X,*DENSITY OF SKIN MATERIAL,LBS./FT.(CALC			VIPRF	1055
		5ULATED)*//20X,*S*//			VIPRF	1056
		613X,*CATGCRY=*9X,A2,7X,*EQUIPMENT MOUNTING CATEGORY*//			VIPRF	1057
		719X,*D=F12.1,6X,*DIAMETER OF FUSELAGE(IN.)*//20X,*F*//)			VIPRF	1058
		220 FORMAT(*VALUES SELECTED FROM ATMOSPHERIC TABLE*)			VIPRF	1059
		225 FORMAT(			VIPRF	1060
1060		*10X,*P=F12.6,6X,*MEAN AIR DENSITY AT ALTITUDE H(SLUG/CU.FT.)*//			VIPRF	1061
		*10X,*P=F12.6,6X,*MEAN AIR DENSITY AT ZERO ALTITUDE(SLUG/CL.FT.)*//			VIPRF	1062
		*20X,*0*//			VIPRF	1063
		*17X,*F/R=F12.5,6X,*NORMALIZED MEAN AIR DENSITY*//20X,*0*//			VIPRF	1064
1065		*19X,*V=F12.7,6X,*KINEMATIC VISCOSITY AT ALTITUDE H(FT.SQ./SEC.)*//			VIPRF	1065
		*20X,*0*//			VIPRF	1066
		*19X,*V=F12.7,6X,*KINEMATIC VISCOSITY AT ZERO ALTITUDE(FT.SQ./SE			VIPRF	1067
		*C.)*//20X,*0*//			VIPRF	1068
		*17X,*V/V=F12.3,6X,*NORMALIZED KINEMATIC VISCOSITY*//20X,*0*//			VIPRF	1069
		*20X,*C=F12.2,6X,*SPEED OF SOUND AT ALTITUDE H(FT./SEC.)*//)			VIPRF	1070
1070		230 FORMAT(*VALUES CALCULATED FOR AERODYNAMIC PARAMETERS*)			VIPRF	1071
		235 FORMAT(			VIPRF	1072
		110X,*U=F12.2,6X,*FREE STREAM VELOCITY(FT.SEC.)*//			VIPRF	1073
		220X,*2*,35X,*2*/19X,*Q=F12.5,6X,*DYNAMIC PRESSURE(PSF)*//			VIPRF	1074
		*18X,*RE=F12.5,6X,*REYNOLDS NUMBER AT DISTANCE X*//20X,*X*//			VIPRF	1075
1075		*15X,*DELTA=F12.4,6X,*BOUNDARY LAYER THICKNESS AT ZERO ALTITUDE(			VIPRF	1076
		*FT.)*//20X,*0*//			VIPRF	1077
		*15X,*DELTA=F12.4,6X,*BOUNDARY LAYER THICKNESS AT ALTITUDE H(FT.			VIPRF	1078
		*7)*//20X,*0*//			VIPRF	1079
					VIPRF	1080
1080					VIPRF	1081
					VIPRF	1082
		PRINT 246 *PRINT 353,IPLANE,IFLITE			VIPRF	1083
		PRINT 240			VIPRF	1084



PROGRAM	VIPRF	74/74	OPT=1	ETN 4.5+414	08/16/77	13.11.28
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1085	240	FORMAT(1H=,*PARAMETERS OF THE BOUNDARY LAYER FUNCTION FOR F(F)*)	VIPRF	1085
		PRINT 24F,PFM,PFMDR,PRF,YPF,FZPF,APFHI	VIPRF	1086
	240	FORMAT(64X,*2*/16X,*P (F)=*,F12.4,6X,*MAXIMUM VALUE OF PSD,PSF /HZ	VIPRF	1087
		1.**/17X,*M*/	VIPRF	1088
		270X,*-0 2*,4X,*2*/16X,*P (F)=*,F12.2,6X,*MAXIMUM VALUE OF PSD,DR.	VIPRF	1089
		3RE.(0.41771Y10 ) PSF/47,**/17X,*M*/	VIPRF	1090
1090		410X,*F'=*,F12.3,6X,*SLOPE FACTOR,HIGH FREQ.ROLL-OFF*/	VIPRF	1091
		510X,*X'=*,F12.3,6X,*NORMALIZING FREQ.RATIO,HIGH-FREQ.ROLL-OFF*/	VIPRF	1092
		610X,*F'=*,F12.1,6X,*LOCATOR FREQUENCY,HIGH FREQ.ROLL-OFF(HZ.)*//	VIPRF	1093
		720X,*C*/	VIPRF	1094
		810X,*ALPHA'=*,F12.3,6X,*FORM FACTOR,HIGH FREQ.ROLL-OFF*)	VIPRF	1095
1095			VIPRF	1096
		TITLE1(1)=1CH(S AND L F SITITLE1(2)=7HLIGHT)*	VIPRF	1097
		XMFMAX=AHFMAX SXHFMAX=AHFMAX	VIPRF	1098
			VIPRF	1099
			VIPRF	1100
1100		IF(IFLITE.EQ.ISANDL) GO TO 280	VIPRF	1101
		IF(IFLITE.NE.IPUFFT) GO TO 250	VIPRF	1102
			VIPRF	1103
			VIPRF	1104
		*****	VIPRF	1105
1105		* * *	VIPRF	1106
		* PUFFET-TURN PHASE *	VIPRF	1107
		* * *	VIPRF	1108
		*****	VIPRF	1109
		ILINE1(1)=1CHCENTER FREQ ILINE1(2)=1CHQUENCY OF	VIPRF	1110
1110		ILINE1(3)=1CHSPECIAL TR ILINE1(4)=1CHANSFER FUN	VIPRF	1111
		ILINE1(5)=3SHOTION	VIPRF	1112
		ITITLE1(1)=1CH(PUFFET TU SITITLE1(2)=1CHRN PHASE)*	VIPRF	1113
			VIPRF	1114
		SXLO=PUFXLO SXHI=PUFXHI \$SAHI=PUFPHI \$M=3HOUT	VIPRF	1115
1115		SALO=PUFALO \$SAHI=PUFAHI \$DELTA=PUFCFL \$SF7LC=PUF7L	VIPRF	1116
			VIPRF	1117
		C=3DS(X-XF)	VIPRF	1118
		SBTFD=CBVAL(NDDR) IF(D.GE.(NDDR-1)) GO TO 239	VIPRF	1119
1120			VIPRF	1120
		CALL TERPLIN(C,DELDOR,0.,Y1,2,SBTFD,CBVAL,NDDR)	VIPRF	1121
			VIPRF	1122
	232	SBTFD=PUFMAX+SBTFD IF(SBTFD.EQ.SDELTA) SBTFD=1.01*SDELTA	VIPRF	1123
		IF(SBTFD.GT.SDELTA) GO TO 247	VIPRF	1124
			VIPRF	1125
1125		HILO(1)=PI \$SIGN(1)=-1.0 \$SXHI=0.167 \$SAHI=2.0 \$SF7HI=30.0	VIPRF	1126
		\$SPEAK=SDELTA	VIPRF	1127
		FCS=FCMCVE*\$SXHI*\$SF7HI \$SF7HI=FCS/\$SXHI \$FRQ=SXLO*\$SF7LO	VIPRF	1128
		CALL DATA(\$FHI,SDELTA,SBTFD,SXHI,SAHI,FRQ,SF7HI,SIGN(1),HILO(1))	VIPRF	1129
		GO TO 253	VIPRF	1130
1130			VIPRF	1131
	247	HILO(1)=0. \$SIGN(1)=1.0 \$FCS=SXLO*\$SF7LO \$SPEAK=SBTFD	VIPRF	1132
		\$SF7HI=FCMCVE*\$FCS/\$SXHI \$FRQ=FMINGF	VIPRF	1133
		CALL DATA(\$FLO,SBTFD,SDELTA,SXLO,SALO,FRQ,SF7LO,SIGN(1),HILO(1))	VIPRF	1134
		GO TO 253	VIPRF	1135
1135			VIPRF	1136
			VIPRF	1137
		*****	VIPRF	1138
		* * *	VIPRF	1139
		* TAKE-OFF PHASE *	VIPRF	1140
1140		* * *	VIPRF	1141

PROGRAM	VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
					VIPRF	1142
					VIPRF	1143
					VIPRF	1144
1145					VIPRF	1145
					VIPRF	1146
					VIPRF	1147
					VIPRF	1148
					VIPRF	1149
1150					VIPRF	1150
					VIPRF	1151
					VIPRF	1152
					VIPRF	1153
					VIPRF	1154
1155					VIPRF	1155
					VIPRF	1156
					VIPRF	1157
					VIPRF	1158
					VIPRF	1159
1160					VIPRF	1160
					VIPRF	1161
					VIPRF	1162
					VIPRF	1163
					VIPRF	1164
1165					VIPRF	1165
					VIPRF	1166
					VIPRF	1167
					VIPRF	1168
					VIPRF	1169
1170					VIPRF	1170
					VIPRF	1171
					VIPRF	1172
					VIPRF	1173
					VIPRF	1174
1175					VIPRF	1175
					VIPRF	1176
					VIPRF	1177
					VIPRF	1178
					VIPRF	1179
1180					VIPRF	1180
					VIPRF	1181
					VIPRF	1182
					VIPRF	1183
					VIPRF	1184
1185					VIPRF	1185
					VIPRF	1186
					VIPRF	1187
					VIPRF	1188
					VIPRF	1189
1190					VIPRF	1190
					VIPRF	1191
					VIPRF	1192
					VIPRF	1193
					VIPRF	1194
					VIPRF	1195
1195					VIPRF	1196
					VIPRF	1197
					VIPRF	1198

	PROGRAM VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
	II=5HS (F) \$J=1HM \$PRINT 352,II,SPEAK,II,IPLANE(1),IX,J,IX				VIPRF	1199
1200	757 FORMAT(17X,A5,*=*,F12.2,6X,*MAXIMUM VALUE OF *,A5,*-DP.,FOR*,				VIPRF	1200
	1A10,*TYPE AIPCRAFT*/18X,A2,1X,A1,37X,A2)				VIPRF	1201
	IF (IFLITE,SC,IBUFET,AND,SPTEF,LT,SDELTA) GO TO 257				VIPRF	1202
	PRINT 380,SPLO,SBHI, SXLO, SXHI, SF7LO, SF7HI				VIPRF	1203
1205	PRINT 441,FCS, (ILINE1(J),J=1,7),M				VIPRF	1204
	PRINT 425,SALC,SAHI				VIPRF	1205
	IF (IFLITE,SC,IBUFET) PRINT 254,SDELTA,FMINGF,BUFMAX,D,XF				VIPRF	1206
	254 FORMAT(14-,15X,*DELTA =*,F12.2,6X,*VALUE OF S (F) AT*,				VIPRF	1207
	1F6.1,* HZ,*/21X,*C*,29X,*RT*/				VIPRF	1208
1210	267X,*2*,12X,*-4*,9X,*2 2*/16X,*S (F)*=*,F12.1,6X,*MAXIMUM VALUE OF				VIPRF	1209
	3 S (F) (WHEN C=0.)-DP.,RE 1.0 G /HZ./RE.(2X10 DYNES-CM.) /HZ.*/				VIPRF	1210
	417X,*RT M*,38X,*RT M*/				VIPRF	1211
	521X,*C*=*,F12.2,6X,*DIFFERENCE,X -X*/53X,*PT E**				VIPRF	1212
	620X,*X =*,F12.2,6X,*F DISTANCE FROM THE LEADING EDGE OF THE FUSELA				VIPRF	1213
1215	7GE*/21X,*F*,19X,*AERODYNAMIC PROFILE (FT.) TO THE CENTER OF THE WIN				VIPRF	1214
	8G CHORE*)				VIPRF	1215
	GO TO 280				VIPRF	1216
	257 PRINT 255,SBHI, SXHI, SF7HI, SAHI, FCS				VIPRF	1217
1220	255 FORMAT(20X,*B*=*,F12.2,6X,*SLOPE FACTOR,HIGH-FREQ.ROLL-OFF**				VIPRF	1218
	120X,*X*=*,F12.3,6X,*NORMALIZING FREQ.RATIO,HIGH-FREQ.ROLL-CFF**				VIPRF	1219
	220X,*F*=*,F12.2,6X,*LOCATOR FREQ.,HIGH-FREQ.ROLL-OFF*/21X,*0*/				VIPRF	1220
	316X,*ALPHA*=*,F12.2,6X,*FORM FACTOR,HIGH-FREQ.ROLL-OFF**				VIPRF	1221
	420X,*F =*,F12.2,6X,*CENTER FREQ. OF TRANSFER FUNCTION(HZ.)*				VIPRF	1222
1225	521X,*C**)				VIPRF	1223
	PRINT 254,SDELTA,FMINGF,SDELTA,BUFMAX,D,XE				VIPRF	1224
	PRINT 260,SPTEF,D,SDELTA,SPTEF,FRO				VIPRF	1225
	260 FORMAT(14-,				VIPRF	1226
	120X,*NOTE: SINCE S (F)=*,G12.5,* CORRESPONDING TO D=*,G12.5/				VIPRF	1227
1230	272X				VIPRF	1228
	/25X,*IS LESS THAN DELTA=*,G12.5* ONLY THE HIGH-FREQ.ROL				VIPRF	1229
	3L-CFF PORTION */25X,*OF THE S(F) TRANSFER FUNCTION IS USED IN CALC				VIPRF	1230
	4ULATING F (F),*/70X,*01*/25X,*(S(F)=*,G12.5,* AT F=X*,4H*F =,G12.5				VIPRF	1231
	5* HZ.)**/52X,*0*)				VIPRF	1232
					VIPRF	1233
1235					VIPRF	1234
					VIPRF	1235
1238					VIPRF	1236
					VIPRF	1237
					VIPRF	1238
					VIPRF	1239
1240					VIPRF	1240
					VIPRF	1241
1245	24: XX=RS IF(RS.GT.RSMAX) XX=RSMAX				VIPRF	1242
	CALL TERPLIN(XX,X1,RSVALS(1),RSVALS,1,DELPS,DBRS,NPSVAL)				VIPRF	1243
	CALL TERPLIN(XX,Y1,RSVALS(1),RSVALS,1,F7HFHI,FPRIME,NRSVAL)				VIPRF	1244
	FRC=F7HFHI				VIPRF	1245
					VIPRF	1246
					VIPRF	1247
	AK=1.0 IF(WC.LE.2.5) GO TO 320				VIPRF	1248
	AK=0.55 IF(WC.GE.200.0) GO TO 320				VIPRF	1249
1250					VIPRF	1250
	DO 310 J=1,14				VIPRF	1251
	II=J *Y1=WEK(J)				VIPRF	1252
	IF(WC.LE.X1) GO TO 315				VIPRF	1253
	310 CONTINUE				VIPRF	1254
	315 AK=VALK(II)+(WE-X1)*(VALK(II-1)-VALK(II))/(WEK(II-1)-X1)				VIPRF	1255

PROGRAM	VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
125F	327	FZHFHI=AK*F7HFHI			VIPRF	1256
		F7HFLO=275.0*T/0.036 \$IF(CATGRY.EQ.06) FZHFLO=350.0*T/0.036			VIPRF	1257
					VIPRF	1258
					VIPRF	1259
		XHFLO=XHFLO \$XHFHI=XHFHI			VIPRF	1260
1260		X1=XHFLO*F7HFLO \$X2=XHFHI*FZHFHI \$IF(X2.GE.X1) GO TO 32F			VIPRF	1261
		CONST=0.025			VIPRF	1262
					VIPRF	1263
	323	XHFLO=XHFLO-CONST*XHFLO \$XHFHI=XHFHI+CONST*XHFHI			VIPRF	1264
		IF(XHFLO.GT.1.0) GO TO 321			VIPRF	1265
1265		XHFLO=1.0 \$XHFHI=F7HFLO/FZHFHI \$GO TO 325			VIPRF	1266
					VIPRF	1267
	321	IF(XHFHI.LT.1.0) GO TO 322			VIPRF	1268
		XHFHI=1.0 \$XHFLO=F7HFHI/FZHFLO \$GO TO 325			VIPRF	1269
					VIPRF	1270
1270	322	X1=XHFLO*F7HFLO \$X2=XHFHI*FZHFHI \$IF(X2.LT.X1) GO TO 323			VIPRF	1271
		XHFLO=X2/F7HFLO			VIPRF	1272
					VIPRF	1273
					VIPRF	1274
	325	DELWE=C. \$IF(WE.LE.10.0) GO TO 340			VIPRF	1275
1275		IF(CATGRY.NE.018.AND.CATGRY.NE.06) GO TO 340			VIPRF	1276
		IF(WE.GE.100.) GO TO 330			VIPRF	1277
		CALL TERFLIN(WE,DWE100,10.,X1,0,DELWE,WE100,NWE100)			VIPRF	1278
		GO TO 340			VIPRF	1279
	330	IF(WE.GE.1000.) GO TO 335			VIPRF	1280
1280		CALL TERFLIN(WE,DWE1K,100.,X1,0,DELWE,WE1000,NWE1K)			VIPRF	1281
		GO TO 340			VIPRF	1282
	335	DELWE=WE5000(9) \$IF(WE.GT.WEMAX) GO TO 340			VIPRF	1283
		CALL TERFLIN(WE,DWE5K,1000.0,X1,0,DELWE,WE5000,NWE5K)			VIPRF	1284
					VIPRF	1285
1285					VIPRF	1286
					VIPRF	1287
	340	DELWS=C. \$IF(WS.LE.0.5) GO TO 350			VIPRF	1288
		DELWS=20.*ALOG10(0.5/WS)			VIPRF	1289
					VIPRF	1290
					VIPRF	1291
1290	350	IF(CATGRY.EQ.06) XHFMAY=XHFMAY+7.0			VIPRF	1292
		XHFCOR=XHFMAY+DELWE+DELWS+DELRS			VIPRF	1293
		IF(IFLITE.EQ.ISANFL) GO TO 351			VIPRF	1294
		PRINT 246 \$PRINT 353,IPLANK,IFLITE			VIPRF	1295
	246	FORMAT(1H1)			VIPRF	1296
1295	353	FORMAT(1H-,7H*****,3A10,1H-,A10,7H*****)			VIPRF	1297
	351	II=4HH(F) \$PRINT 363,II,IPLANK			VIPRF	1298
	363	FORMAT(1H-,*PARAMETERS OF THE TRANSFER FUNCTION FOR: *,A10/43X,A2)			VIPRF	1299
		PRINT 355,XHFMAY,DELRS,DELWE,DELWS,XHFCOR			VIPRF	1300
	355	FORMAT(			VIPRF	1301
1300		175X,*2*,13X,*-4*,8Y,*2 2*/17X,*H (F)=*,F12.2,6X,*MAXIMUM VALUE OF			VIPRF	1302
		2 H(F)-DR.RE. 1.0 G /47.,RE.(2X10 DYNES-CM. ) /HZ.*18X,*M*/			VIPRF	1303
		216X,*DEL R =*,F12.2,6X,*CORRECTION FACTOR TO H (F) FOR R (DB.)*/			VIPRF	1304
		321X,*S*,41X,*M*,9X,*S*/			VIPRF	1305
		416X,*DEL W =*,F12.2,6X,*CORRECTION FACTOR TO H (F) FOR W (DB.)*/			VIPRF	1306
1305		521X,*F*,41X,*M*,9X,*F*/			VIPRF	1307
		616X,*DEL W =*,F12.2,6X,*CORRECTION FACTOR TO H (F) FOR W (DB.)*/			VIPRF	1308
		821X,*S*,41X,*M*,9X,*S*/			VIPRF	1309
		917X,*H (F)=*,F12.2,6X,*CORRECTED VALUE OF H (F)*/18X,*M*,2X,			VIPRF	1310
		**R*,30X,*M*)			VIPRF	1311
1310					VIPRF	1312
		IF(WE.LE.10.0) GO TO 375				



PROGRAM VICEF	74/74	OPT=1	FTN 4,5+414	08/16/77	13.11.28
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	IF(CATGRY.EQ.012.OR.CATGRY.EQ.06) GO TO 375	VIPRF	1313
	PRINT 254	VIPRF	1314
1315	350 FORMAT(1HC,*NOTE:THE CORRECTION FACTOR FOR W IS SET EQUAL TO ZERO	VIPRF	1315
	1 EVEN THOUGH W >10 POUNDS.*//33X,*F*,35X,*F*//)	VIPRF	1316
		VIPRF	1317
		VIPRF	1318
	373 RHFI=0.6 IF(RS.GT.0.) RHFI=0.3	VIPRF	1319
	PRINT 340,RHFLC,RHFI,XHFLO,XHFHI,FZHFLO,FZHFHI	VIPRF	1320
1320	380 FORMAT(	VIPRF	1321
	120X,*F*=?,F12.3,6X,*SLOPE FACTOR,LOW-FREQ.ROLL-OFF*/	VIPRF	1322
	220X,*F*=?,F12.3,6X,*SLOPE FACTOR,HIGH FREQ.ROLL-OFF*/	VIPRF	1323
	320X,*X*=?,F12.3,6X,*NORMALIZING FREQ.RATIO,LOW-FREQ.ROLL-OFF*/	VIPRF	1324
	420X,*Y*=?,F12.3,6X,*NORMALIZING FREQ.RATIO,HIGH-FREQ.ROLL-OFF*/	VIPRF	1325
1325	520X,*F*=?,F12.2,6X,*LOCATOR FREQ., LOW FREQ.ROLL-OFF*/21X,*0*/	VIPRF	1326
	620X,*F*=?,F12.2,6X,*LOCATOR FREQ.,HIGH FREQ.ROLL-OFF*/21X,*0*/	VIPRF	1327
	PRINT 362,K,FRO	VIPRF	1328
	390 FORMAT(21X,*K*=?,F12.4,6X,*CORRECTION FACTOR TO F' FOR k (F'=K X *,	VIPRF	1329
	1F8.1,*)*/63X,*0*,6X,*F*,2X,*0*/	VIPRF	1330
1330	PRINT 425,AMFLC,AMFHI	VIPRF	1331
		VIPRF	1332
		VIPRF	1333
	C *****	VIPRF	1334
	C * * *	VIPRF	1335
1335	C * M (F) *	VIPRF	1336
	C * * *	VIPRF	1337
	C *****	VIPRF	1338
	IF(IFLITE.NE.ISANFL) GO TO 356	VIPRF	1339
	PRINT 246 PRINT 353,IPLAND,IPLITE	VIPRF	1340
1340	354 II=4*H(F) PRINT 383,II,IPLANK	VIPRF	1341
	FZMFLO=FMFLO *FZMFHI=FMFHI	VIPRF	1342
		VIPRF	1343
	DELR=0. IF(RS.GE.2.9) GO TO 370	VIPRF	1344
1345	CALL CLAC(XX,EXMERS,C.,DELR,OBMERS,NMERS)	VIPRF	1345
		VIPRF	1346
	370 DELWS=0.1*DELR	VIPRF	1347
		VIPRF	1348
	IF(CATGRY.EQ.06) XMFMAX=XMFMAX+2.0	VIPRF	1349
1350	XMFCCR=XMFMAX+DELR+DELR	VIPRF	1350
		VIPRF	1351
	PRINT 385,XMFMAX,DELR,DELR,XMFCCR	VIPRF	1352
	PRINT 380,AMFLC,AMFHI,XHFLO,XHFHI,FZHFLO,FZHFHI	VIPRF	1353
	380 FORMAT(	VIPRF	1354
	175Y,*2*,17X,*-4*,9X,*2 2*/17X,*M (F)=*,F12.2,6X,*MAXIMUM VALUE OF	VIPRF	1355
1355	2 M(F)=OB.PF. 1.0 G /H7./RE.(2X10 DYNES-CM. ) /HZ.*//18X,*M*/	VIPRF	1356
	316X,*FCL W =*,F12.2,6X,*CORRECTION FACTOR TO M (F) FOR W (DE.)*//	VIPRF	1357
	421X,*S*,41X,*M*,9X,*S*/	VIPRF	1358
	516X,*FCL R =*,F12.2,6X,*CORRECTION FACTOR TO M (F) FOR R (DE.)*//	VIPRF	1359
	621X,*S*,41X,*M*,9X,*S*/	VIPRF	1360
1360	717X,*M (F)=*,F12.2,6X,*CORRECTED VALUE OF M (F)*//18X,*M*,2X,*C*,	VIPRF	1361
	839X,*M*)	VIPRF	1362
	PRINT 425,AMFLC,AMFHI	VIPRF	1363
		VIPRF	1364
		VIPRF	1365
1365	C *****	VIPRF	1366
	C * * *	VIPRF	1367
	C * L (F) *	VIPRF	1368
	C * * *	VIPRF	1369



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1370	*****	VIPRF	1370
	M=1HF	VIPRF	1371
	CALL QUAD(XE,DXMOD1,0.,CORLEF,DBMOD1,NMODE1)	VIPRF	1372
	IF(CORLEF.LT.-21.0) CORLEF=-21.0	VIPRF	1373
	XLFCOF=XLFMX+CORLEF	VIPRF	1374
1375		VIPRF	1375
	IF(IFLITE.EQ.ISANDL) GO TO 387	VIPRF	1376
	PRINT 246 \$PRINT 353,IPLANE,IFLITE	VIPRF	1377
387	II=4HL(F) \$PRINT 383,II,IPLANK	VIPRF	1378
	J=1HM \$K=1H \$L=1HC	VIPRF	1379
	\$PRINT 390,XLFMAX,J,K,K,CORLEF,XE,IPLANE(1),M,J,M,XLFCCR,J,L,J	VIPRF	1380
1380	390 FORMAT(	VIPRF	1381
	176Y,*2*,12X,*-4*,8X,*2 2*/17X,*L (F)=*,F12.2,6X,*MAXIMUM VALUE OF	VIPRF	1382
	2 L (F)-RD,RC. 1.0 G /47.,RC.(2X10 FYNES-CM. ) /HZ.*//16X,A1,2X,A2,	VIPRF	1383
	336X,A1/	VIPRF	1384
	416X,*CFL X=*,F12.2,6X,*CORRECTION FACTOR TO L (F) FOR DISTANCE X	VIPRF	1385
1385	F=*,F6.2,* CN*,A10,* TYPE AIRCRAFT*/21X,A2,40X,A1,16X,A2/	VIPRF	1386
	617Y,*L (F)=*,F12.2,6X,*CORRECTED VALUE OF L (F)*//16X,A1,2X,A2,	VIPRF	1387
	738X,A1)	VIPRF	1388
		VIPRF	1389
	FZLFLO=FN/2.0 \$FZLFHI=2.0*FN	VIPRF	1390
1390	PLFLO=9RLFLO \$PLFHI=9PLFHI \$XLFO=XXLFLO \$XLFHI=XXLFHI	VIPRF	1391
		VIPRF	1392
	IF(F2N.EQ.0.) GO TO 395	VIPRF	1393
	PLFHI=.23 \$XLFHI=0.70 \$FZLFHI=1.42*FN	VIPRF	1394
		VIPRF	1395
1395	390 PRINT 380,PLFLO,PLFHI,XLFLO,XLFHI,FZLFLO,FZLFHI	VIPRF	1396
	ILINE1(1)=10HFIRST BODY \$ILINE1(2)=10H BENDING M	VIPRF	1397
	ILINE1(3)=10HMODE FREQU \$ILINE1(4)=8HNCY(HZ.) \$ILINE1(5)=1H	VIPRF	1398
	IFN=1HN \$PRINT 441,FN,(ILINE1(II),II=1,7),IFN	VIPRF	1399
	PRINT 425,PLFLO,ALFHI	VIPRF	1400
1400		VIPRF	1401
	*****	VIPRF	1402
	* * *	VIPRF	1403
	* L (F) *	VIPRF	1404
1405	* 2 *	VIPRF	1405
	* * *	VIPRF	1406
	*****	VIPRF	1407
	IF(F2N.EQ.0.) GO TO 399	VIPRF	1408
		VIPRF	1409
1410	CALL QUAD(XE,DXMOD2,0.,CORL2F,DBMOD2,NMODE2)	VIPRF	1410
	IF(CORL2F.LT.-21.0) CORL2F=-21.0	VIPRF	1411
	XL2FCF=XL2FMX+CORL2F	VIPRF	1412
		VIPRF	1413
	IF(IFLITE.EQ.ISANDL) GO TO 393	VIPRF	1414
1415	PRINT 246 \$PRINT 353,IPLANE,IFLITE	VIPRF	1415
	393 II=4HL(F) \$J=1HM \$K=1H2 \$L=2HMC \$PRINT 383,II,K	VIPRF	1416
	PRINT 390,XL2FMX,K,J,K,CORL2F,XE,IPLANE(1),M,K,M,XL2FCR,K,L,K	VIPRF	1417
		VIPRF	1418
	FL2FLO=F2N/XL2FLO \$FL2FHI=F2N/XL2FHI	VIPRF	1419
1420	PRINT 380,FL2FLO,FL2FHI,XL2FLO,XL2FHI,FL2FLO,FL2FHI	VIPRF	1420
		VIPRF	1421
	ILINE1(1)=10HSECOND BODY \$ILINE1(2)=10HY BENDING	VIPRF	1422
	ILINE1(3)=10HMODE FREQU \$ILINE1(4)=9HENCY(HZ.) \$ILINE1(5)=1H	VIPRF	1423
	IFN=2H2N \$PRINT 441,F2N,(ILINE1(II),II=1,7),IFN	VIPRF	1424
1425	PRINT 425,AL2FLO,AL2FHI	VIPRF	1425
		VIPRF	1426

PROGRAM	VIPRF	74/74	CPT=1	FTN 4,5+414	08/16/77	13.11.28
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					VIPRF	1427
					VIPRF	1428
					VIPRF	1429
1430	387	IFN=1HC \$IF(CATGRY,EO,C4A) IFN=3HC3A \$IF(CATGRY,EO,C4B) IFN=3HC3P			VIPRF	1430
		ILINE1(1)=10HISOLATOR N \$ILINE1(2)=10HATURAL FRE			VIPRF	1431
		ILINE1(3)=10HQUENCY(HZ. \$ILINE1(4)=1H)			VIPRF	1432
					VIPRF	1433
		IF(CATGRY,EO,C1A) GO TO 398			VIPRF	1434
		IF(CATGRY,EO,C1B) GO TO 430			VIPRF	1435
1435		IF(CATGRY,EO,C2A) GO TO 431			VIPRF	1436
		IF(CATGRY,EO,C2B) GO TO 433			VIPRF	1437
		IF(CATGRY,EO,C3A) GO TO 442			VIPRF	1438
		IF(CATGRY,EO,C3B) GO TO 435			VIPRF	1439
		IF(CATGRY,EO,C4A) GO TO 398			VIPRF	1440
1440		IF(CATGRY,EO,C4B) GO TO 398			VIPRF	1441
		IF(CATGRY,EO,C5) GO TO 427			VIPRF	1442
		IF(CATGRY,EO,C6) GO TO 427			VIPRF	1443
					VIPRF	1444
					VIPRF	1445
1445	C	*****			VIPRF	1446
	C	* * * * *			VIPRF	1447
	C	* CATEGORY 1A *			VIPRF	1448
	C	* * * * *			VIPRF	1449
		399 DELWE=C. \$IF(WF,LF,10,0) GO TO 410			VIPRF	1450
1450		IF(WF,LT,210,0) GO TO 435			VIPRF	1451
		C1AAHI=1.92 \$DELWE=-6.7			VIPRF	1452
		GO TO 410			VIPRF	1453
		400 CALL QUAD(WF,DXC1A,XINC1A,C1AAHI,C1AAWF,NC1A)			VIPRF	1454
		CALL QUAD(WF,DXC1A,XINC1A,DELWE,C1AMWE,NC1A)			VIPRF	1455
1455		410 C1AMXC=C1AMAX+DELWE			VIPRF	1456
					VIPRF	1457
		IF(FCCAT1,EO,0.) FCCAT1=C1AFH			VIPRF	1458
		C1AFZL=FCCAT1/C1AYLO \$C1AFZH=FCCAT1/C1AXHI \$FC=FCCAT1			VIPRF	1459
					VIPRF	1460
1460					VIPRF	1461
		ILINE2(1)=10H(EQUIPMENT \$ILINE2(2)=10H MOUNTED O			VIPRF	1462
		ILINE2(3)=10HN PRIMARY \$ILINE2(4)=10HSTRUCTURE			VIPRF	1463
		ILINE2(5)=10HTHROUGH IS \$ILINE2(6)=10HOLATORS)			VIPRF	1464
					VIPRF	1465
1465		IF(CATGRY,NE,C1A) GO TO 415			VIPRF	1466
					VIPRF	1467
		PEAK=C1AMXC \$XLO=C1AXLO \$XHI=C1AXHI \$PLO=C1APLO \$PHI=C1APHI			VIPRF	1468
		ALC=C1AALC \$AHI=C1AAHI \$FZLO=C1AFZL \$FZHI=C1AFZH			VIPRF	1469
		GO TO 440			VIPRF	1470
1470					VIPRF	1471
		415 PRINT 246 \$PRINT 353,IPLANE,IPLIFE			VIPRF	1472
		IT=PHY (F) \$L=241A \$PRINT 387,II,L \$PRINT 438,CATGRY			VIPRF	1473
		PRINT 420,C1AMAX,IPLANE(1),DELWE,WF,C1AMXC			VIPRF	1474
		PRINT 380,C1APLO,C1APHI,C1AXLO,C1AXHI,C1AFZL,C1AFZH			VIPRF	1475
1475		L=3HC1A \$PRINT 441,FCCAT1,(ILINE1(K),K=1,7),L			VIPRF	1476
		PRINT 425,C1AALO,C1AAHI			VIPRF	1477
					VIPRF	1478
		IF(CATGRY,EO,C4A) GO TO 442			VIPRF	1479
		GO TO 435			VIPRF	1480
1480					VIPRF	1481
					VIPRF	1482
	C	*****			VIPRF	1483

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	C	*			VIPRF	1484
	C	* CATEGORY 2A	*		VIPRF	1485
1485	C	*	*		VIPRF	1486
	C	*****			VIPRF	1487
	C	431 PEAK=C2AMAX \$XLO=C2AXLC \$XHI=C2AXHI \$BLO=C2APLO \$BHI=C2ABHI			VIPRF	1488
	C	ALC=C2AALC \$AHI=C2AAHI			VIPRF	1489
	C				VIPRF	1490
1490	C	IF(FCCAT1.EQ.0.) FCCAT1=C2AFN			VIPRF	1491
	C	FZLO=FCCAT1/XLO \$FZHI=FCCAT1/XHI \$FC=FCCAT1			VIPRF	1492
	C				VIPRF	1493
	C	ILINE2(1)=10H(SECONDARY \$ILINE2(2)=10H STRUCTURE			VIPRF	1494
	C	ILINE2(3)=10H EQUIP.MOU \$ILINE2(4)=10HNTED ON IN			VIPRF	1495
1495	C	ILINE2(5)=10HSTRUMENT P \$ILINE2(6)=10HANEL,ISCL. \$ILINE2(7)=2H)\$			VIPRF	1496
	C	GO TO 440			VIPRF	1497
	C				VIPRF	1498
	C				VIPRF	1499
1500	C	*****			VIPRF	1500
	C	* CATEGORY 2B	*		VIPRF	1501
	C	*	*		VIPRF	1502
	C	*****			VIPRF	1503
	C	437 PEAK=C2BMAX \$XLO=C2BXLC \$XHI=C2BXHI \$BLO=C2BPLO \$BHI=C2BRHI			VIPRF	1504
1505	C	ALC=C2BALC \$AHI=C2BAHI			VIPRF	1505
	C				VIPRF	1506
	C	IF(FCCAT1.EQ.0.) FCCAT1=C2BFN			VIPRF	1507
	C	FZLO=FCCAT1/XLC \$FZHI=FCCAT1/XHI \$FC=FCCAT1			VIPRF	1508
	C				VIPRF	1509
1510	C	ILINE1(1)=10HFIRST INST \$ILINE1(2)=10HRUMENT PAN			VIPRF	1510
	C	ILINE1(3)=10HEL RESOMAN \$ILINE1(4)=7HCE(HZ.)			VIPRF	1511
	C				VIPRF	1512
	C	ILINE2(1)=10H(SECONDARY \$ILINE2(2)=10H STRUCTURE			VIPRF	1513
	C	ILINE2(3)=10H EQUIP.MOU \$ILINE2(4)=10HNTED ON IN			VIPRF	1514
1515	C	ILINE2(5)=10HSTRU.PANEL \$ILINE2(6)=10H,NON-ISCL. \$ILINE2(7)=2H)\$			VIPRF	1515
	C	GO TO 440			VIPRF	1516
	C				VIPRF	1517
	C				VIPRF	1518
	C				VIPRF	1519
1520	C	*****			VIPRF	1520
	C	* CATEGORY 3A	*		VIPRF	1521
	C	*	*		VIPRF	1522
	C	*****			VIPRF	1523
	C	442 XX=2H3A			VIPRF	1524
1525	C	PBI=C3ABHI \$XLC=C3AXLC \$ALC=C3AALC			VIPRF	1525
	C				VIPRF	1526
	C	IF(WE.CT.10.0) GO TO 447			VIPRF	1527
	C	PEAK=C3AMAX \$PLO=C3APLC \$XHI=C3AXHI \$AHI=C3AAHI			VIPRF	1528
	C	GO TO 448			VIPRF	1529
1530	C				VIPRF	1530
	C	447 IF(WE.LT.200.0) GO TO 444			VIPRF	1531
	C	PEAK=C3AYMX(NC3) \$PLO=C3AP(NC3) \$XHI=C3AXF(NC3) \$AHI=C3AAP(NC3)			VIPRF	1532
	C	GO TO 448			VIPRF	1533
	C				VIPRF	1534
	C				VIPRF	1535
1535	C	444 CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,PEAK,C3AYMX,NC3)			VIPRF	1536
	C	CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,PLO,C3AP,NC3)			VIPRF	1537
	C	CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,XHI,C3AXF,NC3)			VIPRF	1538
	C	CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,AHI,C3AAP,NC3)			VIPRF	1539
	C				VIPRF	1540

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1540	448	FC=FCCAT1 \$IF (CATGRY,FC,04A) FC=FCCAT2 \$IF (FC,EO,0.) FC=C3AFK FZLO=FC/XLO \$FZHI=FC/YHI	VIPRF	1541		
			VIPRF	1542		
			VIPRF	1543		
			VIPRF	1544		
1545		ILINE2(1)=10H(EQUIPMENT \$ILINE2(2)=10H HARD MOUN ILINE2(3)=10HTFD ON ISC \$ILINE2(4)=10HLATED SHEL ILINE2(5)=10HF OP BACK \$ILINE2(6)=2H)\$ GO TO 440	VIPRF	1545		
			VIPRF	1546		
			VIPRF	1547		
			VIPRF	1548		
			VIPRF	1549		
1550			VIPRF	1550		
			VIPRF	1551		
			VIPRF	1552		
			VIPRF	1553		
			VIPRF	1554		
1555			VIPRF	1555		
			VIPRF	1556		
			VIPRF	1557		
			VIPRF	1558		
			VIPRF	1559		
1560		ILINE1(1)=10HLOWEST SHF \$ILINE1(2)=10HLE FIRST R ILINE1(3)=10HENDING MOD \$ILINE1(4)=FHE(HZ.)	VIPRF	1560		
			VIPRF	1561		
			VIPRF	1562		
			VIPRF	1563		
			VIPRF	1564		
			VIPRF	1565		
1565	446	IF (WE,GT,10.0) GO TO 447 PLC=C3BLC \$PHI=C3BPHI \$XLO=C3XLO \$XHI=C3FXHI \$ALO=C3ALO \$AHI=C3AHI PEAK=-6.0-2.0*(WE-10.0)/3. GO TO 449	VIPRF	1566		
			VIPRF	1567		
			VIPRF	1568		
			VIPRF	1569		
1570	447	CALL TERPLIN(WE,Y1,C3WE(1),C3WE,1,PEAK,C3BYMX,NC3) CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,PLC,C3BPHI,NC3) CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,PHI,C3BPHI,NC3) CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,XLO,C3BX,NC3) CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,XHI,C3BYF,NC3) CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,ALO,C3BA,NC3) CALL TERPLIN(WE,X1,C3WE(1),C3WE,1,AHI,C3BAF,NC3)	VIPRF	1570		
			VIPRF	1571		
			VIPRF	1572		
			VIPRF	1573		
			VIPRF	1574		
1575			VIPRF	1575		
			VIPRF	1576		
			VIPRF	1577		
			VIPRF	1578		
			VIPRF	1579		
1580	449	FC=FCCAT1 \$IF (CATGRY,FC,04B) FC=FCCAT2 \$IF (FC,EO,0.) FC=C3FFK FZLO=FC/XLO \$FZHI=FC/YHI	VIPRF	1580		
			VIPRF	1581		
			VIPRF	1582		
			VIPRF	1583		
			VIPRF	1584		
1585		ILINE2(1)=10H(EQUIPMENT \$ILINE2(2)=10H HARD MOUN ILINE2(3)=10HTFD ON MOUN \$ILINE2(4)=10H-ISOLATED ILINE2(5)=10HSHLE OP R \$ILINE2(6)=5HACK)\$ GO TO 440	VIPRF	1585		
			VIPRF	1586		
			VIPRF	1587		
			VIPRF	1588		
			VIPRF	1589		
1590			VIPRF	1590		
			VIPRF	1591		
			VIPRF	1592		
			VIPRF	1593		
			VIPRF	1594		
			VIPRF	1595		
1595	437	DELWE=0. \$IF (WE,LE,1.0) GO TO 436 DELWE=-6.0 \$IF (WE,GE,10.0) GO TO 436 DELWE=-6.0-2.0*(WE-10.0)/3. PEAK=C3MAX+DELWE PLC=C3BLC \$PHI=C3BPHI \$XLO=C3XLO \$XHI=C3FXHI \$ALO=C3ALO \$AHI=C3AHI	VIPRF	1596		
			VIPRF	1597		



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	IF(FCCAT1.EC,J.) FCCAT1=055N	VIPRF	1598
	FZLQ=FCCAT1/XLO F7HI=FCCAT1/XHI FFC=FCCAT1	VIPRF	1599
		VIPRF	1600
1600		VIPRF	1601
	ILINE2(1)=10H(LIGHT WSI SILINE2(2)=10HGH T EQUIP.	VIPRF	1602
	ILINE2(3)=10HMCOUNTED ON SILINE2(4)=10H PRIMARY S	VIPRF	1603
	ILINE2(5)=10HTPUCTURE P SILINE2(6)=10HY BRACKETS	VIPRF	1604
	ILINE2(7)=2H)3	VIPRF	1605
1605		VIPRF	1606
	ILINE1(1)=10HLOWEST NAT SILINE1(2)=10HURAL FREQU	VIPRF	1607
	ILINE1(3)=10HENCY OF BR SILINE1(4)=10HACKET AND	VIPRF	1608
	ILINE1(5)=10HEQUIPMENT SILINE1(6)=10HCOMBINATIO	VIPRF	1609
	ILINE1(7)=5HN(H7.)	VIPRF	1610
1610	GO TO 440	VIPRF	1611
		VIPRF	1612
		VIPRF	1613
	C *****	VIPRF	1614
	C *	VIPRF	1615
1615	C * CATEGORY 6 *	VIPRF	1616
	C *	VIPRF	1617
	C *****	VIPRF	1618
		VIPRF	1619
	437 IF(IFLITE.NE.ISANDL) PRINT 245	VIPRF	1620
1620	PRINT 438	VIPRF	1621
	439 FORMAT(1H-,*TRANSFER FUNCTION FOR CATEGORY 6: EQUIP.MOUNTED ON,OR	VIPRF	1622
	1 ATTACHED TO FORWARD LOOKING RADAR PULK-HEADS*///	VIPRF	1623
	2* FOR THIS CATEGORY Y(F)=1 AT ALL FREQUENCIES SO THAT R(F)=Y(F)G(F	VIPRF	1624
	3)=G(F).*/	VIPRF	1625
1625	4* CHANGES ARE MADE AS FOLLOWS WHEN THIS CATEGORY IS SPECIFIED:*/	VIPRF	1626
	520X,*H(F)*7.0 DB IS ADDED TO H(F)*/4EX,*M*/	VIPRF	1627
	622X,*F + F =350,CT/0.035(T DENOTES PLATE THICKNESS)*/23X,*C*4X*0*/	VIPRF	1628
	720X,*M(F)*2.0 DB IS ADDED TO M(F)*/4EX,*M*)	VIPRF	1629
	GO TO 600	VIPRF	1630
1630		VIPRF	1631
		VIPRF	1632
	440 IF(IFLITE.NE.ISANDL) PRINT 246	VIPRF	1633
	II=5HY (F) IJ=1HM SM=1H	VIPRF	1634
	PRINT 383,II,XX	VIPRF	1635
1635	IF(CATEGORY.EC,C4A.OR.CATEGORY.EC.C4B) PRINT 438,CATGRY	VIPRF	1636
	IF(CATEGORY.EC.C5) PRINT 420,OSMAX,IPLANE(1),DELWF,WE,PEAK	VIPRF	1637
	IF(CATEGORY.NE.C5) PRINT 352,II,PEAK,II,IPLANE(1),J,M,M	VIPRF	1638
	PRINT 386,SLO,BHI,XLO,XHI,FZLQ,F7HI	VIPRF	1639
		VIPRF	1640
1640	PRINT 441,FC,(ILINE1(II),II=1,7),IFN	VIPRF	1641
	PRINT 428,ALO,AHI	VIPRF	1642
	420 FORMAT(	VIPRF	1643
	217X,*Y (F)=*,F12.2,6X,*MAXIMUM VALUE OF Y(F)-DB.,FOR*,A10,	VIPRF	1644
	3*TYPE AIRCRAFT*/18X,*M*/	VIPRF	1645
1645	416X,*DEL W =*,F12.2,6X,*CORRECTION FACTOR TO Y (F) FOR EQUIPMENT WE	VIPRF	1646
	518T W =*,F6.1 * LBS.*/21X,*F*,41X,*M*,26X,*F*/	VIPRF	1647
	617X,*Y (F)=*,F12.2,6X,*CORRECTED VALUE OF Y (F)*/18X,*M*,2X,*C*,	VIPRF	1648
	739X,*M*)	VIPRF	1649
	425 FORMAT(	VIPRF	1650
1650	116X,*ALPHA =*,F12.3,6X,*FORM FACTOR,LOW-FREQ.ROLL-OFF*/	VIPRF	1651
	216X,*ALPHA' =*,F12.3,6X,*FORM FACTOR,HIGH-FREQ.ROLL-OFF*)	VIPRF	1652
	433 FORMAT(42X,*REQUIRED WHEN CATEGORY *,A2,* EQUIPMENT MOUNTING IS S	VIPRF	1653
	10ECIFIED)*///)	VIPRF	1654



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1655 441 FORMAT(2CX,*F=*,F12.2,5X,7A10/21X,A3)
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 \*  
 \* L(F)-H(F)-H(F) \*  
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 \*\*\*\*\*  
 600 TWOB(1)=2.\*BLFLO \$TWOB(2)=2.\*BMFLO \$TWOB(3)=2.\*BHFL0  
 F7(1)=F7LFLO \$F7(2)=F7MFLO \$F7(3)=F7HFLO  
 XFERM(1)=XLFCOR \$XFERM(2)=XMFCCR \$XFERM(3)=XHFCOR  
 FLX(1)=ATAN2(TWOB(1)\*(XLFLO\*\*ALFLO),1.-XLFLO\*XLFLO)  
 FLX(2)=ATAN2(TWOB(2)\*(XMFLO\*\*AMFLO),1.-XMFLO\*XMFLO)  
 FLX(3)=ATAN2(TWOB(3)\*(XHFL0\*\*AHFL0),1.-XHFL0\*XHFL0)  
 ALPHA(1)=ALFLO \$ALPHA(2)=AMFLO \$ALPHA(3)=AHFL0  
 HILO(1)=0. \$HILO(2)=0. \$HILO(3)=0.  
 SIGN(1)=1.0 \$SIGN(2)=1.0 \$SIGN(3)=1.0 \$K=3 \$DP(4)=-1000.0  
 J=0 \$CONST=0.10 \$II=1 \$L=0  
 FRQ=FMINF \$FMAX=XLFL0\*F7LFLO  
 IF(F2N.EQ.0.) GO TO 620  
 Y1=XL2FLO\*FL2FLO \$IF(X1.GE.FMAX) GO TO 610  
 PRINT 605,Y1,FMAX  
 605 FORMAT(1H-,\*THE FREQUENCY AT WHICH THE MAXIMUM VALUE OF L2(F) OCCU  
 1RS,\*,G12.5,\* HZ,\*/\* IS LESS THAN THE CORRESPONDING FREQUENCY FOR L  
 2(F),\*,G12.5/\* THE PROGRAM ASSUMES THAT THE FREQUENCY OF THE MAXIMU  
 3M VALUE OF L2(F) WILL BE \*/\* GREATER THAN OR EQUAL TO THE CORRESPON  
 4DING FREQUENCY OF L(F),\*)  
 GO TO 1000  
 610 TWOB(4)=2.\*BL2FLO \$F7(4)=FL2FLO \$ALPHA(4)=AL2FLO  
 XFERM(4)=XL2FCR  
 FLX(4)=ATAN2(TWOB(4)\*(XL2FLO\*\*AL2FLO),1.-XL2FLO\*XL2FLO)  
 K=4 \$HILO(4)=0. \$SIGN(4)=1.0  
 IF(FMAX.LE.FMINF) GO TO 625  
 CALL GPCINTS(FREQ,DECBEL,FRQ,FMAX,CONST,DP,XFERMX,TWOB,FLX,F7,  
 1HILO,SIGN,ALPHA,II,J,K,L)  
 FRQ=FMAX  
 625 FMAX=XMFLO\*F7MFLO  
 TWOB(1)=2.\*BLFHI \$F7(1)=F7LFHI \$ALPHA(1)=ALFHI  
 FLX(1)=PI-ATAN2(TWOB(1)\*(XLFHI\*\*ALFHI),1.-XLFHI\*XLFHI)  
 HILO(1)=PI \$SIGN(1)=-1.0  
 IF(F2N.EQ.0.) GO TO 640  
 IF(X1.LE.FRQ) GO TO 630  
 FMAX=X1 \$II=1  
 CALL GPCINTS(FREQ,DECBEL,FRQ,FMAX,CONST,DP,XFERMX,TWOB,FLX,F7,

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	1HILO, SIGN, ALPHA, II, J, K, L)		VIPRF	1712
	FRQ=FMAX \$FMAX=XMFLO*FZMFLO		VIPRF	1713
			VIPRF	1714
1715	63* TWOB(4)=2.0*RL2FHI \$FZ(4)=FL2FHI \$ALPHA(4)=AL2FHI		VIPRF	1715
	FLX(4)=PI-ATAN2(TWOB(4)*(XL2FHI**AL2FHI), 1.-XL2FHI*XL2FHI)		VIPRF	1716
	HILO(4)=PI \$SIGN(4)=-1.0		VIPRF	1717
			VIPRF	1718
	64* II=1		VIPRF	1719
1720	CALL GPOINTS(FREQ, DECBEL, FRQ, FMAX, CONST, DB, XFERMX, TWOB, FLX, FZ,		VIPRF	1720
	1HILO, SIGN, ALPHA, II, J, K, L)		VIPRF	1721
			VIPRF	1722
	FRQ=FMAX \$FMAX=XMFHI*FZMFHI		VIPRF	1723
	IF(FMAX.EQ.FRQ) GO TO 590		VIPRF	1724
	DB(2)=XMFCCR \$II=1 \$L=2		VIPRF	1725
1725	CALL GPOINTS(FREQ, DECBEL, FRQ, FMAX, CONST, DB, XFERMX, TWOB, FLX, FZ,		VIPRF	1726
	1HILO, SIGN, ALPHA, II, J, K, L)		VIPRF	1727
			VIPRF	1728
			VIPRF	1729
	590 FRQ=FMAX \$FMAX=XHFLO*FZHFLO		VIPRF	1730
1730	TWOB(2)=2.0*RMFHI \$FZ(2)=FZMFHI \$ALPHA(2)=AMFHI		VIPRF	1731
	FLX(2)=PI-ATAN2(TWOB(2)*(XMFHI**AMFHI), 1.-XMFHI*XMFHI)		VIPRF	1732
	HILO(2)=PI \$SIGN(2)=-1. \$II=1 \$L=0		VIPRF	1733
	CALL GPOINTS(FREQ, DECBEL, FRQ, FMAX, CONST, DB, XFERMX, TWOB, FLX, FZ,		VIPRF	1734
1735	1HILO, SIGN, ALPHA, II, J, K, L)		VIPRF	1735
			VIPRF	1736
	FRQ=FMAX \$FMAX=XHFHI*FZHFHI		VIPRF	1737
	IF(FMAX.EQ.FRQ) GO TO 590		VIPRF	1738
	DB(3)=XHFCCR \$II=1 \$L=3		VIPRF	1739
1740	CALL GPOINTS(FREQ, DECBEL, FRQ, FMAX, CONST, DB, XFERMX, TWOB, FLX, FZ,		VIPRF	1740
	1HILO, SIGN, ALPHA, II, J, K, L)		VIPRF	1741
			VIPRF	1742
			VIPRF	1743
			VIPRF	1744
	590 FRQ=FMAX \$FMAX=FMAXGF		VIPRF	1745
1745	TWOB(3)=2.0*BMFHI \$FZ(3)=FZMFHI \$ALPHA(3)=AMFHI		VIPRF	1746
	FLX(3)=PI-ATAN2(TWOB(3)*(XMFHI**AMFHI), 1.-XMFHI*XMFHI)		VIPRF	1747
	HILO(3)=PI \$SIGN(3)=-1. \$II=1 \$L=0		VIPRF	1748
	CALL GPOINTS(FREQ, DECBEL, FRQ, FMAX, CONST, DB, XFERMX, TWOB, FLX, FZ,		VIPRF	1749
1750	1HILO, SIGN, ALPHA, II, J, K, L)		VIPRF	1750
	NPTS=J		VIPRF	1751
			VIPRF	1752
			VIPRF	1753
			VIPRF	1754
1755	C *****		VIPRF	1755
	C *		VIPRF	1756
	C * P(F)		VIPRF	1757
	C *		VIPRF	1758
	C *****		VIPRF	1759
			VIPRF	1760
1760	LXNAME(1)=10H(F)PEQUENC SLXNAME(2)=10H(V(H)7())\$		VIPRF	1761
	X=XE \$YSTEP=5.0		VIPRF	1762
			VIPRF	1763
	IF(INCPLT.EQ.IPLANK) GO TO 459		VIPRF	1764
1765	IPLCT=IPLCT+1		VIPRF	1765
			VIPRF	1766
	LXNAME(1)=10H(P(F))-\$ SLYNAME(2)=4H(P)\$		VIPRF	1767
	ILINE1(1)=10H(POUNDIFY SILINE1(2)=10HLAYER PSD) \$ILINE1(3)=1H\$		VIPRF	1768

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      J=10*(F(1)*F(1))+3*F(5)*F(5)*F(5)

1770      450  TWOBPF=2.*BPF*FLXPF*(PI-ATAN2(TWOBPF*(XPF**APFHI),1.-XPF*XPF)
      DO 460 II=1,NPTS
      K=II $X1=FRFQ(II) $IF(X1,GE,FMINPF) GO TO 463
      Y1=Y1/FZPF
1775      X1=PF*FRFQ+20.*ALOG10((PI-ATAN2(TWOBPF*(X1**APFHI),1.-X1*X1))/FLXPF)
      460  DBTL(II)=X1
      463  L=1
      DO 465 IT=X,NPTS
      L=L+1 $X1=FRFQ(II) $FSEL(L)=X1 $X1=X1/FZPF
      Y1=PF*FRFQ+20.*ALOG10((PI-ATAN2(TWOBPF*(X1**APFHI),1.-X1*X1))/FLXPF)
      465  DBTL(II)=X1

1785      IF(IFLITE,NE,ISANPL) GO TO 465

      FRC=FMAXPF
1790      467  FRC=FRQ+CONST*FRC $IF(FRC,GT,FMAXPF) GO TO 472
      L=L+1 $FSEL(L)=FRC
      GO TO 467

1795      472  CALL CNCFUN(FSEL,DBTL,L,PFMDR,0.,BPF,0.,XPF,0.,FZPF,0.,APFHI,
      1FMINPF,FMAXPF,DBMIN,C,IFIRST,J,M,1H,2WHI)

      IF(INOPLT,EQ,IBLANK) GO TO 475
1800      CALL ENOPL(IPLCT) $GO TO 473

      *****
      *                                     *
      *      S(F)                         *
      *                                     *
      *****

1805      461  IPHASE=0 $IF(INOPLT,EQ,IBLANK) GO TO 457
      IPHASE=1 $II=5H S(F)
      IF(IFLITE,EQ,IFURPT,AND,SPTEO,LT,SDELTA) GO TO 450
      IF(IFLITE,EQ,ITURP) GO TO 450
1810      PRINT 458,II,IX,SPLO,BPF,SPHI, SXLO,XPF, SXHI, SF7LO,FZPF, SFZHI, SABC,
      1APFHI,SAHI,PFMDR,SPFAK
      458  FORMAT(1H1,*PARAMETERS*,3X,*P(F)*,8X,A10/27X,A2/
      1RX,*P=*,11X,G12.3/8X,*X'=*,G11.3,G12.3/
      2PX,*X=*,11X,G12.3/8X,*Y'=*,G11.3,G12.3/8X,*F=*,11X,G12.5/9X,*Q'/
      3RX,*F'=*,G11.5,G12.5/8X,*Q*/4X,*ALPHA=*,11X,G12.3/4X,*ALPHA'=*,
      4G11.3,G12.3/2X,*MAX.VAL.=*,G11.4,G12.4)
      M=4HROTH $GO TO 452

1815      451  PRINT 451,II,IX,BPF,SPHI,XPF, SXHI, FZPF, SFZHI, APFHI, SAHI, PFMDR,
      1SPFAK
      451  FORMAT(1H1,*PARAMETERS*,3X,*P(F)*,8X,A10/27X,A2/
      1FX,*E'=*,G11.3,G12.3/8X,*X'=*,G11.3,G12.3/
      2PX,*F'=*,G11.4,G12.4/4X,*ALPHA'=*,G11.3,G12.3/

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PROGRAM VIPRF		74/74	CPT=1	FTN 4,5+414	08/16/77	13.11.28
1825	32X,*MAX,VAL,=*,G11.4,G12.4)				VIPRF	1826
	M=2HHT				VIPRF	1827
					VIPRF	1828
	457 K=7H 2(F) 9L=54 P(F)				VIPRF	1829
1830	PRINT 790,II,K,IPLANK				VIPRF	1830
	PRINT 461,II,K,L,IPLANK				VIPRF	1831
	461 FORMAT(14=,3X,*FREQUENCY(47.)*,9X,A5,10X,A10,11X,A5,12X,A10)				VIPRF	1832
	PRINT 455,IX,IPLANK,IX				VIPRF	1833
	455 FORMAT(25X,A2,15X,A2,17X,A2)				VIPRF	1834
1835	457 CALL XFFFUN(FREQ,DPSPL,NPTS,SPEAK,SXLO,SXHI,SBLO,SBHI,				VIPRF	1835
	1SFZLO,SFZHI,SALO,SAHI,M)				VIPRF	1836
	DO 457 K=1,NPTS				VIPRF	1837
1840	IF(DPSPL(K).LT.C.) DPSPL(K)=0.				VIPRF	1838
	457 CONTINUE				VIPRF	1839
					VIPRF	1840
	CALL TWOFUN(FREQ,DPSPL,DPSL,NPTS,FMINGF,FMAXGF,DBMIN,FYVAL)				VIPRF	1841
1845	IF(INCPLT.EQ.IPLANK) GO TO 475				VIPRF	1842
					VIPRF	1843
	K=2HHT				VIPRF	1844
1850	IF(IFLITS.EQ.IBUFT.AND.SRTED.LT.SDELTA) GO TO 456				VIPRF	1845
	IF(IFLITS.EQ.ITURD) GO TO 456				VIPRF	1846
	K=4HRECTH				VIPRF	1847
	IF(SFZLO.LT.FMINGF) GO TO 456				VIPRF	1848
	FLX1=ATAN2(2.*SPLC*(SXLO**SALO),1.-SXLO*SXLO)				VIPRF	1849
1855	IF(FLX1.LT.0.) FLX1=FLX1+2.*PI				VIPRF	1850
	Y1=SPEAK+20.*ALOG10(PI/(2.*FLX1)) SX2=SFZLO/FZPF				VIPRF	1851
	Y2=PEMCR+20.*ALOG10((PI-ATAN2(TWOORF*(X2**APFHI),1.-X2*Y2))/FLXPF)				VIPRF	1852
	YVAL=X1+X2 9CALL CURVF(SFZLO,YVAL,1,1)				VIPRF	1853
1860	456 FLX1=PI-ATAN2(2.*SBHI*(SXHI**SAHI),1.-SXHI*SXHI)				VIPRF	1854
	X1=SPEAK+20.*ALOG10(PI/(2.*FLX1)) SX2=SFZHI/FZPF				VIPRF	1855
	Y2=PEMCR+20.*ALOG10((PI-ATAN2(TWOORF*(X2**APFHI),1.-Y2*Y2))/FLXPF)				VIPRF	1856
	YVAL=X1+X2 9CALL CURVF(SFZHI,YVAL,1,1)				VIPRF	1857
1865	CALL HEIGHT(HITE1)				VIPRF	1858
	CALL LOCORXA(SPLO,SBHI,SXLO,SXHI,SFZLO,SFZHI,SALO,SAHI,FMINGF,				VIPRF	1859
	1FMAXGF,YVAL,DYVAL,K)				VIPRF	1860
	CALL ENDPL(IPLCT)				VIPRF	1861
1870					VIPRF	1862
					VIPRF	1863
					VIPRF	1864
					VIPRF	1865
					VIPRF	1866
					VIPRF	1867
					VIPRF	1868
					VIPRF	1869
					VIPRF	1870
					VIPRF	1871
					VIPRF	1872
					VIPRF	1873
					VIPRF	1874
1875					VIPRF	1875
					VIPRF	1876
					VIPRF	1877
					VIPRF	1878
					VIPRF	1879
	477 IPLCT=IPLCT+1				VIPRF	1880
1880	LYNAME(1)=10H(H)((F())) 3LYNAME(2)=FH-C(3)				VIPRF	1881
	ILINE1(1)=10H(HIGH FREQ ILINE1(2)=10H(UENCY TRAM				VIPRF	1882



PROGRAM	VIPRF	74/74	CPT=1	FTN 4.5+414	08/16/77	13.11.28
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1885	ILINE1(3)=1CHSFER FUNCT \$ ILINE1(4)=5HION)\$	VIPRF	1883
	ITITL1(1)=1CH(PRIMARY S \$ ITITL1(2)=1CHTRUCTURE-F	VIPRF	1884
	ITITL1(3)=9HUSELLAGE)\$	VIPRF	1885
	II=1GH(H())F())=\$ \$J=9H H(F) DB.	VIPRF	1886
		VIPRF	1887
		VIPRF	1888
	475 K=0 \$CONST=0.07 \$FRQ=FMINHF \$FMAX=XHFLO*\$FZHFO \$L=0	VIPRF	1889
1890	480 K=K+1 \$FSPL(K)=FRQ	VIPRF	1890
	FRQ=FRQ+CONST*FRQ \$IF(FRQ.LT.FMAX) GO TO 480	VIPRF	1891
	IF(L.FC.1) GO TO 505	VIPRF	1892
	L=1 \$FRQ=FMAX \$FMAX=FMAXHF	VIPRF	1893
	Y1=XHFHI*\$FHFHI \$IF(FRQ.EQ.X1) GO TO 480	VIPRF	1894
1895	K=K+1 \$FSPL(K)=FRQ \$FRQ=X1 \$GO TO 480	VIPRF	1895
		VIPRF	1896
		VIPRF	1897
	505 CALL CNEFUN(FSPL,DBSPL,K,XHFQOR,BHFLO,BHFHI,XHFLO,XHFHI,FZHFO,	VIPRF	1898
	1FZHFI,AFHLO,AFHFI,FMINHF,FMAXHF,DBMIN,C,IFIRST,II,J,1H,4HECTH)	VIPRF	1899
		VIPRF	1900
1900	IPHASE=1 \$IF(INOPLT.NE.IBLANK) GO TO 508	VIPRF	1901
	IF(CATGRY.EQ.C19) GO TO 507	VIPRF	1902
	IPHASE=0 \$GO TO 520	VIPRF	1903
		VIPRF	1904
		VIPRF	1905
1905	508 YVAL=1.10*\$FMINHF \$CALL HEIGHT(HITE1)	VIPRF	1906
	DYVAL=1.5*HITE*YSTEP \$YVAL=DBMIN+YSTEP+1.5*DYVAL	VIPRF	1907
	CALL FLMESS(" (W) =S",+100,XVAL,YVAL)	VIPRF	1908
	CALL FLREAL(W5,+2,"ABUT","ABUT")	VIPRF	1909
	CALL FLMESS(" DSE.S",+100,"ABUT","ABUT")	VIPRF	1910
1910	CALL FLMESS(" S \$",+100,XVAL,YVAL-0.5*DYVAL)	VIPRF	1911
		VIPRF	1912
	CALL FLMESS(" (P) =S",+100,XVAL,YVAL-1.5*DYVAL)	VIPRF	1913
	CALL FLREAL(R5,+1,"ABUT","ABUT")	VIPRF	1914
	CALL FLMESS(" IN.S",+100,"ABUT","ABUT")	VIPRF	1915
1915	CALL FLMESS(" S \$",+100,XVAL,YVAL-2.0*DYVAL)	VIPRF	1916
	CALL FLMESS(" (W) =S",+100,XVAL,YVAL-3.0*DYVAL)	VIPRF	1917
	CALL FLREAL(W5,+1,"ABUT","ABUT")	VIPRF	1918
	CALL FLMESS(" LRS.S",+100,"ABUT","ABUT")	VIPRF	1919
	CALL HEIGHT(0.7*HITE1)	VIPRF	1920
1920	CALL FLMESS(" (D) S",+100,XVAL,YVAL-7.5*DYVAL)	VIPRF	1921
	CALL HEIGHT(HITE1)	VIPRF	1922
	CALL FFSFT("BASALF") \$CALL FLMESS(IFLITE,10,XVAL,YVAL-4.5*DYVAL)	VIPRF	1923
	CALL BASALF("L/OSTD")	VIPRF	1924
	CALL HEIGHT(HITE)	VIPRF	1925
1925	CALL ENDFL(IPLCT)	VIPRF	1926
		VIPRF	1927
		VIPRF	1928
		VIPRF	1929
1930	*****	VIPRF	1930
	* C(F) *	VIPRF	1931
	* *	VIPRF	1932
	*****	VIPRF	1933
		VIPRF	1934
		VIPRF	1935
1935	707 IPLOT=IPLOT+1	VIPRF	1936
		VIPRF	1937
	LYNAME(1)=1CH(G())F())-D \$LYNAME(2)=1CH(R)()RE.1	VIPRF	1938
	LYNAME(3)=1CH (G.S)C./C \$LYNAME(4)=7FH)7())*	VIPRF	1939



PROGRAM	VIPRF	74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
ILINE1(1)=10H(RESPONSE \$ILINE1(2)=10HOF PRIMARY	VIPRF	1940				
ILINE1(3)=10H STRUCTURE \$ILINE1(4)=2H)\$	VIPRF	1941				
ITITL1(1)=2H \$ \$YSTFO=5.0	VIPRF	1942				
	VIPRF	1943				
PRINT 246 \$PRINT 353,IFLANE,IFLITE	VIPRF	1944				
	VIPRF	1945				
IF(F2N.NE.0.) GO TO 514	VIPRF	1946				
PRINT 509	VIPRF	1947				
509 FORMAT(1H-,4X,*PARAMETERS*,3X,*P(F)*,5X,*L(F)*,5X,*M(F)*,5X*H(F)*)	VIPRF	1948				
II=1HF \$K=2HF*	VIPRF	1949				
PRINT 511,II,BLFLO,BMFLO,BHFLO	VIPRF	1950				
511 FORMAT(9X,44,F18.3,3F9.3)	VIPRF	1951				
PRINT 512,K,BPF,BLFHI,BMFHI,BHFHI	VIPRF	1952				
512 FORMAT(9X,44,5F9.7)	VIPRF	1953				
II=1HX \$K=2HX*	VIPRF	1954				
PRINT 511,II,XLFLO,XMFLO,XHFLO	VIPRF	1955				
PRINT 512,K,XPF,XLFHI,XMFHI,XHFHI	VIPRF	1956				
II=1HF \$K=2HF* \$L=1HC	VIPRF	1957				
PRINT 511,II,FZLFLO,FZMFLO,FZHFL0	VIPRF	1958				
PRINT 513,L	VIPRF	1959				
513 FORMAT(1CX,A1)	VIPRF	1960				
PRINT 512,K,FZFF,FZLFHI,FZMFHI,FZHFI	VIPRF	1961				
PRINT 513,L	VIPRF	1962				
II=1HA \$K=2HA*	VIPRF	1963				
PRINT 511,II,ALFLO,AMFLO,AHFLO	VIPRF	1964				
PRINT 512,K,APFHI,ALFHI,AMFHI,AHFHI	VIPRF	1965				
II=4HMAX.	VIPRF	1966				
PRINT 512,II,PFMDR,XLFCOR,XMFCOR,XHFCOR	VIPRF	1967				
GO TO 514	VIPRF	1968				
	VIPRF	1969				
	VIPRF	1970				
514 PRINT 521	VIPRF	1971				
521 FORMAT(1H-,4X,*PARAMETERS*,3X,*P(F)*,5X,*L(F)*,5X,*L (F)*,5X,	VIPRF	1972				
1*M(F)*,5X,*H(F)*/*7X,*2*)	VIPRF	1973				
II=1HF \$K=2HF*	VIPRF	1974				
PRINT 511,II,BLFLO,BL2FLO,BMFLO,BHFLO	VIPRF	1975				
PRINT 512,K,BPF,BLFHI,BL2FHI,BMFHI,BHFHI	VIPRF	1976				
II=1HX \$K=2HX*	VIPRF	1977				
PRINT 511,II,XLFLO,XL2FLO,XMFLO,XHFLO	VIPRF	1978				
PRINT 512,K,XPF,XLFHI,XL2FHI,XMFHI,XHFHI	VIPRF	1979				
II=1HF \$K=2HF* \$L=1HC	VIPRF	1980				
PRINT 511,II,FZLFLO,FL2FLO,FZMFLO,FZHFL0	VIPRF	1981				
PRINT 513,L	VIPRF	1982				
PRINT 512,K,FZFF,FZLFHI,FL2FHI,FZMFHI,FZHFI	VIPRF	1983				
PRINT 513,L	VIPRF	1984				
II=1HA \$K=2HA*	VIPRF	1985				
PRINT 511,II,ALFLO,AL2FLO,AMFLO,AHFLO	VIPRF	1986				
PRINT 512,K,APFHI,ALFHI,AL2FHI,AMFHI,AHFHI	VIPRF	1987				
II=4HMAX.	VIPRF	1988				
PRINT 512,II,PFMDR,XLFCOR,XL2FCR,XMFCOR,XHFCOR	VIPRF	1989				
	VIPRF	1990				
514 II=5H P(F) \$K=5H L-M-H(F) \$L=5H G(F) \$M=10H G SQ./HZ.	VIPRF	1991				
PRINT 790,II,K,L \$PRINT 461,II,K,L,M \$PRINT 455,IX,IBLANK,IBLANK	VIPRF	1992				
	VIPRF	1993				
	VIPRF	1994				
520 CALL TWOFUN(FREQ,CBEL,DECBEL,NPTS,FMINGF,FMAXGF,DBMIN,DYVAL)	VIPRF	1995				
	VIPRF	1996				

PROGRAM VIPRF		74/74	OPT=1	FTN 4,5+414	08/16/77	13.11.28
		IF(CATGRY.NE.C10) GO TO 774			VIPRF	1997
		CALL ENOPL(IPLCT) \$GO TO 860			VIPRF	1998
					VIPRF	1999
2000		774 IPHASE=0 \$IF(INOPLT.EQ.IPLANK) GO TO 775			VIPRF	2000
		IPHASE=1 \$CALL ENOPL(IPLCT)			VIPRF	2001
					VIPRF	2002
					VIPRF	2003
					VIPRF	2004
					VIPRF	2005
2005		* Y(F)			VIPRF	2006
		* *			VIPRF	2007
		*****			VIPRF	2008
		IPLCT=IPLCT+1			VIPRF	2009
		LYNAME(1)=10H(Y(F))-D \$LYNAME(2)=10H(R)RE.1.0 \$LYNAME(3)=4H()			VIPRF	2010
2010		ILINE1(1)=10H(TRANSFER \$ILINE1(2)=10HFUNCTION F \$ILINE1(3)=4HOR)			VIPRF	2011
					VIPRF	2012
		DO 774 II=1,7			VIPRF	2013
		774 ITITL1(II)=ILINE2(II)			VIPRF	2014
					VIPRF	2015
2015		II=10H(Y(F))=\$ \$K=10H Y (F) DB. \$YSTEP=5.0			VIPRF	2016
		X1=CATGRY \$IF(CATGRY.EQ.C4A) X1=2H3A			VIPRF	2017
		IF(CATGRY.EQ.C4B) X1=2H33			VIPRF	2018
					VIPRF	2019
					VIPRF	2020
2020		774 IF(CATGRY.NE.C6) GO TO 785			VIPRF	2021
					VIPRF	2022
		DO 780 II=1,NPTS			VIPRF	2023
		780 DPFL(II)=0.			VIPRF	2024
		GO TO 787			VIPRF	2025
2025					VIPRF	2026
					VIPRF	2027
		785 CALL CNFFUN(FREQ,DPFL,NPTS,PEAK,BLO,BHI,XLC,XHI,FZLO,FZHI,ALC,AHI,			VIPRF	2028
		1FMINGF,FMAXGF,DBMIN,1,IFIRST,II,K,X1,4HROTH)			VIPRF	2029
					VIPRF	2030
2030		787 IPHASE=1 \$IF(INOPLT.NE.IPLANK) GO TO 788			VIPRF	2031
		IF(CATGRY.NE.C4A.AND.CATGRY.NE.C4B) GO TO 789			VIPRF	2032
		IPHASE=0 \$GO TO 860			VIPRF	2033
					VIPRF	2034
		789 CALL ENOPL(IPLCT)			VIPRF	2035
2035					VIPRF	2036
					VIPRF	2037
					VIPRF	2038
					VIPRF	2039
		* R(F)			VIPRF	2040
2040		* *			VIPRF	2041
		*****			VIPRF	2042
		782 IPLCT=IPLCT+1			VIPRF	2043
		PRINT 246 \$PRINT 353,IPLANE,IPLITE			VIPRF	2044
		II=6H Y (F) \$K=7H G(F) \$L=5H R(F) \$M=10H G SQ./HZ.			VIPRF	2045
2045		PRINT 790,II,K,L			VIPRF	2046
		790 FORMAT(1H=,*VALUES CALCULATED FOR FUNCTIONS: *,7A10)			VIPRF	2047
		PRINT 461,II,K,L,M			VIPRF	2048
					VIPRF	2049
		II=2H3A \$IF(CATGRY.EQ.C4A) GO TO 793			VIPRF	2050
2050		II=2H3B \$IF(CATGRY.EQ.C4B) GO TO 793			VIPRF	2051
		PRINT 455,CATGRY,IPLANK,IPLANK			VIPRF	2052
		GO TO 795			VIPRF	2053

PROGRAM VIPRF		7474	OPT=1	FTN 4.5+414	08/16/77	13.11.28
		793	PRINT 45F,II,IPLANK,IPLANK		VIPRF	2054
2055					VIPRF	2055
		795	LYNAME(1)=10H(R())F())-D 3LYNAME(2)=10H(B)()RF.1		VIPRF	2056
			LYNAME(3)=10H (G.S)G./() 3LYNAME(4)=7HH)7())\$		VIPRF	2057
			ILINE1(1)=10H(RESPONSE \$ILINE1(2)=10HOF THE AIR		VIPRF	2058
2060			ILINE1(3)=10HCRAFT FOUR 3ILINE1(4)=7HPMENT)\$		VIPRF	2059
			ITITL1(1)=2H \$		VIPRF	2060
					VIPRF	2061
		800	CALL TWOFUN(FREQ,DPFL,DECPFL,NPTS,FMINGF,FMAXGF,DBMIN,DYVAL)		VIPRF	2062
2065					VIPRF	2063
			IF(CATGRY.EQ.C4A.OR.CATGRY.EQ.C4B) GO TO 805		VIPRF	2064
			CALL ENDPL(IPLCT) \$GO TO 860		VIPRF	2065
		805	LYNAME(2)=10H(P)()RF.1		VIPRF	2066
			LYNAME(3)=10H (G.S)G./() 3LYNAME(4)=7HH)Z())\$		VIPRF	2067
2070			IF(INCFLT.EQ.IPLANK) GO TO 810		VIPRF	2068
			CALL ENDPL(IPLCT)		VIPRF	2069
					VIPRF	2070
					VIPRF	2071
					VIPRF	2072
					VIPRF	2073
					VIPRF	2074
2075	C		*****		VIPRF	2075
	C	*	*		VIPRF	2076
	C	*	Y(F)	*	VIPRF	2077
	C	*	1A	*	VIPRF	2078
	C	*	*	*	VIPRF	2079
2080	C		*****		VIPRF	2080
					VIPRF	2081
			IPLCT=IPLCT+1		VIPRF	2082
					VIPRF	2083
2085			LYNAME(1)=10H(Y())F())-D		VIPRF	2084
			ILINE1(1)=10H(TRANSFER 3ILINE1(2)=10HFUNCTION F \$ILINE1(3)=4HOR)*		VIPRF	2085
					VIPRF	2086
			ITITL1(1)=10H(EQUIPMENT \$ITITL1(2)=10H MOUNTED O		VIPRF	2087
			ITITL1(3)=10HN PRIMARY \$ITITL1(4)=10HSTRUCTURE		VIPRF	2088
2090			ITITL1(5)=10HTHROUGH IS \$ITITL1(6)=9HOLATORS)*		VIPRF	2089
			II=10H(Y())F())=\$ SK=10H Y (F) DB. \$YSTEP=5.0 \$L=2H1A		VIPRF	2090
					VIPRF	2091
		910	CALL ONEFUN(FREQ,DPFL,NPTS,C1AMXC,C1APLO,C1APHI,C1AXLO,C1AXHI,		VIPRF	2092
			1C1AFZL,C1AFZH,C1AALO,C1AAHI,FMINGF,FMAXGF,DBMIN,1,IFIRST,II,K,L,		VIPRF	2093
2095			24HPOTH)		VIPRF	2094
					VIPRF	2095
			IF(INCFLT.NE.IPLANK) CALL ENDPL(IPLCT)		VIPRF	2096
					VIPRF	2097
					VIPRF	2098
					VIPRF	2099
2100	C		*****		VIPRF	2100
	C	*	*	*	VIPRF	2101
	C	*	A(F)	*	VIPRF	2102
	C	*	*	*	VIPRF	2103
	C		*****		VIPRF	2104
2105			IPLCT=IPLCT+1		VIPRF	2105
			IPHASE=1		VIPRF	2106
			PRINT 246 PRINT 353,IPLANE,IPLITE		VIPRF	2107
			II=6H Y (F) \$J=8H R (F) SK=6H A (F) \$M=10H G SQ./H7.		VIPRF	2108
			L=2H3A \$IF(CATGRY.EQ.C4B) L=2H3B		VIPRF	2109
					VIPRF	2110

PROGRAM	VIPRF	74/74	CPT=1	FTN 4.5+414	08/16/77	13.11.28
2110	PRINT 791,II,J,K SPRINT 461,II,J,K,M				VIPRF	2111
	M=2H1A SPRINT 455,M,L,CATGRY				VIPRF	2112
					VIPRF	2113
	LYNAME(1)=10H(A(1)F(1))-D				VIPRF	2114
2115	ILINE1(1)=10H(INPUT TO SILINE1(2)=10HTHE AIRCRA				VIPRF	2115
	ILINE1(3)=10HFT EQUIPM SILINE1(4)=4HNT) :				VIPRF	2116
					VIPRF	2117
	ITITL1(1)=10H(EQUIPMENT SITITL1(2)=10H MOUNTED T				VIPRF	2118
	ITITL1(3)=10HROUGH ISC SITITL1(4)=10HLATORS ON				VIPRF	2119
2120	IF (CATGRY.EQ.C43) GO TO 820				VIPRF	2120
					VIPRF	2121
					VIPRF	2122
	ITITL1(5)=10HISOLATED S SITITL1(6)=10HHELE OR RA				VIPRF	2123
	ITITL1(7)=4HCK) :				VIPRF	2124
2125	GO TO 940				VIPRF	2125
2126					VIPRF	2126
	920 ITITL1(5)=10HNON-ISOL.S SITITL1(6)=10HHELE OR RA				VIPRF	2127
	ITITL1(7)=4HCK) :				VIPRF	2128
					VIPRF	2129
2130	340 CALL TROFJA(FRFQ,DREL,DECREFL,NPTS,FMINGE,FMAXGE,DRMIN,DYVAL)				VIPRF	2130
					VIPRF	2131
					VIPRF	2132
	CALL FADFL(IPLCT)				VIPRF	2133
2135					VIPRF	2134
					VIPRF	2135
	960 IF (JFLITE.EQ.ISANCL.OR.ICK.EQ.1) GO TO 1000				VIPRF	2136
	IFLITE=JFLITE IICK=1 *GO TO 3				VIPRF	2137
					VIPRF	2138
	1000 CONTINUE				VIPRF	2139
2140	IF (IFEROP.EQ.4) GO TO 890				VIPRF	2140
	IF (IFEROP.EQ.7) GO TO 1				VIPRF	2141
	IPLANE(1)=IHOLD(1) SIPLANE(2)=IHOLD(2)				VIPRF	2142
	IPLANE(3)=IHOLD(3) SIPLANE(4)=IHOLD(4)				VIPRF	2143
2145	INCPLE=IHOLD(5)				VIPRF	2144
	GO TO 31				VIPRF	2145
					VIPRF	2146
					VIPRF	2147
	990 CALL DCHFL				VIPRF	2148
					VIPRF	2149
2150					VIPRF	2150
	PRINT 900				VIPRF	2151
	900 FORMAT(1H1,45X,*AVERAGE*,23X,*AVERAGE*,8X,*SPEED*,9X,*AVERAGE*,				VIPRF	2152
	16X,*AV.KINEMATIC*/31Y,*AVERAGE*,7X,*PRESSURE*,7X,*AVERAGE*,				VIPRF	2153
	29X,*DENSITY*,10X,*CF*,9X,*KINEMATIC*,7X,*VISCOSITY*/				VIPRF	2154
2155	715Y,*ALTITUDE*,7X,*PRESSURE*,6X,*NORMALIZED*,6X,*DENSITY*,				VIPRF	2155
	48Y,*NORMALIZED*,6X,*SOUND*,8X,*VISCOSITY*,7X,*NORMALIZED*)				VIPRF	2156
	DO 010 I=1,61				VIPRF	2157
	FNORM=AVF(I)/AVP(1) SNORM=AVDENS(I)/AVDENS(1)				VIPRF	2158
	VNORM=VISCOS(I)/VISCOS(1)				VIPRF	2159
2160	910 PRINT 920,ALTUD(I),AVP(I),PNORM,AVDENS(I),DNORM,SOUND(I),				VIPRF	2160
	1VISCOS(I),VNORM				VIPRF	2161
	920 FORMAT(F22.2,F15.1,F15.4,F15.7,F15.4,F15.1,F15.7,F15.4)				VIPRF	2162
	STOP				VIPRF	2163
	END				VIPRF	2164
					VIPRF	2165







PROGRAM VIPPE			74/74	OPT=1	FTN 4.5+414		08/16/77	13.11.28
VARIABLES	SN	TYP	RELOCATION					
26744	C3BEM	REAL			24757	C3BX	REAL	ARRAY
26003	C3BYN	REAL	ARRAY		25015	C3FMYX	REAL	ARRAY
24675	C3WE	REAL	ARRAY		13743	C4A	REAL	
13744	C4D	REAL			13741	C5	REAL	
26702	C5AHT	REAL			20701	C5ALO	REAL	
20676	C5PHI	REAL			20675	C5ELC	REAL	
26703	C5FN	REAL			20704	C5MAX	REAL	
26701	C5YHT	REAL			20677	C5XLC	REAL	
13745	C6	REAL			21013	D	REAL	
24160	D	REAL	ARRAY		21562	DBFL	REAL	ARRAY
24123	DEMERS	REAL	ARRAY		21076	DEMIN	REAL	
12	DEMORI	REAL	ARRAY	KARDS	160	DEMOD2	REAL	ARRAY KARDS
23746	DEDS	REAL	ARRAY		22010	DFSPL	REAL	ARRAY
23432	DE1A10	REAL	ARRAY		23310	DB1A7D	REAL	ARRAY
22704	DE1F15	REAL	ARRAY		23026	DB1F16	REAL	ARRAY
22562	DE1F4	REAL	ARRAY		23166	DB1111	REAL	ARRAY
23503	DE2A10	REAL	ARRAY		23361	DB2A7D	REAL	ARRAY
22755	DE2F15	REAL	ARRAY		23115	DB2F16	REAL	ARRAY
22633	DE2F4	REAL	ARRAY		23237	DB2111	REAL	ARRAY
22504	DE2VAL	REAL	ARRAY		21334	DECBEL	REAL	ARRAY
13727	DELDDP	REAL			21022	DELRS	REAL	
20775	DELTA0	REAL			20774	DELTAZ	REAL	
21031	DELW0	REAL			21032	DELWS	REAL	
20750	DE	REAL			21105	DNCRM	REAL	
13723	DXF1V	REAL			13721	DXF100	REAL	
13725	DXF0K	REAL			13715	DXC1A	REAL	
13714	DXMERS	REAL			11	DXMOD1	REAL	KARDS
157	DXMOD2	REAL		KARDS	14002	DX1A10	REAL	
13776	DX1A7D	REAL			13762	DX1F15	REAL	
13766	DX1F16	REAL			13756	DX1F4	REAL	
13772	DX1111	REAL			14004	DX2A10	REAL	
14000	DX2A7D	REAL			13764	DX2F15	REAL	
13770	DX2F16	REAL			13760	DX2F4	REAL	
13774	DX2111	REAL			21100	DYVAL	REAL	
21060	EC	REAL			20752	ECCAT1	REAL	
20753	ECCAT2	REAL			7	ECMOVE	REAL	KARDS
21017	ECS	REAL			24174	FLX	REAL	ARRAY
21075	FLY05	REAL			21101	FLX1	REAL	
21054	FL2FHI	REAL			21053	FL2FLO	REAL	
21072	FMAX	REAL			20502	FMAXGF	REAL	
20600	FMAXHF	REAL			20575	FMAXPF	REAL	
20615	FMEHT	REAL			20514	FMELC	REAL	
20601	FMINCF	REAL			20577	FMINHF	REAL	
20575	FMINPF	REAL			0	FN	REAL	KARDS
23673	FFBIHF	REAL	ARRAY		21106	FFFO	REAL	ARRAY
21020	FFO	REAL			22236	FFEL	REAL	ARRAY
24200	F7	REAL	ARRAY		21023	F7HFHI	REAL	
21025	F7HFLO	REAL			21071	F7HI	REAL	
21066	F7LFHT	REAL			21043	F7LFLO	REAL	
21070	F7LO	REAL			21035	F7MFHI	REAL	
21036	F7MFLO	REAL			20776	F7PF	REAL	
2	F2N	REAL		KARDS	0	H	REAL	PPLOTT
24204	H1LO	REAL	ARRAY		45	H1TE	REAL	PPLOTT
46	H1TE1	REAL		PPLOTT	20503	HMAX	REAL	
20745	I	INTEGER			13732	IALUM	INTEGER	
13753	IA1	INTEGER			13752	IA7D	INTEGER	
57	IFLANK	INTEGER		PPLOTT	375	IPUFET	INTEGER	KARDS

PROGRAM VIP2F			74/74	OPT=1	FTN 4.5+414		08/16/77	13.11.28
VAPIAEFS	SN	TYPE	RELOCATION					
20761	ICM	INTEGER			20755	IERRCR	INTEGER	
21077	IFIRST	INTEGER			6	IFLITE	INTEGER	PPLOTT
20763	IFM	INTEGER			341	IFNISH	INTEGER	KARDS
13751	IF111	INTEGER			13747	IF15	INTEGER	
13750	IF15	INTEGER			13746	IF4	INTEGER	
22555	IFOLD	INTEGER	ARRAY		20757	II	INTEGER	
337	ILAND	INTEGER		KARDS	10	ILINE1	INTEGER	ARRAY PPLCTT
324	ILINT2	INTEGER	ARRAY	KARDS	13733	IMAG	INTEGER	
56	INOPLT	INTEGER		PPLOTT	55	IPHA5E	INTEGER	PPLOTT
26	IELANE	INTEGER	ARRAY	PPLOTT	20607	IPLOT	INTEGER	
334	ISANDL	INTEGER		KARDS	13730	ISTEEL	INTEGER	
336	ITAKOF	INTEGER		KARDS	13731	ITITAN	INTEGER	
17	ITITL1	INTEGER	ARRAY	PPLOTT	340	ITURP	INTEGER	KARDS
20762	IX	INTEGER			20760	J	INTEGER	
20746	JFLITE	INTEGER			21041	K	INTEGER	
21042	L	INTEGER			31	LXNAME	INTEGER	ARRAY PPLCTT
75	LYNAME	INTEGER	ARRAY	PPLOTT	20755	M	INTEGER	
20754	MATERL	INTEGER			13712	NEF7PF	INTEGER	
13715	NC1A	INTEGER			20737	NC3	INTEGER	
13726	NFOR	INTEGER			13713	NMFRS	INTEGER	
10	NMODE1	INTEGER		KARDS	156	NMODE2	INTEGER	KARDS
21073	NETS	INTEGER			20574	NRSVAL	INTEGER	
13722	NWE1K	INTEGER			13720	NWE100	INTEGER	
13724	NWE5K	INTEGER			14001	N1A10	INTEGER	
13775	N1A70	INTEGER			13771	N1F111	INTEGER	
13761	N1F15	INTEGER			13765	N1F16	INTEGER	
13755	N1F4	INTEGER			14003	N2A10	INTEGER	
13777	N2A70	INTEGER			13773	N2F111	INTEGER	
13763	N2F15	INTEGER			13767	N2F16	INTEGER	
13757	N2F4	INTEGER			21061	PEAK	REAL	
21000	PEM	REAL			21001	PFMOB	REAL	
13754	PI	REAL			21104	PNCRM	REAL	
20772	QSO	REAL			20766	R	REAL	
20773	PEX	REAL			20767	RMORM	REAL	
3	PS	REAL		PPLOTT	20604	RSMAK	REAL	
24021	REVALS	REAL	ARRAY		21010	SAHI	REAL	
21007	SALO	REAL			21006	SPHI	REAL	
21021	SFLO	REAL			21014	SRTFO	REAL	
21011	SFCLTA	REAL			21015	SFZHI	REAL	
21012	SF7LO	REAL			24210	SIGN	REAL	ARRAY
24507	SCUND	REAL	ARRAY		21016	SPEAK	REAL	
21005	SXHI	REAL			21004	SXLO	REAL	
20751	T	REAL			20722	TAKAHI	REAL	
20721	TAKALO	REAL			20716	TAKPHI	REAL	
20715	TAKPLO	REAL			20723	TAKMAX	REAL	
20720	TAKYHI	REAL			20717	TAKXLO	REAL	
20734	TEAHI	REAL			20733	TREHI	REAL	
20735	TEFO	REAL			20736	TREF	REAL	
47	TICLEN	REAL		PPLCTT	24170	TWOB	REAL	ARRAY
21074	TWOBOF	REAL			20771	U	REAL	
20764	V	REAL			23572	VALK	REAL	ARRAY
24600	VISCOS	REAL	ARRAY		20770	VNCRM	REAL	
4	WE	REAL		PPLCTT	23554	WEK	REAL	ARRAY
20605	WEMAX	REAL			24074	WE100	REAL	ARRAY
24103	WE1000	REAL	ARRAY		24112	WF5000	REAL	ARRAY
5	WS	REAL		PPLCTT	2	Y	REAL	PPLCTT
44	XAXIS	REAL		PPLCTT	5	XBT	REAL	KARDS

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PROGRAM VPRF      74/74  OPT=1      ITN 4.5+414      08/16/77  13.11.28

VARIABLES      SN  TYPE      RELOCATION
41  XCYCLE      REAL      PPLOTT      20747  XL      REAL
24164  XFCMY      REAL      APRAY      21073  XHFCCR      REAL
21027  XFFHT      REAL      21026  XFFLC      REAL
21003  XFFMAY      REAL      21063  YHI      REAL
13717  XINC14      REAL      21040  XLFCCR      REAL
21050  XLFHT      REAL      21047  XLFLO      REAL
1  XLFMAX      REAL      KARDS      21062  XLC      REAL
21052  XL2FCCR      REAL      20540  XL2FHI      REAL
20637  XL2FLC      REAL      3  XL2FMX      REAL      KARDS
1  XMAKNG      REAL      PPLOTT      21036  XMFCCR      REAL
20621  XMFHI      REAL      20520  XMFLC      REAL
21002  XMFMAX      REAL      20506  XPF      REAL
5  XTL      REAL      KARDS      21103  XVAL      REAL
54  XY      REAL      PPLOTT      20525  XXHFHI      REAL
20624  XXHFLO      REAL      20513  XXLFHI      REAL
20612  XXLFLO      REAL      50  X1      REAL      PPLOTT
51  X2      REAL      PPLOTT      52  X3      REAL      PPLOTT
57  X6      REAL      PPLOTT      43  YAXIS      REAL      PPLOTT
42  YSTEP      REAL      21102  YVAL      REAL

FILE NAMES      MODE
0  INPUT      FMT      2041  OUTPUT      FMT      4102  FILE      0  TAPES      FMT

EXTERNALS      TYPE      ARCS
ALOG10      REAL      1  LIBRARY      ATAN2      REAL      2  LIBRARY
BASALF      1      DELTA      0
COMPRS      0      CURVE      4
DCHEPL      0      FNCPL      1
ECF      REAL      1      GPCINTS      17
HEIGHT      1      LOCFLYA      13
MARKTR      1      MIXALF      1
ONEFUN      21      OHAD      6
PEANODES      17      PLSET      1
RLMESS      4      PLREAL      4
TRFPLIA      8      TWOFUN      8
XFERFUN      13      YAXANG      1
YJNTAX      0

INLINE FUNCTIONS      TYPE      ARCS
AFS      REAL      1  INTRIN      AMOD      REAL      2  INTRIN

STATEMENT LABELS
6337  1      14703  2      FMT      7141  3
6445  4      14753  5      FMT      14665  6      FMT
7120  7      14767  8      FMT      6501  9
6513  10      6577  11      7177  12
7212  13      6525  14      14014  15      FMT
14273  16      FMT      0  17      6552  18
6564  19      6414  20      7017  21
7222  22      6575  23      14360  24      FMT
14030  25      FMT      6417  26      6464  27
7100  28      14183  29      FMT      7031  30
6346  31      7045  32      14054  33      FMT
7227  34      7057  35      14072  36      FMT
14110  37      FMT      14124  38      FMT      14147  39      FMT
6422  40      6455  41      0  42
6425  43      7241  44      7264  45

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PROGRAM VIPRF

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## STATEMENT LABELS

6430	46		6435	47		6433	48	
6637	50		14416	52	FMT	6664	54	
6710	56		6734	58		6676	60	
6746	62		6722	64		6760	66	
6772	68		7004	70		6612	74	
6624	76		7132	78		7320	90	
7340	92		7346	94		7354	96	
7357	100		15060	205	FMT	15104	210	FMT
15156	220	FMT	15164	225	FMT	15246	230	FMT
15255	235	FMT	7463	239		15333	240	FMT
15353	245	FMT	15735	246	FMT	7510	247	
7524	250		15433	251	FMT	7563	252	
7676	253		15523	254	FMT	15617	255	FMT
7622	256		7723	257		15670	260	FMT
7731	260			310		7760	315	
7766	320		10015	321		10022	322	
10005	323		10027	325		10043	330	
10050	335		10055	340		10063	350	
10101	351		15454	352	FMT	15737	353	FMT
16054	354	FMT	15770	355	FMT	10136	356	
10150	370		10116	375		16101	380	FMT
16154	382	FMT	15751	383	FMT	16231	385	FMT
10205	387		10321	389		16344	390	FMT
10267	393		10233	395		10357	398	
10367	405		10373	410		10432	415	
16734	420	FMT	16771	425	FMT	10747	427	
10460	431		10514	433		10642	435	
10757	436		11027	437		17006	438	FMT
16577	439	FMT	11036	440		17017	441	FMT
10556	442		10574	443		10605	444	
10667	446		10704	447		10615	448	
10722	449		11506	450		17162	451	FMT
11512	452			453		17234	455	FMT
11606	456		11522	457		17111	458	FMT
11365	459			460		17220	461	FMT
11421	463			465		11467	466	
11451	467		11460	472		11647	473	
11671	475		11677	480		11716	505	
12044	507		11726	508		17252	509	FMT
17271	511	FMT	17304	512	FMT	17341	513	FMT
12135	514		12200	518		12213	520	
17411	521	FMT	11265	580		11320	590	
11074	600		17030	605	FMT	11162	610	
11200	620		11206	625		11235	630	
11251	640			770		12222	774	
12265	775			780		12276	785	
12300	787		12311	788		12313	789	
17611	790	FMT	12342	793		12344	795	
12361	800		12372	805		12427	810	
12507	820		12513	840		12517	860	
12544	860		17700	900	FMT		910	
17751	920	FMT	12526	1000				

LOCOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
6360		* I	775 775	100	EXT REFS
6460	42	I	825 826	78	INSTACK
7060	1000	* I	944 2139	34510	EXT REFS NCT INNER

PROGRAM MIPDF					74774	OPT=1	FTN 4.5+414		08/16/77	13.11.28
LCODES	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES					
7144	17	II	980 982	48	INSTACK					
7752	710	* J	1250 1233	67	INSTACK EXITS					
11376	465	* II	1772 1776	233	EXT REFS EXITS					
11423	465	* IT	1778 1782	239	EXT REFS					
11527	453	K	1839 1841	38	INSTACK					
12245	770	II	2010 2013	38	INSTACK					
12272	780	II	2022 2023	27	INSTACK					
12550	910	* I	2157 2160	239	EXT REFS					
COMMON BLOCKS		LENGTH								
PFLOTT		48								
KARDS		225								
STATISTICS										
PROGRAM LENGTH			170178	7695						
BUFFER LENGTH			61440	3172						
OF LABELED COMMON LENGTH			4228	274						



SUBROUTINE REACCS		74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
1	SUBROUTINE REACCS(ZFN,ZLFMAX,ZF2N,ZL2FMX,ZBUFMX,ZXBT,ZXTL, 1ZFOMOV,NOMOD1,DXM1,DBM1,NOMOD2,DXM2,DBM2,ITYPCK,ICRAFT,IERROR)				VIPRF	2166
					VIPRF	2167
					VIPRF	2168
	COMMON/KAPCS/FK,YLFMAX,F2N,XL2FMX,BUFMAX,XBT,XTL,FCMOVE, 1NMODE1,DXMOD1,DBMOD1(100),NMODE2,DXMOD2,DBMOD2(100), 2ILINE2(8),ISANFL,IRUFET,ITAKOF,ILAND,ITURF,IFNISH				VIPRF	2169
					VIPRF	2170
					VIPRF	2171
					VIPRF	2172
	DIMENSION DBM1(1),DBM2(1),IDATA(8)				VIPRF	2173
					VIPRF	2174
10	DATA IBLANK/1H /				VIPRF	2175
	IERROR=0				VIPRF	2176
					VIPRF	2177
					VIPRF	2178
	*****				VIPRF	2179
15	* * READ INPUT DATA CARD 4 * *****				VIPRF	2180
					VIPRF	2181
					VIPRF	2182
					VIPRF	2183
	READ(5,20) ILIN2				VIPRF	2184
20	20 FORMAT(A10)				VIPRF	2185
					VIPRF	2186
					VIPRF	2187
	C CHECK WHETHER "END-OF-JOB" CARD WAS READ				VIPRF	2188
					VIPRF	2189
25	IF(EOF(5).EQ.0) GO TO 110				VIPRF	2190
					VIPRF	2191
	PRINT 40				VIPRF	2192
	40 FORMAT(1H-,29X,*THE END-OF-JOB CARD WAS ENCOUNTERED INSTEAD OF THE 1 EXPECTED*)				VIPRF	2193
	PRINT 43				VIPRF	2194
30	43 FORMAT(29X,*PROFILE PARAMETERS-SPECIAL VALUES CARD.*)				VIPRF	2195
					VIPRF	2196
	IF(ITYPCK.EQ.1) GO TO 50				VIPRF	2197
					VIPRF	2198
					VIPRF	2199
35	PRINT 45				VIPRF	2200
	45 FORMAT(29X,*PROGRAM EXECUTION STOPS BECAUSE*)				VIPRF	2201
	PRINT 47				VIPRF	2202
	47 FORMAT(29X,*INPUT DATA VALUES ARE NOT STORED IN THE PROGRAM FOR THE 16 SPECIFIED TYPE OF AIRCRAFT*/29X,*VALUES ARE STORED ONLY FOR THE 2 TYPES F-4,F-15,F-16,F-111,A-10 AND A-70 AIRCRAFT.*)				VIPRF	2203
40	CALL CONEFL				VIPRF	2204
	STOP				VIPRF	2205
					VIPRF	2206
					VIPRF	2207
					VIPRF	2208
	50 IERROR=4 *PRINT 60				VIPRF	2209
45	60 FORMAT(				VIPRF	2210
	11H-,29X, *PROGRAM EXECUTION PROCEEDS ASSUMING THAT A PLANK "PROF				VIPRF	2211
	11L PARAMETERS-SPECIAL VALUES" CARD*/29X,*THEN A "FINISH" CARD SHO				VIPRF	2212
	21L HAVE FOLLOWED THE "AIRCRAFT PARAMETERS" CARD.*)				VIPRF	2213
					VIPRF	2214
50	65 FK=ZFN *YLFMAX=ZLFMAX *F2N=ZF2N *XL2FMX=ZL2FMX *BUFMX=ZBUFMX XBT=ZXBT *XTL=ZXTL *FCMOVE=ZFCMOV				VIPRF	2215
	PRINT 67,FN,YLFMAX,F2N,XL2FMX,BUFMAX,XBT,XTL,FCMOVE				VIPRF	2216
	67 FORMAT(1H-,29X,*PROFILE PARAMETERS-SPECIAL VALUES,INPUT DATA VALUE 16 STORED IN PROGRAM*/29X,A10.1)				VIPRF	2217
55					VIPRF	2218
					VIPRF	2219
	70 NMODE1=NOMOD1 *DXMOD1=DXM1				VIPRF	2220
	DO 80 I=1,NMODE1				VIPRF	2221
					VIPRF	2222

SUBROUTINE READPCS		74/76	OPT=1	FTN 4.5+414	08/16/77	13.11.28
	80 DBMOC1(I)=DBM1(I)				VIPRF	2223
	J=6HFIRST 3PRINT 85,J,NMODE1,DXMOD1,(DBMOC1(I),I=1,NMODE1)				VIPRF	2224
60	87 FORMAT(1H-,28X,46,* BENDING MODE VALUES,INPUT DATA VALUES STORED I				VIPRF	2225
	1N PROGRAM*/29X,I2,13F6.2/(29X,13F6.2))				VIPRF	2226
					VIPRF	2227
	91 IF(F2N.NF,0.) GO TO 120				VIPRF	2228
65					VIPRF	2229
	PRINT 92				VIPRF	2230
	92 FORMAT(1H-,28X,*SECOND BENDING MODE VALUES WILL NOT BE USED IN PRO				VIPRF	2231
	GRAM CALCULATIONS*/29X,*BECAUSE F =0.*/38X,*2N*)				VIPRF	2232
	RETURN				VIPRF	2233
70					VIPRF	2234
	107 NMODE2=NMODE2 \$DXMOD2=DXM2				VIPRF	2235
	DO 105 I=1,NMODE2				VIPRF	2236
	107 DBMOC2(I)=DBM2(I)				VIPRF	2237
					VIPRF	2238
75	J=6HSECOND 3PRINT 85,J,NMODE2,DXMOD2,(DBMOC2(I),I=1,NMODE2)				VIPRF	2239
					VIPRF	2240
	RETURN				VIPRF	2241
					VIPRF	2242
					VIPRF	2243
80	0 CHECK WHETHER "FINISH" CARD WAS READ				VIPRF	2244
					VIPRF	2245
	110 IF(ILINE2(1).NE.IFINISH) GO TO 160				VIPRF	2246
					VIPRF	2247
	PRINT 120				VIPRF	2248
85	120 FORMAT(1H-,28X,*THE "FINISH" CARD WAS ENCOUNTERED INSTEAD OF THE F				VIPRF	2249
	1XEXPECTED*)				VIPRF	2250
	PRINT 43				VIPRF	2251
					VIPRF	2252
	IF(ITVCK.EQ.1) GO TO 140				VIPRF	2253
90					VIPRF	2254
	IFERROR=1 3PRINT 130				VIPRF	2255
	130 FORMAT(29X,*THE PROGRAM PROCEEDS TO THE NEXT SET,IF ANY,OF INPUT F				VIPRF	2256
	1AT3 CARDS BECAUSE*)				VIPRF	2257
	PRINT 47 \$RETURN				VIPRF	2258
95					VIPRF	2259
	140 PRINT 60 \$GO TO 65				VIPRF	2260
					VIPRF	2261
					VIPRF	2262
	0 CHECK WHETHER "DESCRIPTION" CARD WAS READ				VIPRF	2263
100					VIPRF	2264
	160 I=ILINE2(4) \$IF(I.NE.ISANDL.AND.I.NE.IPUFFY.AND.I.NE.ITAKCF.AND.				VIPRF	2265
	1I.NE.ILAND.AND.I.NE.ITURB) GO TO 203				VIPRF	2266
					VIPRF	2267
	PRINT 180				VIPRF	2268
105	180 FORMAT(1H-,28X,*THE CARD SHOWN BELOW APPARENTLY IS A "DESCRIPTION"				VIPRF	2269
	1 CARD*/29X,*WHICH WAS ENCOUNTERED INSTEAD OF THE EXPECTED*)				VIPRF	2270
	PRINT 43				VIPRF	2271
	PRINT 185,ILINE2				VIPRF	2272
	185 FORMAT(1H-,28X,\$A10)				VIPRF	2273
110					VIPRF	2274
	IF(ITVCK.EQ.1) GO TO 210				VIPRF	2275
					VIPRF	2276
	IFERROR=2				VIPRF	2277
	PRINT 190				VIPRF	2278
					VIPRF	2279

SUBROUTINE READDCS 74/74 OPT=1

FTN 4.5+414

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115	190 FORMAT(1H-,28X,*IT IS ASSUMED THAT THIS APPARENT "DESCRIPTION" CAR	VIPRF	2280
	10*/29X,*BELONGS TO THE NEXT SET,IF ANY,OF INPUT DATA CARDS.*/	VIPRF	2281
	229X,*AND THE PROGRAM PROCEEDS TO THIS SET.*/	VIPRF	2282
	RETURN	VIPRF	2283
		VIPRF	2284
120	210 IERROR=3 \$PRINT 60 \$PRINT 200	VIPRF	2285
	200 FORMAT(29X,*IT ALSO IS ASSUMED THAT THIS APPARENT "DESCRIPTION" CA	VIPRF	2286
	10*/29X,*BELONGS TO THE NEXT SET,IF ANY, OF INPUT DATA CARDS.*/	VIPRF	2287
	GO TO 65	VIPRF	2288
		VIPRF	2289
125	C CHECK VALUE IN CARD COLUMNS 75-80	VIPRF	2290
		VIPRF	2291
	203 ENCODE(10,205,I) ILINE2(8)	VIPRF	2292
	205 FORMAT(R6)	VIPRF	2293
130	DECODE(10,207,I) YFCMOV	VIPRF	2294
	207 FORMAT(F6.2)	VIPRF	2295
	IF(YFCMOV.GE.0.) GO TO 220	VIPRF	2296
		VIPRF	2297
		VIPRF	2298
		VIPRF	2299
135	C CARD IS ASSUMED TO BE CARD 1 OF THE SET OF 1ST BENDING MODE VAL. C	VIPRF	2300
	PRINT 217	VIPRF	2301
	217 FORMAT(1H-,28X,*THE CARD SHOWN BELOW APPARENTLY IS CARD 1 OF THE S	VIPRF	2302
	10*/29X,*1ST BENDING MODE VALUE CARDS INSTEAD OF THE EXPECTED*)	VIPRF	2303
140	PRINT 43 \$PRINT 185,ILINE2	VIPRF	2304
		VIPRF	2305
	IF(ITYPECK.EQ.1) GO TO 213	VIPRF	2306
		VIPRF	2307
	PRINT 45 \$PRINT 47	VIPRF	2308
145	CALL DCNPL \$STOP	VIPRF	2309
		VIPRF	2310
		VIPRF	2311
	213 PRINT 215	VIPRF	2312
	215 FORMAT(1H-,28X,*PROGRAM EXECUTION PROCEEDS ASSUMING THAT A BLANK "	VIPRF	2313
150	10*/29X,*PROFILE PARAMETERS-SPECIAL VALUES" CARD*/29X,*SHOULD HAVE PRECEDE	VIPRF	2314
	20 THIS CARD.*/	VIPRF	2315
		VIPRF	2316
	FN=ZF1 \$XLFMAX=ZLFMAX \$F2N=ZF2N \$XL2FMX=ZL2FMX \$BUFMX=ZBUFMX	VIPRF	2317
	XBT=ZXBET \$XTL=ZXTL \$FCMOVE=ZFCMOV	VIPRF	2318
		VIPRF	2319
155	PRINT 260,FN,XLFMAX,F2N,XL2FMX,BUFMAX,XBT,XTL,FCMOVE	VIPRF	2320
		VIPRF	2321
	NCARDS=1 \$AMODE=5HFIRST \$IMODCK=1	VIPRF	2322
	GO TO 570	VIPRF	2323
		VIPRF	2324
160	C CARD IS ASSUMED TO BE THE "PROFILE PARAMETERS-SPECIAL VALUES" CARD	VIPRF	2325
		VIPRF	2326
	227 IF(ITYPECK.EQ.1) GO TO 230	VIPRF	2327
		VIPRF	2328
		VIPRF	2329
165	DECODE(80,225,ILINE2) FN,XLFMAX,F2N,XL2FMX,BUFMAX,XBT,XTL,FCMOVE	VIPRF	2330
	225 FORMAT(RF11.3)	VIPRF	2331
	PRINT 227,ILINE2	VIPRF	2332
	227 FORMAT(1H-,28X,*PROFILE PARAMETERS-SPECIAL VALUES CARD*/29X,8A10)	VIPRF	2333
	GO TO 230	VIPRF	2334
170		VIPRF	2335
	230 FN=ZF1 \$XLFMAX=ZLFMAX \$F2N=ZF2N \$XL2FMX=ZL2FMX \$BUFMX=ZBUFMX	VIPRF	2336

	SLBROUTINE READCDS	74/74	OPT=1	FTN 4,5+414	08/16/77	13.11.28
	XRT=YXRT \$XTL=ZXTL \$FCMOVE=ZFCMOV				VIPRF	2337
	J=1H				VIPRF	2338
175	DO 240 I=1,8				VIPRF	2339
	IF(ILINE2(I),NF,1) GO TO 270				VIPRF	2340
	240 CONTINUE				VIPRF	2341
					VIPRF	2342
180	PPRINT 260,FN,XLEMAX,F2N,XL2FMX,BUFMAX,XRT,XTL,FCMOVE				VIPRF	2343
	260 FORMAT(1H0,29X,*PROFILE PARAMETERS-SPECIAL VALUES CARD,INPUT DATA				VIPRF	2344
	1VALUES STORED IN PROGRAM(A BLANK CARD WAS READ)*/				VIPRF	2345
	229X,8F10.1)				VIPRF	2346
185	GO TO 298				VIPRF	2347
					VIPRF	2348
					VIPRF	2349
					VIPRF	2350
					VIPRF	2351
					VIPRF	2352
	27 DECODE(80,225,ILINE2) YFN,YLEMAX,YF2N,YL2FMX,YBUFMAX,YXRT,YXTL,				VIPRF	2353
	1YFCMCV				VIPRF	2354
190					VIPRF	2355
	J=9H *				VIPRF	2356
	DO 277 I=1,8				VIPRF	2357
	277 IDATA(I)=1H				VIPRF	2358
					VIPRF	2359
					VIPRF	2360
195	IF(YFN,EO,0.) GO TO 290				VIPRF	2361
	FN=YFN \$IDATA(1)=J				VIPRF	2362
	280 IF(YLEMAX,EO,0.) GO TO 282				VIPRF	2363
	XLEMAX=YLEMAX \$IDATA(2)=J				VIPRF	2364
	282 IF(YF2N,EO,0.) GO TO 284				VIPRF	2365
200	F2N=YF2N \$IDATA(3)=J				VIPRF	2366
	284 IF(YL2FMX,EO,0.) GO TO 286				VIPRF	2367
	XL2FMX=YL2FMX \$IDATA(4)=J				VIPRF	2368
	286 IF(YBUFMAX,EO,0.) GO TO 288				VIPRF	2369
	BUFMAX=YBUFMAX \$IDATA(5)=J				VIPRF	2370
205	288 IF(YXRT,EO,0.) GO TO 290				VIPRF	2371
	XRT=YXRT \$IDATA(6)=J				VIPRF	2372
	290 IF(YXTL,EO,0.) GO TO 292				VIPRF	2373
	XTL=YXTL \$IDATA(7)=J				VIPRF	2374
210	292 IF(YFCMCV,EO,0.) GO TO 294				VIPRF	2375
	FCMCV=YFCMCV \$IDATA(8)=J				VIPRF	2376
					VIPRF	2377
	294 PRINT 296,FN,XLEMAX,F2N,XL2FMX,BUFMAX,XRT,XTL,FCMOVE,IDATA				VIPRF	2378
	296 FORMAT(1H-,29X,*PROFILE PARAMETERS-SPECIAL VALUES CARD,INPUT DATA				VIPRF	2379
215	1VALUES READ FROM CARD OR STORED IN PROGRAM*/ 29X,8F10.1/29X,8A10/				VIPRF	2380
	229X,32H* INDICATES VALUE READ FROM CARD )				VIPRF	2381
					VIPRF	2382
					VIPRF	2383
	298 NCARDS=1 \$NMODE=FHFIRST \$IMODCK=1				VIPRF	2384
220					VIPRF	2385
	C *****				VIPRF	2386
	C *				VIPRF	2387
	C READ FIRST CARD IN SET				VIPRF	2388
	C OF PENDING MODE VALUE CARDS				VIPRF	2389
225	C *				VIPRF	2390
	C *****				VIPRF	2391
					VIPRF	2392
	300 READ(F,20) ILINE2				VIPRF	2393



SUBROUTINE REARCS 74/74 OPT=1

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230	C	CHECK WHETHER "END-OF-JOB" CARD WAS READ	VIPRF	2394
		IF (ECF(5),EQ,1) GO TO 430	VIPRF	2395
			VIPRF	2396
			VIPRF	2397
			VIPRF	2398
			VIPRF	2399
235		IF (ECF(5),EQ,1) GO TO 430	VIPRF	2400
		IF (IMCECK,EQ,2) GO TO 350	VIPRF	2401
			VIPRF	2402
		PRINT 310,NCARDS,NMODE	VIPRF	2403
240	310	FORMAT(29X,*CARD *,I1,* OF THE SET OF **,A6,* BENDING MODE VALUE**C 1ARDS *,2A10)	VIPRF	2404
			VIPRF	2405
		IF (ITYECK,EQ,1) GO TO 320	VIPRF	2406
			VIPRF	2407
		PRINT 45 *PRINT 47	VIPRF	2408
245		CALL DCEFL \$STOP	VIPRF	2409
			VIPRF	2410
			VIPRF	2411
	320	I=10HCR THE FIN \$J=8HISH CARD \$PRINT 330,I,J	VIPRF	2412
	330	FORMAT(29X,*A10)	VIPRF	2413
		PRINT 340 *PRINT 47	VIPRF	2414
250	340	FORMAT(1H*,28X,*PROGRAM EXECUTION PROCEEDS ASSUMING THAT THE "FINI 1SH" CARD FOLLOWED THE*/29X,8A10)	VIPRF	2415
		GO TO 70	VIPRF	2416
			VIPRF	2417
			VIPRF	2418
			VIPRF	2419
255	350	IF (F2N,NE,1) GO TO 380	VIPRF	2420
			VIPRF	2421
		I=10HFINISH CAR \$J=1HD \$PRINT 330,I,J	VIPRF	2422
		PRINT 360	VIPRF	2423
260	360	FORMAT(29X,*PROGRAM EXECUTION PROCEEDS ASSUMING THAT THE "FINISH" 1CARD SHOULD HAVE FOLLOWED*)	VIPRF	2424
		PRINT 370	VIPRF	2425
			VIPRF	2426
	370	FORMAT(29X,*THE DEFECTING SET OF BENDING MODE VALUE CARDS.*)	VIPRF	2427
		PRINT 92	VIPRF	2428
		RETURN	VIPRF	2429
265			VIPRF	2430
	380	IF (ITYECK,EQ,1) GO TO 320	VIPRF	2431
			VIPRF	2432
		PRINT 45 *PRINT 47	VIPRF	2433
		CALL DCEFL \$STOP	VIPRF	2434
270			VIPRF	2435
	390	I=10HCR THE FIN \$J=8HISH CARD \$PRINT 310,NCARDS,NMODE,I,J	VIPRF	2436
		PRINT 360 *PRINT 370	VIPRF	2437
		GO TO 90	VIPRF	2438
			VIPRF	2439
275			VIPRF	2440
		CHECK WHETHER "FINISH" CARD WAS READ	VIPRF	2441
			VIPRF	2442
	430	IF (JLINE2(1),NE,IFNISH) GO TO 450	VIPRF	2443
			VIPRF	2444
280		IF (IMCECK,EQ,2) GO TO 440	VIPRF	2445
			VIPRF	2446
		IF (ITYECK,EQ,1) GO TO 70	VIPRF	2447
			VIPRF	2448
		IF (ECF(5),EQ,1)	VIPRF	2449
285		PRINT 120 *PRINT 310,NCARDS,NMODE	VIPRF	2450



SUBROUTINE READPCS      74/74      OPT=1		FIN 4,5+414	08/16/77	13.11.28
	PRINT 47 \$PRINT 43F	VIPRF	2451	
43	FORMAT(29X,*THE PROGRAM PROCEEDS TO THE NEXT SET,IF ANY,OF DATA CA	VIPRF	2452	
	1PCS,*)	VIPRF	2453	
	RETURN	VIPRF	2454	
260		VIPRF	2455	
		VIPRF	2456	
	44) IF(ITYPECK.EQ.1) GO TO 33	VIPRF	2457	
		VIPRF	2458	
	IF(F2N.EQ.0.) RETURN	VIPRF	2459	
265		VIPRF	2460	
	IFERROR=1	VIPRF	2461	
	PRINT 120 \$PRINT 310,NCARDS,NMODE	VIPRF	2462	
	PRINT 47 \$PRINT 43F	VIPRF	2463	
	RETURN	VIPRF	2464	
310		VIPRF	2465	
		VIPRF	2466	
	CHECK WHETHER "DESCRIPTION" CARD WAS READ	VIPRF	2467	
		VIPRF	2468	
	45) I=ILINE2(4) \$IF(I.NE.ISANDL.AND.I.NE.IPUFET.AND.I.NE.ITAKOF.AND.	VIPRF	2469	
315	1I.NE.ILAND.AND.I.NE.ITURD) GO TO 540	VIPRF	2470	
		VIPRF	2471	
	PRINT 190	VIPRF	2472	
		VIPRF	2473	
	IF(IMCHECK.EQ.2) GO TO 470	VIPRF	2474	
318		VIPRF	2475	
	IF(ITYPECK.EQ.1) GO TO 460	VIPRF	2476	
		VIPRF	2477	
	IFERROR=2 \$PRINT 310,NCARDS,NMODE	VIPRF	2478	
	PRINT 185,ILINE2 \$PRINT 47 \$PRINT 190	VIPRF	2479	
319	RETURN	VIPRF	2480	
		VIPRF	2481	
	46) IFERROR=3	VIPRF	2482	
	I=10CHC9 THE FIN 3J=8HISH CARD \$PRINT 310,NCARDS,NMODE,I,J	VIPRF	2483	
	PRINT 185,ILINE2 \$PRINT 340 \$PRINT 43 \$PRINT 230	VIPRF	2484	
320	GO TO 70	VIPRF	2485	
		VIPRF	2486	
		VIPRF	2487	
	47) IFERROR=7 \$IF(ITYPECK.EQ.1) GO TO 500	VIPRF	2488	
		VIPRF	2489	
325	IF(F2N.NE.0.) GO TO 490	VIPRF	2490	
		VIPRF	2491	
	I=10CHFIMISH CAR 3J=1HD \$PRINT 330,I,J	VIPRF	2492	
	PRINT 350 \$PRINT 370	VIPRF	2493	
	PRINT 92 \$PRINT 280	VIPRF	2494	
330	RETURN	VIPRF	2495	
		VIPRF	2496	
	49) IFERROR=2	VIPRF	2497	
	PRINT 310,NCARDS,NMODE	VIPRF	2498	
	PRINT 185,ILINE2 \$PRINT 47 \$PRINT 495	VIPRF	2499	
335	40) FORMAT(29X,*PROGRAM EXECUTION PROCEEDS ASSUMING THAT THIS APPARENT	VIPRF	2500	
	1 "DESCRIPTION" CARD*/29X,*3BELONGS TO THE NEXT SET,IF ANY,OF INPUT	VIPRF	2501	
	2 DATA CARDS.)*	VIPRF	2502	
	RETURN	VIPRF	2503	
		VIPRF	2504	
340	50) I=10CHC9 THE FIN 3J=8HISH CARD \$PRINT 310,NCARDS,NMODE,I,J	VIPRF	2505	
	PRINT 185,ILINE2 \$PRINT 360 \$PRINT 370 \$PRINT 200	VIPRF	2506	
	GO TO 60	VIPRF	2507	

SUBROUTINE READCDS      74/74      CPT=1		FTN 4,5+414	08/16/77	13.11.28
345	54. DO 543 I=1,8		VIPRF	2508
	IF(ILINE2(I).NE.IPLANK) GO TO 570		VIPRF	2509
	543 CONTINUE		VIPRF	2510
			VIPRF	2511
			VIPRF	2512
			VIPRF	2513
350	C    A PLANK CARD WAS READ		VIPRF	2514
	IF(ITYPCK.EQ.1) GO TO 553		VIPRF	2515
			VIPRF	2516
	IF(IMCCK.EQ.2) GO TO 547		VIPRF	2517
			VIPRF	2518
355	PRINT 545		VIPRF	2519
	545 FORMAT(1H-,2AX,*A PLANK CARD WAS READ INSTEAD OF THE EXPECTED*)		VIPRF	2520
	PRINT 310,NCARDS,NMODE \$PRINT 45 \$PRINT 47		VIPRF	2521
	CALL CONEPL \$STOP		VIPRF	2522
			VIPRF	2523
360	547 IF(F2N.NE.0.) GO TO 550		VIPRF	2524
	PRINT 92		VIPRF	2525
	RETURN		VIPRF	2526
			VIPRF	2527
365	550 PRINT 546		VIPRF	2528
	I=10HOF THE FIN \$J=4H15H CARD \$PRINT 310,NCARDS,NMODE,I,J		VIPRF	2529
	PRINT 45 \$PRINT 47		VIPRF	2530
	CALL CONEPL \$STOP		VIPRF	2531
			VIPRF	2532
370			VIPRF	2533
	553 IF(IMCCK.EQ.2) GO TO 557		VIPRF	2534
			VIPRF	2535
	NMODE1=NCMOD1 \$DXMOD1=DXM1		VIPRF	2536
375	DO 555 I=1,NMODE1		VIPRF	2537
	555 DPMOD1(I)=DPM1(I)		VIPRF	2538
			VIPRF	2539
	J=FIRST \$PRINT 95,J,NMODE1,DXMOD1,(DPMOD1(I),I=1,NMODE1)		VIPRF	2540
	GO TO 510		VIPRF	2541
			VIPRF	2542
380	557 IF(F2N.NE.0.) GO TO 563		VIPRF	2543
	PRINT 92		VIPRF	2544
	RETURN		VIPRF	2545
			VIPRF	2546
385	563 NMODE2=NCMOD2 \$DXMOD2=DXM2		VIPRF	2547
	DO 565 I=1,NMODE2		VIPRF	2548
	565 DPMOD2(I)=DPM2(I)		VIPRF	2549
			VIPRF	2550
	J=SECOND \$PRINT 95,J,NMODE2,DXMOD2,(DPMOD2(I),I=1,NMODE2)		VIPRF	2551
	GO TO 820		VIPRF	2552
			VIPRF	2553
			VIPRF	2554
			VIPRF	2555
			VIPRF	2556
			VIPRF	2557
			VIPRF	2558
390	C    CARD IS ASSUMED TO BE CARD 1 OF THE SET OF 1ST BENDING MODE VALUE		VIPRF	2559
	570 IF(IMCCK.EQ.2) GO TO 575		VIPRF	2560
			VIPRF	2561
	RECODE (R,545,ILINE2) NMODE1,DXMOD1,(DPMOD1(I),I=1,12)		VIPRF	2562
	NVALS=NCMOD1 \$GO TO 540		VIPRF	2563
			VIPRF	2564

SLOPROUTINE REARDCS		74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
400	575 RECODE (R0,F80,ILINE2) NMODE2,DXMOD2,(DRMOD2(I),I=1,12)				VIPRF	2565
	580 FORMAT(I2,13F6.2)				VIPRF	2566
	NVALS=NMODE2				VIPRF	2567
					VIPRF	2568
405	590 PRINT 600,NMODE,ILINE2				VIPRF	2569
	600 FORMAT(140,28X,A6,* BENDING MODE VALUE CARDS*/29X,8A10)				VIPRF	2570
	IF(NVALS.LT.12) GO TO 602				VIPRF	2571
					VIPRF	2572
	J=13 *K=2F IL=0 *IF(K,LT,NVALS) GO TO 620				VIPRF	2573
410	K=NVALS IL=1				VIPRF	2574
					VIPRF	2575
					VIPRF	2576
	C *****				VIPRF	2577
	C *				VIPRF	2578
415	READ 2ND AND SUCCEEDING				VIPRF	2579
	BENDING MODE VALUE CARDS				VIPRF	2580
	C *				VIPRF	2581
	C *****				VIPRF	2582
					VIPRF	2583
					VIPRF	2584
420	620 NCARDS=NCARDS+1				VIPRF	2585
	READ(C,20) ILINE2				VIPRF	2586
					VIPRF	2587
					VIPRF	2588
	C CHECK WHETHER "END-OF-JOB" CARD WAS READ				VIPRF	2589
425	IF(EOF(E),EQ.0) GO TO 650				VIPRF	2590
					VIPRF	2591
	PRINT 40 *PRINT 310,NCARDS,NMODE				VIPRF	2592
	PRINT 45 *PRINT 630,NVALS,NMODE				VIPRF	2593
430	630 FORMAT(29X,*ALL OF THE *,I3,* *,A6,* BENDING MODE VALUES COULD NOT				VIPRF	2594
	1 BE READ FROM INPUT DATA CARDS.)*				VIPRF	2595
	CALL DCEPL ISTOP				VIPRF	2596
					VIPRF	2597
					VIPRF	2598
					VIPRF	2599
435	C CHECK WHETHER "FINISH" CARD WAS READ				VIPRF	2600
					VIPRF	2601
	650 IF(ILINE2(1).NE.FINISH) GO TO 670				VIPRF	2602
					VIPRF	2603
	IFERROR=1				VIPRF	2604
440	PRINT 120 *PRINT 310,NCARDS,NMODE				VIPRF	2605
	PRINT 130 *PRINT 630,NVALS,NMODE				VIPRF	2606
	RETURN				VIPRF	2607
					VIPRF	2608
					VIPRF	2609
445	C CHECK WHETHER "DESCRIPTION" CARD WAS READ				VIPRF	2610
					VIPRF	2611
	67 I=ILINE2(4) *IF(I.NE.ISANDL.AND.I.NE.IRUFET.AND.I.NE.ITAKOF.AND.				VIPRF	2612
	1I.NE.ITAND.AND.I.NE.ITURP) GO TO 690				VIPRF	2613
					VIPRF	2614
450	IFERROR=2				VIPRF	2615
	PRINT 180 *PRINT 310,NCARDS,NMODE				VIPRF	2616
	PRINT 185,ILINE2 *PRINT 190				VIPRF	2617
	RETURN				VIPRF	2618
					VIPRF	2619
455	690 DO 700 I=1,8				VIPRF	2620
	IF(ILINE2(I).NE.IPLANK) GO TO 740				VIPRF	2621

SUBROUTINE PEABOCS    74/74    OPT=1		FTN 4.5+414	08/16/77    13.11.28
	700 CONTINUE	VIPRF	2622
		VIPRF	2623
460	C    A BLANK CARD WAS READ	VIPRF	2624
	PRINT 710	VIPRF	2625
	71. FORMAT(1H-,28X,*A BLANK CARD WAS ENCOUNTERED INSTAD OF THE EXPECT	VIPRF	2626
	1ID*)	VIPRF	2627
465	PRINT 310,NCARDS,NMODE	VIPRF	2628
	PRINT 45 \$PRINT 630,NVALS,NMODE	VIPRF	2629
	CALL DCNDEL \$STOP	VIPRF	2630
		VIPRF	2631
		VIPRF	2632
		VIPRF	2633
		VIPRF	2634
470	C    CARD IS ASSUMED TO BE A MODE VALUE CARD	VIPRF	2635
	74. IF(IMCHECK.EQ.1) DECODE(90,760,ILINE2) (DBMOD1(I),I=J,K)	VIPRF	2636
	IF(IMCHECK.EQ.2) DECODE(90,760,ILINE2) (DBMOD2(I),I=J,K)	VIPRF	2637
	76. FORMAT(13F9.2)	VIPRF	2638
475	PRINT 780,ILINE2	VIPRF	2639
	78. FORMAT(29X,PA10)	VIPRF	2640
	IF(L.IQ.1) GO TO 800	VIPRF	2641
480	J=J+13 \$K=K+13 \$IF(K.LT.NVALS) GO TO 620	VIPRF	2642
	K=NVALS \$L=1	VIPRF	2643
	GO TO 620	VIPRF	2644
		VIPRF	2645
		VIPRF	2646
485	800 IF(IMCHECK.EQ.2) GO TO 820	VIPRF	2647
	81. IMCHECK=2 \$NCARDS=1 \$NMODE=6HSECOND	VIPRF	2648
	GO TO 300	VIPRF	2649
		VIPRF	2650
490		VIPRF	2651
	C    *****	VIPRF	2652
	C    *	VIPRF	2653
	C    READ LAST CARD	VIPRF	2654
	C    IN SET OF DATA CARDS	VIPRF	2655
495	C    *	VIPRF	2656
	C    *****	VIPRF	2657
	820 READ(5,20) ILINE2	VIPRF	2658
		VIPRF	2659
500	C    CHECK WHETHER "END-OF-JOB" CARD WAS READ	VIPRF	2660
	IF(EOF(5).EQ.0) GO TO 850	VIPRF	2661
		VIPRF	2662
	IFERROR=4	VIPRF	2663
505	PRINT 40 \$I=1CHEFINISH CAR \$J=1HD \$PRINT 330,I,J \$PRINT 840	VIPRF	2664
	84. FORMAT(29X,*PROGRAM EXECUTION STOPS AFTER THE CURRENT SET OF INPUT	VIPRF	2665
	1 DATA CARDS.*)	VIPRF	2666
	RETURN	VIPRF	2667
510	C    CHECK WHETHER "FINISH" CARD WAS READ	VIPRF	2668
		VIPRF	2669
		VIPRF	2670
		VIPRF	2671
		VIPRF	2672
		VIPRF	2673
		VIPRF	2674
		VIPRF	2675
		VIPRF	2676
		VIPRF	2677
		VIPRF	2678

SUBROUTINE READCOS		74/74	CRT=1	FTN 4.F+414	08/16/77	13.11.28
E15	867	IF(ILINE2(1).NE.IFINISH) GO TO 870			VIPRF	2679
		PRINT 185,ILINE2			VIPRF	2680
		RETURN			VIPRF	2681
					VIPRF	2682
					VIPRF	2683
E20	0	CHECK WHETHER "DESCRIPTION" CARD WAS READ			VIPRF	2684
					VIPRF	2685
	87	I=ILINE2(4) 3IF(I.NE.ISANDL.AND.I.NE.ISUFET.AND.I.NE.ITAKOF.AND. 1I.NE.ILANF.AND.I.NE.ITUR9) GO TO 880			VIPRF	2686
					VIPRF	2687
					VIPRF	2688
E25		IFERROR=3			VIPRF	2689
		PRINT 181,JI=1CHEFINISH CAR EJ=1HD *PRINT 330,I,J			VIPRF	2690
		PRINT 185,ILINE2 *PRINT 495			VIPRF	2691
		RETURN			VIPRF	2692
					VIPRF	2693
E30	0	A CARD WITH UNKNOWN CONTENTS WAS READ			VIPRF	2694
					VIPRF	2695
	887	IFERROR=4			VIPRF	2696
		PRINT 501,ILINE2			VIPRF	2697
E35	901	FORMAT(1H-,'28X,'*INSTEAD OF THE EXPECTED "FINISH" CARD,THE CARD SHO 1KN BELEN WAS EXCOUNTERED AFTER THE */29X,*LAST CARD IN THE SET OF 2"SECOND PENDING MORE VALUE" CARDS.*//29X,*PROGRAM EXECUTION STOPS A 3ETER OUTPUT AND PLOTS ARE PRODUCED FOR THE CURRENT SET OF INPUT DA 4TA CARDS.*//29X,8A10)			VIPRF	2698
		RETURN			VIPRF	2699
		END			VIPRF	2700
					VIPRF	2701
					VIPRF	2702
					VIPRF	2703
					VIPRF	2704
					VIPRF	2705
					VIPRF	2706

## SYMBOLIC REFERENCE MAP (P=1)

## ENTRY POINTS

## 3 READCOS

VARIABLES	SM	TYPE	RELOCATION					
4	PIEMAX	REAL	KARDS	12	DEMOD1	REAL	ARRAY	KARDS
160	DEMOD2	REAL	ARRAY KARDS	0	DEMI	REAL	ARRAY	F.P.
0	DEMI	REAL	ARRAY F.F.	11	DEMOD1	REAL		KARDS
167	DEMOD2	REAL	KARDS	0	DEMI	REAL		F.P.
0	DEMI	REAL	F.P.	7	DEMOD1	REAL		KARDS
0	DEMI	REAL	KARDS	2	DEMI	REAL		KARDS
3045	I	INTEGER		1200	DEMOD1	INTEGER		
3075	ICRAFT	INTEGER	KARDS	0	DEMOD1	INTEGER	*UNUSED	F.P.
3065	ICRAFT	INTEGER	ARRAY KARDS	0	DEMOD1	INTEGER		F.P.
341	IFINISH	INTEGER	KARDS	337	DEMOD1	INTEGER		KARDS
324	ILINER2	INTEGER	ARRAY KARDS	3062	DEMOD1	INTEGER		
374	ISANDL	INTEGER	KARDS	336	DEMOD1	INTEGER		KARDS
360	ITUR9	INTEGER	KARDS	0	DEMOD1	INTEGER		F.P.
3066	J	INTEGER		3063	DEMOD1	INTEGER		
3064	L	INTEGER		3050	DEMOD1	INTEGER		KARDS
3051	NMOD1	INTEGER		10	DEMOD1	INTEGER		F.P.
166	NMOD2	INTEGER	KARDS	0	DEMOD1	INTEGER		
0	NMOD2	INTEGER	F.F.	3062	DEMOD1	INTEGER		



SUBROUTINE READCDS			74/74	OPT=1	FTN 4.5+414		02/16/77 13.11.28	
VARIABLES	SN	TYPE	RELOCATION					
5 XPT		REAL	KARDS		1 XLFMAX	REAL	KARDS	
3 XL2FMX		REAL	KARDS		6 XTL	REAL	KARDS	
3057 YEUFMX		REAL			3047 YFCMOV	REAL		
3053 YFN		REAL			3055 YF2N	REAL		
3054 YLFMAX		REAL			3056 YL2FMX	REAL		
3060 YXPT		REAL			3061 YYTL	REAL		
0 ZFUFMX		REAL	F.P.		0 ZFCMOV	REAL	F.P.	
0 ZFN		REAL	F.P.		0 ZF2N	REAL	F.P.	
0 ZLFMAX		REAL	F.P.		0 ZL2FMX	REAL	F.P.	
0 ZYPT		REAL	F.P.		0 ZXTL	REAL	F.P.	
FILE NAMES	MODE							
OUTPUT	FMT		TAPES	FMT				
EXTERNALS	TYPE	ARCS			EOF	REAL	1	
DCNEPL		0						
STATEMENT LABELS								
1206 20	FMT		1213 40	FMT		1227 43	FMT	
1240 45	FMT		1250 47	FMT		26 50		
1276 60	FMT		31 65			1335 67	FMT	
50 70			0 80			1357 85	FMT	
70 90			1375 92	FMT		74 100		
0 105			115 110			1424 120	FMT	
1442 130	FMT		133 140			136 160		
1464 160	FMT		1510 185	FMT		1516 190	FMT	
1506 200	FMT		172 203			1571 205	FMT	
1600 207	FMT		164 210			215 213		
1643 215	FMT		1605 217	FMT		242 220		
1712 225	FMT		1720 227	FMT		251 230		
0 240			1742 260	FMT		277 270		
0 277			314 280			317 282		
322 284			325 286			330 288		
377 290			336 292			341 294		
2017 296	FMT		343 299			346 300		
2046 310	FMT		372 320			2072 330	FMT	
2102 340	FMT		403 350			2125 360	FMT	
2142 370	FMT		417 380			427 360		
440 430			2215 435	FMT		460 440		
475 450			527 460			546 470		
570 460			2351 495	FMT		602 500		
617 540			0 543			2420 545	FMT	
642 547			646 550			662 553		
0 555			705 557			711 563		
0 565			732 570			740 575		
2524 580	FMT		744 590			2534 600	FMT	
756 620			2567 630	FMT		775 650		
1011 670			1076 690			0 700		
2644 710	FMT		1055 740			2703 760	FMT	
2711 760	FMT		1111 800			1113 810		
1117 820			2733 940	FMT		1136 860		
1143 870			1172 880			2773 900	FMT	
LCOPS	LABEL	INDX	FROM-TO	LENGTH	PROPERTIES			
57	80	I	57 59	28	INSTACK			
103	105	I	72 73	22	INSTACK			
270	240	* I	176 178	53	INSTACK	EXITS		

SUBROUTINE REARCS				74/74	OPT=1	FTN 4.5+414		08/16/77 13.11.28	
LCOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES				
305	277	I	192 193	39	INSTACK				
620	547	* I	345 347	59	INSTACK	EXITS			
677	555	I	375 376	29	INSTACK				
720	565	I	387 388	29	INSTACK				
1037	700	* I	455 457	59	INSTACK	EXITS			
COMMON BLOCKS		LENGTH							
KAPDS		226							
STATISTICS									
PROGRAM LENGTH			30759	1597					
CM LABELED COMMON LENGTH			3429	226					

SUBROUTINE ONEFUN		74/74	CPT=1	FTN 4.5+414	08/16/77	13.11.28
1	SUBROUTINE ONEFUN(FREQ,DB,N,PEAK,BLO,BHI,XLO,XHI,FZROLO,FZROHI, 1ALC,AHI,FMIN,FMAX,DBMIN,ISETZ,IFIRST,LPEAK,IFUN,ISCRPT,ILOHI) DIMENSION FREQ(1),DB(1)				VIPRF	2707
					VIPRF	2708
					VIPRF	2709
5	COMMON/PELOTT/H,XMAKNO,X,RS,WE,WS,IFLITE,CATGRY,ILINE1(7), 1ITITL1(7),IPLANE(3),LXNAME(4),LYNAME(4),XCYCLE,YSTEP,YAXIS, 2XAXIS,HITE,HITE1,TIGLEN,X1,X2,X3,X4,XX,IPHASE,INOPLT,IBLANK				VIPRF	2710
					VIPRF	2711
					VIPRF	2712
					VIPRF	2713
10	DATA IHI/2PHI/,IX/EH (C)*/				VIPRF	2714
					VIPRF	2715
					VIPRF	2716
	IF(INOPLT.EQ.IBLANK) GO TO 15				VIPRF	2717
					VIPRF	2718
	IF(ILOHI.EQ.IHI) GO TO 5				VIPRF	2719
15					VIPRF	2720
	PRINT 1,IPLANE,IFLITE,IFUN,ISCRPT,BLO,BHI,XLO,XHI,FZPOLO,FZRCHI, 1ALC,AHI,PEAK				VIPRF	2721
	1 FORMAT(1H1,8H*****3A10,1H,,A10,8H*****///* PARAMETERS OF *				VIPRF	2722
	1A5/17X,A2//8X,*B =*,G11.3/8Y,*B* =*,G11.3/				VIPRF	2723
20	2AX,*X =*,G11.3/8X,*X* =*,G11.3/8X,*F =*,G11.5/9X,*C*/				VIPRF	2724
	3BX,*F* =*,G11.5/9X,*C*/4X,*ALPHA =*,G11.3/4X,*ALPHA* =*,G11.3/				VIPRF	2725
	42X,*MAX.VAL. =*,G11.4)				VIPRF	2726
	GO TO 15				VIPRF	2727
					VIPRF	2728
25	PRINT 10,IPLANE,IFLITE,IFUN,ISCRPT,BHI,XHI,FZROHI,AHI,PEAK				VIPRF	2729
	1 FORMAT(1H1,8H*****3A10,1H,,A10,8H*****///* PARAMETERS OF *				VIPRF	2730
	1A5/17X,A2//8X,*B =*,G11.3/8X,*X* =*,F7.3/				VIPRF	2731
	2AX,*F* =*,G11.5/9X,*C*/4X,*ALPHA =*,G11.4/2X,*MAX.VAL. =*,G11.4)				VIPRF	2732
					VIPRF	2733
30					VIPRF	2734
	15 CALL XFERFUN(FREQ,DB,N,PEAK,XLO,XHI,BLO,BHI,FZROLO,FZROHI,ALC,AHI, 1ILOHI)				VIPRF	2735
					VIPRF	2736
					VIPRF	2737
35	IF(ISETZ.EQ.0) GO TO 40				VIPRF	2738
	DO 20 I=1,N				VIPRF	2739
	IF(DB(I).GE.0.) GO TO 40				VIPRF	2740
40	20 DB(I)=0.				VIPRF	2741
					VIPRF	2742
					VIPRF	2743
					VIPRF	2744
					VIPRF	2745
					VIPRF	2746
45	40 IF(INOPLT.EQ.IBLANK) RETURN				VIPRF	2747
	XAXIS=ALOG10(FMAX/FMIN)*XCYCLE				VIPRF	2748
	CALL TITL(1H,1,LXNAME,+100,LYNAME,+100,XAXIS,YAXIS)				VIPRF	2749
					VIPRF	2750
	CALL HEIGHT(HITL)				VIPRF	2751
	CALL HEADIN(ILINE1,+100,2,3)				VIPRF	2752
	CALL HEADIN(ITITL1,+100,2,7)				VIPRF	2753
	CALL FFSFT("BASALF")				VIPRF	2754
	CALL HEADIN(IPLANE,+30,2,3)				VIPRF	2755
50	CALL BASALF("L/CSTO")				VIPRF	2756
	CALL YTIKKS(5)				VIPRF	2757
					VIPRF	2758
	XX=PEAK \$CALL DBELMAX(XX,YSSTEP,DBMAX) \$DBMIN=DBMAX-40.0				VIPRF	2759
	CALL XLOG(FMIN,XCYCLE,DBMIN,YSSTEP)				VIPRF	2760
55	CALL TICKKK(TIGLEN,FMAX,YSSTEP,YAXIS,DBMIN)				VIPRF	2761
					VIPRF	2762
	IFIRST=0				VIPRF	2763

SUBROUTINE ONEFUN 74/74 OPT=1

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	DO 60 I=1,N	VIPRF	2764
	IFIRST=IFIRST+1 *IF (DR(IFIRST).GE.DEMIN) GO TO 80	VIPRF	2765
60	CONTINUE	VIPRF	2766
	80 K=0	VIPRF	2767
	DO 100 I=IFIRST,N	VIPRF	2768
	IF (DR(I).LT.DEMIN) GO TO 120	VIPRF	2769
65	100 K=K+1	VIPRF	2770
	120 CALL TABLE(FREQ(IFIRST),DR(IFIRST),K,IFUN,ISCRPT)	VIPRF	2771
	CALL CURVE(FREQ(IFIRST),DR(IFIRST),K,C)	VIPRF	2772
	CALL HEIGHT(HITE1)	VIPRF	2773
70	X1=1.10*FMIN *X2=PEAK+0.5	VIPRF	2774
	CALL RMFESS(LPEAK,+100,X1,X2)	VIPRF	2775
	CALL RLPEAL(PEAK,+1,"ABUT","ABUT")	VIPRF	2776
	CALL RMFESS(" C(3)S",+100,"ABUT","ABUT")	VIPRF	2777
75	CALL HEIGHT(C.5*HITE1)	VIPRF	2778
	CALL RMFESS(" (H)S",+100,X1,X2-0.5)	VIPRF	2779
		VIPRF	2780
		VIPRF	2781
		VIPRF	2782
		VIPRF	2783
	DYVAL=1.5*HITE*YSTEP *CALL HEIGHT(HITE1)	VIPRF	2784
80		VIPRF	2785
	Y1=3.14159265-ATAN2(2.0*PHI*(XHI**AHI),1.0-XHI*XHI)	VIPRF	2786
	YVAL=PEAK+20.0*ALOG10(3.14159265/(2.0*X1))	VIPRF	2787
	CALL CURVE(FZROHI,YVAL,1,1)	VIPRF	2788
		VIPRF	2789
85	IF (ILCHI.EQ.1HI,2F.FZROLO.LT.FMIN) GO TO 140	VIPRF	2790
		VIPRF	2791
	X1=ATAN2(2.0*ELO*(YLO**ALO),1.-XLO*XLO)	VIPRF	2792
	YVAL=PEAK+20.0*ALOG10(3.14159265/(2.0*X1))	VIPRF	2793
	CALL CURVE(FZROLO,YVAL,1,1)	VIPRF	2794
90		VIPRF	2795
	140 CALL LOCPRX1(BLO,BHI,XLO,XHI,FZROLO,FZROHI,ALC,AHI,FMIN,FMAX,	VIPRF	2796
	1YVAL,DYVAL,ILCHI)	VIPRF	2797
		VIPRF	2798
		VIPRF	2799
	YX=ALOG10(FMAX)-1.10/XC*GLE *XX=10.0**XX	VIPRF	2800
95	Y1=CFMAX-0.25*YSTEP	VIPRF	2801
	CALL PAPANS(XX,X1,DYVAL,XMAKNO,H,X,IX,RS,IFLITE,HITE,HITE1)	VIPRF	2802
		VIPRF	2803
	RETURN	VIPRF	2804
	END	VIPRF	2805

SYMBOLIC REFERENCE MAP (P=1)

ENTRY POINTS  
7 ONEFUN

VARIABLES	SN	TYPE	RELOCATION				
0 AFT		REAL	F.P.	0	ALC	REAL	F.P.
0 PHI		REAL	F.P.	0	RLC	REAL	F.P.
7 CATGPV		REAL	PPLOTT	0	DB	REAL	F.P.
675 CFMAX		REAL		0	DFMIN	REAL	F.P.

SLRPOUTINE ONEFUN

74/74

CPT=1

FTN 4.5+414

08/16/77 13.11.28

VARIABLES	SN	TYPE	RELOCATION				
677	DYVAL	REAL		0	FMAX	REAL	F.P.
0	FMIN	REAL	F.P.	0	FREQ	REAL	F.P.
0	F7ROHI	REAL	F.P.	0	FZROLO	REAL	F.P.
0	H	REAL	PPLOTT	45	HITE	REAL	PPLOTT
46	HITE1	REAL	PPLOTT	574	I	INTEGER	
57	IPLANK	INTEGER	PPLOTT	0	IFIRST	INTEGER	F.P.
6	IFLITE	INTEGER	PPLOTT	0	IFUN	INTEGER	F.P.
545	IHI	INTEGER		10	ILINE1	INTEGER	PPLOTT
0	ILOHI	INTEGER	F.P.	56	INCPLT	INTEGER	PPLOTT
55	IPHASE	INTEGER	PPLOTT	26	IPLANE	INTEGER	PPLOTT
0	ISCRPT	INTEGER	F.P.	0	ISSETZ	INTEGER	F.P.
17	ITITL1	INTEGER	ARRAY	546	IY	INTEGER	
676	K	INTEGER	PPLOTT	0	LPEAK	INTEGER	F.P.
31	LXNAME	INTEGER	ARRAY	35	LYNAME	INTEGER	PPLOTT
0	N	INTEGER	F.P.	0	PEAK	REAL	F.P.
3	RS	REAL	PPLOTT	47	TICLEN	REAL	PPLOTT
4	WE	REAL	PPLOTT	5	WS	REAL	PPLOTT
2	X	REAL	PPLOTT	44	XAXIS	REAL	PPLOTT
41	XCYCLE	REAL	PPLOTT	0	XHI	REAL	F.P.
0	XLO	REAL	F.P.	1	XMAKNO	REAL	PPLOTT
54	XX	REAL	PPLOTT	50	X1	REAL	PPLOTT
51	X2	REAL	PPLOTT	52	X3	REAL	PPLOTT
53	Y6	REAL	PPLOTT	43	YAXIS	REAL	PPLOTT
42	YSTEP	REAL	PPLOTT	700	YVAL	REAL	

FILE NAMES      MODE  
OUTPUT          FMT

EXTERNALS	TYPE	ARCS			
ALOG10	REAL	1	LIBRARY	ATAN2	REAL
BASALF		1		CURVE	2
DEELWAY		3		HEADIN	4
HEIGHT		1		LOCPRXA	13
PARAMS		11		RESET	1
PLMESS		6		PLREAL	4
TABLE		5		TICKMK	5
TITLE		8		XFERFUN	13
XLOG		4		YTICKS	1

## STATEMENT LABELS

567	1	FMT	24	5	634	10	FMT
26	15		0	20	64	40	
0	60		147	80	0	100	
161	120		302	140			

LCOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXITS
56	20	* I	36 38	68	INSTACK	EXITS
140	60	* I	58 60	78	INSTACK	EXITS
152	100	* I	63 65	78	INSTACK	EXITS

COMMON BLOCKS      LENGTH  
PPLOTT              48

## STATISTICS

PROGRAM LENGTH	10038	515
COMMON LENGTH	508	48



SUBROUTINE TWCFUN		74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
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1	SUBROUTINE TWCFUN(FREQ,DB1,DB2,N,FMIN,FMAX,DBMIN,DYVAL)	VIPRF	2806
	DIMENSION FREQ(1),DB1(1),DB2(1)	VIPRF	2807
		VIPRF	2808
	COMMON/PLOT/H,XMAKNO,X,RS,WE,WS,IFLITE,CATGRY,ILINE1(7),	VIPRF	2809
5	ITITL1(7),IPLANE(3),LXNAME(4),LYNAME(4),XCYCLE,YSTEP,YAXIS,	VIPRF	2810
	2XAXIS,HITE,HITE1,TICLEN,X1,X2,X3,X4,XX,IPHASE,INOPLT,IPLANK	VIPRF	2811
		VIPRF	2812
	DATA IX/5H (E) \$/	VIPRF	2813
		VIPRF	2814
10		VIPRF	2815
	DBMAX=-1.0E3	VIPRF	2816
	DO 10 I=1,N	VIPRF	2817
	X1=DB1(I) X2=DB2(I) X3=X1+X2 DB2(I)=X3	VIPRF	2818
	IF(X3.GT.DBMAX) DBMAX=X3 X3=10.0*(X3/10.)	VIPRF	2819
15	IF(IPHASE.EQ.1) PRINT 20,FREQ(I),X1,X2,DB2(I),X3	VIPRF	2820
	20 CONTINUE	VIPRF	2821
	20 FORMAT(6G18.5)	VIPRF	2822
		VIPRF	2823
	IF(IPHASE.EQ.0) RETURN	VIPRF	2824
20		VIPRF	2825
	DYVAL=1.5*HITE*YSTEP	VIPRF	2826
	X1=DBMAX \$CALL DBELMAX(X1,YSSTEP,DBMAX)	VIPRF	2827
	DBMIN=DBMAX-40.0 \$IF(ABS(X1-DB2(1)).LE.35.0) GO TO 30	VIPRF	2828
	YSTEP=10.0 \$DBMIN=DBMAX-80.0 \$DYVAL=2.0*DYVAL	VIPRF	2829
25		VIPRF	2830
	30 XAXIS=ALOG10(FMAX/FMIN)*XCYCLE	VIPRF	2831
	CALL TITLE(1H ,1,LYNAME,+100,LYNAME,+100,XAXIS,YAXIS)	VIPRF	2832
		VIPRF	2833
	CALL HEIGHT(HITE)	VIPRF	2834
30	CALL HEADIN(ILINE1,+100,2,3)	VIPRF	2835
	CALL HEADIN(ITITL1,+100,2,3)	VIPRF	2836
	CALL RESET("BASALF")	VIPRF	2837
	CALL HEADIN(IPLANE,+100,2,3)	VIPRF	2838
	CALL BASALF("L/CSTD")	VIPRF	2839
35	CALL YTICKS(5)	VIPRF	2840
	CALL XLOG(FMIN,XCYCLE,DBMIN,YSSTEP)	VIPRF	2841
	CALL TICKMK(TICLEN,FMAX,YSSTEP,YAXIS,DBMIN)	VIPRF	2842
		VIPRF	2843
	DO 40 I=1,N	VIPRF	2844
40	IF(DB2(I).LT.DBMIN) DB2(I)=DBMIN	VIPRF	2845
	40 CONTINUE	VIPRF	2846
		VIPRF	2847
	CALL CURVE(FREQ,DB2,N,0)	VIPRF	2848
		VIPRF	2849
45	X1=ALOG10(FMAX)-1.1/XCYCLE X1=10.0**X1	VIPRF	2850
	X2=DBMAX-0.25*YSTEP	VIPRF	2851
	CALL PARAMS(X1,X2,DYVAL,XMAKNO,H,X,IX,RS,IFLITE,HITE,HITE1)	VIPRF	2852
	RETURN	VIPRF	2853
	END	VIPRF	2854

SYMBOLIC REFERENCE MAP (R=1)

SUBROUTINE TWOFUN

74/74

OPT=1

FTN 4.5+414

08/16/77 13.11.28

ENTRY POINTS  
3 TWOFUN

VARIABLES	SN	TYPE	RELOCATION
7	CATGEV	REAL	PLOTT
8	DEMIN	REAL	F.P.
9	DP2	REAL	ARRAY F.P.
10	FMAX	REAL	F.P.
11	FREQ	REAL	ARRAY F.P.
12	HITE	REAL	PLOTT
13	I	INTEGER	
14	IFLITE	INTEGER	PLOTT
15	INOPLT	INTEGER	PLOTT
16	IPLANE	INTEGER	ARRAY PLOTT
17	IX	INTEGER	PLOTT
18	LYNAME	INTEGER	ARRAY PLOTT
19	RS	REAL	PLOTT
20	WE	REAL	PLOTT
21	X	REAL	PLOTT
22	XCYCLE	REAL	PLOTT
23	XY	REAL	PLOTT
24	X2	REAL	PLOTT
25	X4	REAL	PLOTT
26	YSTEP	REAL	PLOTT

FILE NAMES	MODE
OUTPUT	FMT

EXTERNALS	TYPE	ARGS
ALOG10	REAL	1 LIBRARY
CURVE		4
HEADIN		6
PARAMS		11
TICKMK		6
XLOG		4

INLINE FUNCTIONS	TYPE	ARGS
AFS	REAL	1 INTRIN

FILE NAMES  
OUTPUT FMT

EXTERNALS	TYPE	ARGS
ALOG10	REAL	1 LIBRARY
CURVE		4
HEADIN		6
PARAMS		11
TICKMK		6
XLOG		4

INLINE FUNCTIONS	TYPE	ARGS
AFS	REAL	1 INTRIN

STATEMENT LABELS

0 10  
0 40

277 20 FMT

67 30

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
20	10	* I	12 16	250	EXT REFS
135	40	I	39 41	30	INSTACK

COMMON BLOCKS	LENGTH
PLOTT	48

STATISTICS

PROGRAM LENGTH	3520	234
COMMON LENGTH	500	48

SUBROUTINE LCCFPA		74/74	OPT=1	FTN 4.5+414	08/16/77	13.11.28
1	SUBROUTINE LCCFPA(BLQ,BHI,XLO,XHI,FZRCLO,FZROHI,ALO,AHI,FMIN, 1FMAX,YVAL,DYVAL,ILQHI)				VIPRF	2855
					VIPRF	2856
					VIPRF	2857
5	COMMON/PFLCTT/H,XMAKNO,X,RS,WE,WS,IFLITE,CATGEY,ILINE1(7), 1ITITL1(7),IPLANE(3),LXNAME(4),LYNAME(4),XCYCLE,YSTEP,YAXIS, 2XAXIS,HITE,HITE1,TICLEN,Y1,X2,X3,X4,XX,IPHASE				VIPRF	2858
					VIPRF	2859
					VIPRF	2860
	DATA IHJ/2HHI/				VIPRF	2861
					VIPRF	2862
10	WIDTH=1.2F				VIPRF	2863
	FZLO=FZRCLO \$IF(FZRCLO.LT.FMIN) FZLO=FMIN				VIPRF	2864
	FZHI=FZROHI \$IF(FZROHI.GT.FMAX) FZHI=FMAX				VIPRF	2865
	IF(ILQHI.NE.IHI) GO TO 100				VIPRF	2866
	X3=FZHI \$X4=FMAX				VIPRF	2867
15	DHIMAX=ALOG10(FMAX/FZHI)*XCYCLE \$IF(DHIMAX.GE.WIDTH) GO TO 220				VIPRF	2868
	X3=FMIN \$X4=FZHI				VIPRF	2869
	GO TO 220				VIPRF	2870
					VIPRF	2871
					VIPRF	2872
20	100 DLOHI=ALOG10(FZHI/FZLO)*XCYCLE \$DHIMAX=ALOG10(FMAX/FZHI)*XCYCLE				VIPRF	2873
	XX=ALOG10(FZLO/FMIN)*XCYCLE \$IF(XX.LT.WIDTH) GO TO 140				VIPRF	2874
	IF(DHIMAX.LT.WIDTH) GO TO 120				VIPRF	2875
	X1=FMIN \$X2=FZLO \$X3=FZHI \$X4=FMAX				VIPRF	2876
	GO TO 200				VIPRF	2877
					VIPRF	2878
25	120 X1=FMIN \$X4=FZLO \$IF(DLOHI.LT.WIDTH) GO TO 180				VIPRF	2879
	X1=FMIN \$X3=FZLO \$X3=FZLO \$X4=FZHI				VIPRF	2880
	GO TO 200				VIPRF	2881
					VIPRF	2882
					VIPRF	2883
30	140 IF(DLOHI.LT.WIDTH) GO TO 160				VIPRF	2884
	X1=FZLO \$X4=FZHI				VIPRF	2885
	IF(DHIMAX.LT.WIDTH) GO TO 180				VIPRF	2886
	X1=FZLO \$X2=FZHI \$X3=FZHI \$X4=FZHI				VIPRF	2887
	GO TO 200				VIPRF	2888
					VIPRF	2889
35	160 IF(DHIMAX.LT.WIDTH) RETURN				VIPRF	2890
	X1=FZHI \$X4=FMAX				VIPRF	2891
					VIPRF	2892
					VIPRF	2893
40	180 XX=ALOG10(X4/X1)*XCYCLE \$XX=(XX-2.0*WIDTH)/3.0				VIPRF	2894
	Y2=ALOG10(X1) \$X3=X2+(XX*WIDTH)/XCYCLE \$X3=10.0**X3				VIPRF	2895
	X2=X2+(2.0**XX*WIDTH)/XCYCLE \$X2=10.0**X2				VIPRF	2896
					VIPRF	2897
	200 CALL FFOXPA(FZLO,FLO,YLO,ALO,X1,X2,YVAL,DYVAL,XCYCLE,3,0)				VIPRF	2898
	220 CALL FFOXPA(FZHI,FHI,XHI,AHI,X3,X4,YVAL,DYVAL,XCYCLE,3,1)				VIPRF	2899
45	RETURN				VIPRF	2900
	END					

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS  
3 LCCFPA

SUBROUTINE LOCFBXA				74/74	OPT=1	FTN 4.5+414		08/16/77 13.11.28	
VARIABLES	SN	TYPE	RELOCATION						
0 AHI		REAL	F.P.	0	ALO	REAL	F.P.		
0 BHI		REAL	F.P.	0	BLO	REAL	F.P.		
7 CATGRV		REAL	PLOTT	222	DHIMAX	REAL			
223 DLOHI		REAL		0	DYVAL	REAL	F.P.		
0 FMAX		REAL	F.P.	0	FMIN	REAL	F.P.		
221 FZHI		REAL		220	FZLO	REAL			
0 FZPOHI		REAL	F.P.	0	FZROLO	REAL	F.P.		
0 H		REAL	PLOTT	45	HITE	REAL	PLOTT		
46 HITE1		REAL	PLOTT	6	IFLITE	INTEGER	PLOTT		
206 IHI		INTEGER		10	ILINE1	INTEGER	ARRAY	PLOTT	
0 ILOHI		INTEGER	F.P.	55	IPHASE	INTEGER	PLOTT		
26 IPLANE		INTEGER	ARRAY	17	ITITL1	INTEGER	ARRAY	PLOTT	
31 LYNAMF		INTEGER	ARRAY	35	LYNAME	INTEGER	ARRAY	PLOTT	
3 RS		REAL	PLOTT	47	TICLEN	REAL	PLOTT		
4 WF		REAL	PLOTT	217	WIDTH	REAL			
5 WS		REAL	PLOTT	2	X	REAL	PLOTT		
44 XAXIS		REAL	PLOTT	41	XCYCLE	REAL	PLOTT		
0 XHI		REAL	F.P.	0	XLO	REAL	F.P.		
1 XPAKNO		REAL	PLOTT	54	XX	REAL	PLOTT		
F0 X1		REAL	PLOTT	51	X2	REAL	PLOTT		
F2 X7		REAL	PLOTT	53	X4	REAL	PLOTT		
43 YAXIS		REAL	PLOTT	42	YSTEP	REAL	PLOTT		
0 YVAL		REAL	F.P.						
EXTERNALS	TYPE	ARGS							
ALOG10	REAL	1 LIBRARY		FRCXBA		11			
STATEMENT LABELS									
74 100		61 120				71 140			
102 160		107 180				133 200			
144 220									
COMMON BLOCKS	LENGTH								
PLOTT	46								
STATISTICS									
PROGRAM LENGTH		2248	148						
OF LABELED COMMON LENGTH		568	46						

SUBROUTINE DBELMAX 74/74 CPT-1

FTN 4.5+414

08/16/77 13.11.28

```

1      SUBROUTINE DBELMAX(PEAK,YSTEP,DBMAX)
      I=PEAK/YSTP $J=0 $SIGN=-1.0 $IF(PEAK.LT.0.) GO TO 10
      J=1 $SIGN=1.0
      DBMAX=YSTP*(I+J)
5      IF (AMOD(PEAK,YSTEP).GT.SIGN*YSTP/2.) DBMAX=DBMAX+F.
      RETURN
      END

```

```

VIPRF 2901
VIPRF 2902
VIPRF 2903
VIPRF 2904
VIPRF 2905
VIPRF 2906
VIPRF 2907

```

## SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS  
7 DBELMAX

VARIABLES	SN	TYPE	RELOCATION			
0 DBMAX		REAL	F.F.	35	I	INTEGER
36 J		INTEGER		0	PEAK	REAL
37 SIGN		REAL		0	YSTP	REAL

F.P.  
F.P.

INLINE FUNCTIONS    TYPE    ARCS  
AMOD    REAL    2    INTRIN

STATEMENT LABELS  
15 16

STATISTICS  
PROGRAM LENGTH    405    32



SUBROUTINE GPOINTS 74/74 OPT=1 FTN 4.5+414 08/16/77 13.11.28

```

1      SUBROUTINE GPOINTS(FREQ,DEGBEL,FRQ,FMAX,CONST,DB,XFERMX,TWOB,FLX,
      1FZ,HILC,SIGN,ALPHA,II,J,K,L)
      DIMENSION XFERMX(4),TWOB(4),FZ(4),ALPHA(4),FLX(4)
      DIMENSION FREQ(1),DEGBEL(1),DB(4),DBPRV(4),HILC(4),SIGN(4)
      DO 20 I=1,K
      IF(L.EQ.I) GO TO 20
      X1=FREQ/FZ(I) $DBPRV(I)=DB(I)
      DB(I)=XFERMX(I)+20.*ALOG10((HILC(I)+SIGN(I)*ATAN2(
10    1TWOB(I)*(X1**ALPHA(I)),1.-X1*X1))/FLX(I))
      20 CONTINUE
      X1=DB(1) $X2=DB(2) $X3=DB(3) $X4=DB(4) $ITYPE=ITYPE
      IF(X1.LE.X2) GO TO 30
      IF(X1.LE.X3) GO TO 40
      IF(X1.LE.X4) GO TO 50
      ITYPE=1 $GO TO 60
      30 IF(X2.LE.X3) GO TO 40
      IF(X2.LE.X4) GO TO 50
      ITYPE=2 $GO TO 60
      40 IF(X3.LE.X4) GO TO 50
      ITYPE=3 $GO TO 60
      50 ITYPE=4
      60 IF(ITYPE.NE.ITYPEF.AND.II.EQ.0) GO TO 70
      J=J+1 $FREQ(J)=FREQ $DBREL(J)=DB(ITYPE) $GO TO 80
      70 X1=DBPRV(ITYPE)-DBPRV(ITYPEF)
      FREQ=FFRV+CONST*FFRV*X1/(X1+DB(ITYPEF)-DB(ITYPE))
      J=J+1 $FREQ(J)=FREQ $X1=FREQ/FZ(ITYPE)
      35 X1=XFERMX(ITYPE)+20.*ALOG10((HILC(ITYPE)+SIGN(ITYPE)*
      1ATAN2(TWOB(ITYPE)*(X1**ALPHA(ITYPE)),1.-X1*X1))/FLX(ITYPE))
      DBREL(J)=X1
      80 IF(FREQ.GE.20.0.AND.FREQ.LE.500.0) X1=CONST/2.0
      IF(FREQ.LT.20.0.OR.FREQ.GT.500.0) X1=CONST
      FPRV=FREQ
      FREQ=FREQ+X1*FREQ $IF(FREQ.GT.FMAX) RETURN
      II=0 $GO TO 10
      END

```

VIPRF 2908  
VIPRF 2909  
VIPRF 2910  
VIPRF 2911  
VIPRF 2912  
VIPRF 2913  
VIPRF 2914  
VIPRF 2915  
VIPRF 2916  
VIPRF 2917  
VIPRF 2918  
VIPRF 2919  
VIPRF 2920  
VIPRF 2921  
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VIPRF 2939  
VIPRF 2940  
VIPRF 2941  
VIPRF 2942  
VIPRF 2943  
VIPRF 2944  
VIPRF 2945  
VIPRF 2946  
VIPRF 2947  
VIPRF 2948  
VIPRF 2949  
VIPRF 2950  
VIPRF 2951

## SYMBOLIC REFERENCE MAP (P=1)

ENTRY POINTS  
7 GPOINTS

VARIABLES	SN	TYPE	RELOCATION						
0 ALPHA	REAL	ARRAY	F.P.	0	CONST	REAL			F.P.
0 DB	REAL	ARRAY	F.P.	206	DBPRV	REAL	ARRAY		

```

SUBROUTINE GPOINTS 74/74 OPT=1
FTN 4.5+414 08/16/77 13.11.28

VARIABLES      SN  TYPE      RELOCATION
0  DECBLL      REAL      ARRAY      F.P.
0  FMAX        REAL      F.P.
0  FREQ        REAL      ARRAY      F.P.
0  FZ          REAL      ARRAY      F.P.
176 I          INTEGER
204 ITYPEP     INTEGER
0  J           INTEGER      F.P.
0  L           INTEGER      F.P.
0  THOP        REAL      ARRAY      F.P.
177 X1         REAL
201 X3         REAL

EXTERNALS      TYPE      ARGS
ALOG10        REAL      1 LIBRARY

STATEMENT LABELS
15 10          40 20
67 40          67 50
104 70         146 80

LCOPS LABEL    INDEX    FROM-TO    LENGTH    PROPERTIES
16 20          * I      6 11      258      EXT REFS

STATISTICS
PROGRAM LENGTH      258      173

```

SUBROUTINE XFERFUN 74/74 OPT=1

FTN 4.5+414

08/16/77 13.11.28

1	SUBROUTINE XFERFUN(FREQ,DECBEL,N,PEAK,XLO,XHI,BLO,BHI,FZEROL,	VIPRF	2952
	1 FZEROL,ALC,AHI,ILOHI)	VIPRF	2953
	DIMENSION FREQ(1),DECBEL(1)	VIPRF	2954
	DATA PI/3.141592657,IHI/24HI/	VIPRF	2955
5	J=1 \$IF(ILOHI.EQ.IHI) GO TO 40	VIPRF	2956
		VIPRF	2957
	FMAX=XLO*FZEROL \$TWOB=2.*BLO	VIPRF	2958
	FLX=ATAN2(TWOB*(XLO**ALO),1.-XLO*XLO)	VIPRF	2959
		VIPRF	2960
10	DO 10 I=1,N	VIPRF	2961
	J=I \$FREQ=FREQ(I) \$IF(FREQ.GT.FMAX) GO TO 20	VIPRF	2962
	X1=FREQ/FZEROL	VIPRF	2963
	10 DECBEL(I)=PEAK+20.*ALOG10(ATAN2(TWOB*(X1**ALO),1.-X1*X1)/FLX)	VIPRF	2964
		VIPRF	2965
15	20 X1=FMAX \$FMAX=YHI*FZEROL \$IF(X1.EQ.FMAX) GO TO 40	VIPRF	2966
	20 FREQ=FREQ(J) \$IF(FREQ.GT.FMAX) GO TO 40	VIPRF	2967
	DECBEL(J)=PEAK \$J=J+1	VIPRF	2968
	GO TO 20	VIPRF	2969
		VIPRF	2970
20	40 TWOB=2.*BHI \$FLX=PI-ATAN2(TWOB*(XHI**AHI),1.-XHI*XHI)	VIPRF	2971
		VIPRF	2972
	DO 50 I=J,N	VIPRF	2973
	FREQ=FREQ(I) \$X1=FREQ/FZEROL	VIPRF	2974
	50 DECBEL(I)=PEAK+20.*ALOG10((PI-ATAN2(TWOB*(X1**AHI),1.-X1*X1))/FLX)	VIPRF	2975
25		VIPRF	2976
	RETURN	VIPRF	2977
	END	VIPRF	2978

## SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS  
3 XFERFUN

VARIABLES	SN	TYPE	RELOCATION				
0 AHI		REAL	F.P.	0	ALO	REAL	F.P.
0 AHI		REAL	F.P.	0	BLO	REAL	F.P.
0 DECBEL		REAL	ARRAY	135	FLX	REAL	
133 FMAX		REAL		0	FREQ	REAL	ARRAY
137 FREQ		REAL		0	FZEROL	REAL	F.P.
0 FZEROL		REAL	F.P.	136	I	INTEGER	
126 IHI		INTEGER		0	ILOHI	INTEGER	F.P.
132 J		INTEGER		0	N	INTEGER	F.P.
0 PEAK		REAL	F.P.	125	PI	REAL	
134 TWOB		REAL		0	XHI	REAL	F.P.
0 XLO		REAL	F.P.	140	X1	REAL	

EXTERNALS	TYPE	ARCS				
ALOG10	REAL	1	LIBRARY	ATAN2	REAL	2
						LIBRARY

STATEMENT LABELS

0	10	54	20
70	40	0	50

0 30

INACTIVE

SUBROUTINE XFERFUN				74/74	OPT=1	FTN 4.5+414		08/16/77 13.11.28
LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS	EXITS	
32	10	* I	10 13	219		EXT REFS		
103	50	* I	22 24	208		EXT REFS		
STATISTICS								
PROGRAM LENGTH				1778	127			

SLBROUTINE PARAMS 74/74 OPT=1

FTN 4,5+414

08/16/77 13.11.28

1	SUBROUTINE PARAMS (XVAL,YVAL,DYVAL,XMAKNO,H,DISTFT,JX,RS,IFLITE,	VIPRF	2979
	1HITF,HITF1)	VIPRF	2980
	CALL HEIGHT(HITE1)	VIPRF	2981
	CALL RLMESS("(H)=S",+100,XVAL,YVAL)	VIPRF	2982
5	CALL FLRFAL(XMAKNO,+2,"ABUT","ABUT")	VIPRF	2983
	CALL RLMESS("(H)=S",+100,XVAL,YVAL-DYVAL)	VIPRF	2984
	II=H *CALL INTNO(II,"ABUT","ABUT")	VIPRF	2985
	CALL RLMESS("(FT)=S",+100,"ABUT","ABUT")	VIPRF	2986
	CALL RLMESS("(X)=S",+100,XVAL,YVAL-2.0*DYVAL)	VIPRF	2987
10	CALL FLRFAL(DISTFT,1,"ABUT","ABUT")	VIPRF	2988
	CALL RLMESS("(FT)=S",+100,"ABUT","ABUT")	VIPRF	2989
	CALL RLMESS(JX,+100,XVAL,YVAL-2.5*DYVAL)	VIPRF	2990
	CALL RLMESS("(R)=S",+100,XVAL,YVAL-3.5*DYVAL)	VIPRF	2991
	CALL FLREAL(RS,+1,"ABUT","ABUT")	VIPRF	2992
15	CALL RLMESS("(IN)=S",+100,"ABUT","ABUT")	VIPRF	2993
	CALL RLMESS("(SS)=S",+100,XVAL,YVAL-4.0*DYVAL)	VIPRF	2994
	CALL RESET("BASALF")	VIPRF	2995
	CALL RLMESS(IFLITE,10,XVAL,YVAL-5.0*DYVAL)	VIPRF	2996
	CALL BASALF("L/CSTO")	VIPRF	2997
20	CALL HEIGHT(HITE)	VIPRF	2998
	RETURN	VIPRF	2999
	END	VIPRF	3000

## SYMBOLIC REFERENCE MAP (R=1)

## ENTRY POINTS

7 PARAMS

VARIABLES	SN	TYPE	RELOCATION			
0 DISTFT		REAL	F.P.	0	DYVAL	REAL F.P.
0 H		REAL	F.P.	0	HITE	REAL F.P.
0 HITF1		REAL	F.P.	0	IFLITE	INTEGER F.P.
240 II		INTEGER		0	JX	INTEGER F.P.
0 RS		REAL	F.P.	0	XMAKNO	REAL F.P.
0 XVAL		REAL	F.P.	0	YVAL	REAL F.P.

EXTERNALS	TYPE	ARCS			
BASALF		1	HEIGHT		1
INTNO		3	RESET		1
RLMESS		6	FLREAL		4

## STATISTICS

PROGRAM LENGTH 3418 225



SUBROUTINE TABLE      74/74    OPT=1      FTN 4.5+414      08/16/77    13.11.28

1	SUBROUTINE TABLE(FREQ,DB,N,IFUN,ISCRPT)	VIPRF	3001
	DIMENSION FREQ(1),DB(1)	VIPRF	3002
	PRINT 10,IFUN,IFUN,IFUN,IFUN,ISCRPT,ISCRPT,ISCRPT,ISCRPT	VIPRF	3003
5	10 FORMAT(1H=,* FREQ.(HZ.)*,2X,A10,3(14X,*FREQ.(HZ.)*,2X,A10)/	VIPRF	3004
	116X,A2,3(34X,A2))	VIPRF	3005
	NLINES=N/4 \$LINPRT=MOD(N,4)	VIPRF	3006
	DO 20 I=1,NLINES	VIPRF	3007
	I1=I+NLINES \$I2=I1+NLINES \$I3=I2+NLINES	VIPRF	3008
10	20 PRINT 70,FREQ(I),DB(I),FREQ(I1),DB(I1),FREQ(I2),DB(I2),FREQ(I3),	VIPRF	3009
	100(I1))	VIPRF	3010
	30 FORMAT(F10.1,F12.2,3(F24.1,F12.2))	VIPRF	3011
	IF (LINPRT.EQ.0) RETURN	VIPRF	3012
15	NLINES=N-LINPRT+1	VIPRF	3013
	DO 40 I=NLINES,N	VIPRF	3014
	40 PRINT 80,FREQ(I),DB(I)	VIPRF	3015
20	50 FORMAT(106X,F12.1,F12.2)	VIPRF	3016
	RETURN	VIPRF	3017
	END	VIPRF	3018
		VIPRF	3019
		VIPRF	3020
		VIPRF	3021
		VIPRF	3022
		VIPRF	3023

## SYMBOLIC REFERENCE MAP (P=1)

ENTRY POINTS  
3 TABLE

VARIABLES	SM	TYPE	RELOCATION						
0 DB		REAL	AFRAY	F.P.	0	FREQ	REAL	ARRAY	F.P.
143 I		INTEGER			0	IFUN	INTEGER		F.P.
0 ISCRPT		INTEGER		F.P.	144	I1	INTEGER		
145 I2		INTEGER			146	I3	INTEGER		
142 LINPRT		INTEGER			0	N	INTEGER		F.P.
141 NLINES		INTEGER							

FILE NAMES      MODE  
OUTPUT      FMTINLINE FUNCTIONS      TYPE      ARGS  
MCD      INTEGER      2      INTPIN

STATEMENT LABELS									
102	10	FMT		0	20				
0	40			136	50	FMT		125	30      FMT

LOCES	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
24	20	* I	0 10	25B	EXT REFS
55	40	* I	18 19	11B	EXT REFS

STATISTICS			
PROGRAM LENGTH		171B	121

SUBROUTINE TICKMK 74/74 OPT=1

FTN 4.F+414

08/16/77 13.11.28

1	SUBROUTINE TICKMK(TICLEN,FMAX,YSTEP,YAXIS,DBMIN)	VIPRF	3024
	DIMENSION FREQ(2),DECPCL(2)	VIPRF	3025
		VIPRF	3026
	Y1=ALOG10(FMAX) \$X2=Y1-2.5*TICLEN \$X1=X1-TICLEN	VIPRF	3027
5	X1=10.**X1 \$X2=10.**X2	VIPRF	3028
	DBMAX=DBMIN+YSTEP*YAXIS \$DB=DBMIN \$DELOB=YSTEP/5.	VIPRF	3029
	FREQ(1)=FMAX \$FREQ(2)=FMAX \$DECPCL(1)=DBMIN \$DECPCL(2)=DBMAX	VIPRF	3030
	CALL CURVE(FREQ,DECPCL,2,0)	VIPRF	3031
		VIPRF	3032
10	17 DB=DELOB	VIPRF	3033
	IF(DB.GT.DBMAX) RETURN	VIPRF	3034
	FREQ(1)=Y1 \$IF(AMOD(DB, YSTEP).EQ.0.) FREQ(1)=X2	VIPRF	3035
	DECPCL(1)=DB \$DECPCL(2)=DB	VIPRF	3036
	CALL CURVE(FREQ,DECPCL,2,0)	VIPRF	3037
15	GO TO 10	VIPRF	3038
		VIPRF	3039
	RETURN	VIPRF	3040
	END	VIPRF	3041

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

17 I THERE IS NO PATH TO THIS STATEMENT.

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS  
3 TICKMK

VARIABLES	SN	TYPE	RELOCATION					
66 DB		REAL		65 DBMAX	REAL			
0 DBMIN		REAL	F.P.	72 DECPCL	REAL	ARRAY		
67 DELOB		REAL		0 FMAX	REAL			F.P.
70 FREQ		REAL	ARRAY	0 TICLEN	REAL			F.P.
63 X1		REAL		64 X2	REAL			
0 YAXIS		REAL	F.P.	0 YSTEP	REAL			F.P.

EXTERNALS	TYPE	ARGS		
ALOG10	REAL	1	LIBRARY	
			CURVE	4

INLINE FUNCTIONS	TYPE	ARGS
AMOD	REAL	2
		INTRIN

STATEMENT LABELS  
71 10STATISTICS  
PROGRAM LENGTH 749 60

```

SUBROUTINE FROXBA (FZERO, BETA, X, ALPHA, F1, F2, Y, DY, XCYLE, NXPLAC,
1 IPRIIME)
DATA WIDTH/1.25/
2
3 XX=ALOG10(F2/F1)*XCYLE BXX=(XX-WIDTH)/2.0
4 XX=ALOG10(F1)+XX/XCYLE BXX=10.0**XX
5 IF=3HF = SIX=3HX = SIP=3HR = $IA=3HA =
6 IF(IPRIIME.EQ.1) GO TO 10
7 IF=3HF = SIX=3HX = SIP=3HR = $IA=3HA =
10
11 CALL FLMESS(IF,3,XX,Y)
12 CALL FLREAL(FZERO,1,"ABUT","ABUT")
13 CALL FLMESS(" (H) 75",+100,"ABUT","ABUT")
14 CALL FLMESS(" 05",+100,XX,Y=0.5*DY)
15 CALL FLMESS(IX,3,XX,Y=1.5*DY)
16 CALL FLREAL(X,NXPLAC,"ABUT","ABUT")
17 CALL BASALF("L/CPELK")
18 CALL FLMESS(IR,3,XX,Y=2.5*DY)
19 CALL FLREAL(BETA,3,"ABUT","ABUT")
20 CALL FLMESS(IA,3,XX,Y=3.5*DY)
21 CALL FLREAL(ALPHA,2,"ABUT","ABUT")
22 CALL BASALF("L/CSTR")
23
24 RETURN
25 END

```

VIPRF 3042  
 VIPRF 3043  
 VIPRF 3044  
 VIPRF 3045  
 VIPRF 3046  
 VIPRF 3047  
 VIPRF 3048  
 VIPRF 3049  
 VIPRF 3050  
 VIPRF 3051  
 VIPRF 3052  
 VIPRF 3053  
 VIPRF 3054  
 VIPRF 3055  
 VIPRF 3056  
 VIPRF 3057  
 VIPRF 3058  
 VIPRF 3059  
 VIPRF 3060  
 VIPRF 3061  
 VIPRF 3062  
 VIPRF 3063  
 VIPRF 3064  
 VIPRF 3065  
 VIPRF 3066

## SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS  
 3 FROXBA

VARIABLES	SN	TYPE	RELOCATION			
0 ALPHA	REAL	F.F.	0 BETA	REAL	F.P.	
0 DY	REAL	F.F.	0 FZERO	REAL	F.P.	
0 F1	REAL	F.F.	0 F2	REAL	F.P.	
231 IA	INTEGER		230 IB	INTEGER		
226 IF	INTEGER		0 IPRIIME	INTEGER	F.P.	
227 IX	INTEGER		0 NXPLAC	INTEGER	F.P.	
203 WIDTH	REAL		0 X	REAL	F.F.	
0 XCYLE	REAL	F.F.	225 XY	REAL		
0 Y	REAL	F.F.				

EXTERNALS	TYPE	ARGS			
ALOG10	REAL	1 LIBRARY	BASALF	1	
FLMESS		4	FLREAL	4	

STATEMENT LABELS  
 36 10

STATISTICS  
 PROGRAM LENGTH 2648 192

SUBROUTINE BETA

74/74 OPT=1

FTN 4.5+414

08/16/77 13.11.28

1	SUBROUTINE BETA(B,PEAK,SPLVAL,X,ALPHA,FREQ,FZERO,SGN,HILO)	VIPRF	3067
	FBETA(XX,PEAK,SPLVAL,X,ALPHA,FREQ,FZERO,SGN,HILO)=	VIPRF	3068
	1(10.0**((SPLVAL-PEAK)/20.0))*	VIPRF	3069
5	2(HILO+SGN*ATAN2(2.0*XX**ALPHA,1.0-XX))-	VIPRF	3070
	3(HILO+SGN*ATAN2(2.0*XX*(FREQ/FZERO)**ALPHA,	VIPRF	3071
	41.0-(FREQ/FZERO)*(FREQ/FZERO)))	VIPRF	3072
		VIPRF	3073
		VIPRF	3074
	PPRV=1.0 DELP=0.05	VIPRF	3075
10	FPRV=FBETA(PPRV,PEAK,SPLVAL,X,ALPHA,FREQ,FZERO,SGN,HILO)	VIPRF	3076
	B=PPRV*DELP	VIPRF	3077
	F=FBETA(B,PEAK,SPLVAL,X,ALPHA,FREQ,FZERO,SGN,HILO)	VIPRF	3078
	IF(FPRV*F.LE.0.) GO TO 30	VIPRF	3079
	IF(ABS(FPRV).GT.ABS(F)) GO TO 10	VIPRF	3080
15	DELP=-DELP B=PPRV F=FPRV	VIPRF	3081
		VIPRF	3082
	10 PPRV=P FPRV=F B=B*DELP	VIPRF	3083
	F=FBETA(B,PEAK,SPLVAL,X,ALPHA,FREQ,FZERO,SGN,HILO)	VIPRF	3084
	IF(FPRV*F.GT.0.) GO TO 10	VIPRF	3085
20		VIPRF	3086
	30 B=(PPRV*F-B*FPRV)/(F-FPRV)	VIPRF	3087
	RETURN	VIPRF	3088
	END	VIPRF	3089

## SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS  
3 BETA

VARIABLES	SN	TYPE	RELOCATION				
0 ALPHA		REAL	F.P.	0	P	REAL	F.P.
157 PPRV		REAL		160	DELP	REAL	
162 F		REAL		161	FPRV	REAL	
0 FREQ		REAL	F.P.	0	FZERO	REAL	F.P.
0 HILO		REAL	F.P.	0	PEAK	REAL	F.P.
0 SGN		REAL	F.P.	0	SPLVAL	REAL	F.P.
0 X		REAL	F.P.				

EXTERNALS  
ATAN2 REAL ARCS 2 LIBRARYINLINE FUNCTIONS  
ABS REAL ARCS 1 INTRIN FPETA REAL 9 SFSTATEMENT LABELS  
103 10 147 30STATISTICS  
PROGRAM LENGTH 1638 11F

SUBROUTINE TERPLIN		74/74	OPT=1	FTN 4,5+414	08/16/77	13.11.28
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1	SUBROUTINE TERPLIN(X,DELX,XINIT,XARRAY,IXARRAY,Y,YARRAY,N)	VIPRF	3090
	DIMENSION XARRAY(1),YARRAY(1)	VIPRF	3091
		VIPRF	3092
5	IF(IXARRAY.EQ.1) GO TO 100	VIPRF	3093
		VIPRF	3094
	I=(X-XINIT)/DELX \$XI=I	VIPRF	3095
	Y=YARRAY(I+1)+(X-XINIT-XI*DELX)*(YARRAY(I+2)-YARRAY(I+1))/DELX	VIPRF	3096
	RETURN	VIPRF	3097
10		VIPRF	3098
	100 DO 110 I=1,N	VIPRF	3099
	J=I \$IF(XARRAY(I).GE.X) GO TO 120	VIPRF	3100
	110 CONTINUE	VIPRF	3101
15		VIPRF	3102
	120 IF(XARRAY(J).NE.X) GO TO 130	VIPRF	3103
	Y=YARRAY(J) \$RETURN	VIPRF	3104
		VIPRF	3105
	130 Y=YARRAY(J-1) +	VIPRF	3106
20	1(X-XARRAY(J-1))*(YARRAY(J)-YARRAY(J-1))/(XARRAY(J)-XARRAY(J-1))	VIPRF	3107
		VIPRF	3108
	RETURN	VIPRF	3109
	END	VIPRF	3110
		VIPRF	3111
		VIPRF	3112

## SYMBOLIC REFERENCE MAP (P=1)

ENTRY POINTS  
3 TERPLIN

VARIABLES	SN	TYPE	RELOCATION			
0 DELX		REAL	F.P.	61	I	INTEGER
0 IXARRAY		INTEGER	F.P.	63	J	INTEGER
0 N		INTEGER	F.P.	0	X	REAL
0 XARRAY		REAL	ARRAY	62	XI	REAL
0 XINIT		REAL	F.P.	0	Y	REAL
0 YARRAY		REAL	ARRAY			F.P.

## STATEMENT LABELS

31	100		0	110		40	120
47	130						

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXITS
32	110	* I	12 14	60	INSTACK	

## STATISTICS

PROGRAM LENGTH	1143	68
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SUBROUTINE QUAD      74/74    OPT=1      FTN 4.5+414      08/16/77  13.11.28

1      SUBROUTINE QUAD(X,DELY,XINITL,Y,YVALS,N)      VIPRF  3113
      DIMENSION YVALS(1)      VIPRF  3114

      XI=(X-XINITL)/DELY $I=XI $XI=I      VIPRF  3115
5      X1=XINITL+XI*DELY $XX1=X-X1      VIPRF  3116
      I=I+1 $IF(XX1.NE.0.) GO TO 10      VIPRF  3117
      Y=YVALS(I) $RETURN      VIPRF  3118
      VIPRF  3119
10     10 X3=X1+DELY $K=I+1 $IF(I.NE.1) GO TO 20      VIPRF  3120
      X2=X3+DELY $J=K+1 $GO TO 33      VIPRF  3121
      VIPRF  3122
20     20 X2=X1-DELY $J=I-1      VIPRF  3123
      VIPRF  3124
15     30 XX2=X-X2 $XX3=X-X3      VIPRF  3125
      X1X2=X1-X2 $X1X3=Y1-X3 $X2X3=X2-X3      VIPRF  3126
      Y=XX2*XX3*YVALS(I)/(X1X2*X1X3)-XX1*XX3*YVALS(J)/(X1X2*X2X3)+      VIPRF  3127
      1XX1*XX2*YVALS(K)/(X1X3*X2X3)      VIPRF  3128
      RETURN      VIPRF  3129
20     END      VIPRF  3130
      VIPRF  3131
      VIPRF  3132

```

## SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS  
3 QUAD

VARIABLES	SN	TYPE	RELOCATION				
0 DELX		REAL	F.P.	62	I	INTEGER	
70 J		INTEGER		66	K	INTEGER	
0 N		INTEGER	*UNUSED F.P.	0	X	REAL	F.P.
61 XI		REAL		0	XINITL	REAL	F.P.
64 XX1		REAL		71	XX2	REAL	
72 XX3		REAL		63	X1	REAL	
73 X1X2		REAL		74	X1X3	REAL	
67 X2		REAL		75	X2X3	REAL	
65 X3		REAL		0	Y	REAL	F.P.
0 YVALS		REAL	ARRAY F.P.				

STATEMENT LABELS  
21 10

31 20

36 30

STATISTICS  
PROGRAM LENGTH

760 62

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